# OPTIMIZATION OF A TECHNIQUE FOR PHOSPHORESCENCE LIFETIME IMAGING OF OXYGEN TENSION IN THE MOUSE RETINA

by

Amanda C. Kight

A Thesis

Submitted to the Faculty

of the

## WORCESTER POLYTECHNIC INSTITUTE

in partial fulfillment of the requirements for the

Degree of Master of Science

in

Biomedical Engineering

by

April 2002

APPROVED;

Moss D. Shonat, Ph.D., Major Advisor

Karl C Helmer Ph D Committee Member

Elizabeth Ryder, Ph.D., Committee Member

#### **ACKNOWLEDGEMENTS**

Funding for this project was provided, in part, by a pilot an feasibility grant from the Diabetes and Endocrinology Resource Center (DERC) at the University of Massachusetts Medical School, Worcester, MA, and by a biomedical engineering research grant from the Whitaker Foundation, Rosslyn VA.

I would like to extend my thanks to my family and friends for their support throughout my academic career, and to:

*Kevin Hawkins and Daniel Traviglia*, for their help with hardware and software issues, respectively, and for keeping the lab fun;

*Karl Helmer and Elizabeth Ryder*, my thesis committee, for taking interest in this project and providing constructive criticism;

*Ross Shonat*, my advisor and role model, for having tremendous faith in me and continuously encouraging me to reach my fullest potential.

#### **ABSTRACT**

Retinal hypoxia and inadequate oxygen delivery have been implicated as causal for the development of several eye diseases, including diabetic retinopathy, glaucoma, and retinopathy of prematurity. The imaging of oxygen tension in the retina, generated from a measure of the phosphorescence lifetimes of bolus-injected palladium-porphyrin probes, has been used successfully to study retinal oxygen dynamics in numerous animal models. However, the specific parameters for applying this technique in the mouse have not been thoroughly investigated. The goals of this project were to calibrate a newlyconstructed phosphorescence lifetime imaging instrument and data analysis software against known oxygen concentrations, to determine specific parameters for probe excitation and image collection and analysis in the mouse eye, and to assess any damage caused to the eye by the technique using histological analysis. An in vitro system was developed for calibration of the probe and for estimation of power of excitation light and camera settings necessary to produce acceptable oxygen maps. In vivo experiments were then performed, and plots indicating camera settings necessary for producing varying qualities of oxygen maps were constructed. Trypsin digestion of retinal tissue was used in an attempt to assess any damage to experimental subjects, but this histological technique was deemed inadequate for analyzing the capillary structures of the mouse eye. Alternatively, damage was assessed using the instrument itself to calculate changes in oxygen tension during the experimental process. The results of this work will allow the phosphorescence lifetime imaging system to be used in the mouse to study how changes in retinal oxygen tension correlate with the progression of eye diseases where oxygen is implicated, including diabetic retinopathy.

# TABLE OF CONTENTS

Acknowledgements	ii
Abstract	iii
Table of Contents	iv
List of Tables and Figures	vi
1. Introduction	1
2. Background	3
Oxygen Delivery and Consumption in the Retina	3
Oxygen Measurements in the Eye	7
Imaging and Microscopy	9
Phosphorescence Lifetime Imaging of Oxygen Tension	10
3. Methods	21
Data Acquisition and Analysis	21
In Vitro Experiments	21
In Vivo Oxygen Mapping	24
Histology	27
4. Results	29
Phosphorescence Intensity	29
In Vitro Tests	31
In Vivo Tests	34
Histology	41
5. Discussion	45
Significance of Results.	45
Future Work	46
Conclusions.	48
References	50

Appendix A: Pd-Meso-Tetra (4-carboxyphenyl) Porphrine Probe Solution.  Appendix B: "Retina" Program	
Appendix C: Procedure for Trypsin Digestion of the Retina	
Appendix D: Procedure for Hematoxylin Staining of Trypsin Digests	64
Appendix E: Data Tables and Graphs	65
Appendix F: ARVO Abstract	113
Appendix G: Sigma Xi MS Research Award Executive Summary	114

# LIST OF TABLES AND FIGURES

Tal	ole	Page
3.1	Gain settings and exposure times used for in vivo experiments	26
4.1	Sample data for in vitro image set	29
4.2	Sample data for in vivo image set	29
4.3	Sample raw data for in vivo experiments	36
4.4	Summary of delta PO <sub>2</sub> mean and standard deviation for Mice 1a, 3a, and 4a	40
Fig	ure	
2.1	Cutaway view of retinal layers	4
2.2	The layered structure of the retina	5
2.3	Optical train of a microscope	9
2.4	The phosphorescence lifetime imaging system	11
2.5	Energy diagram for fluorescent and phosphorescent molecules	13
2.6	Quenching of the phosphorescent probe by oxygen	15
2.7	Maps of the mouse retina	18
2.8	Schematic diagram of the phosphorescence lifetime imaging system	19
3.1	In vitro system	22
3.2	Zero-oxygen in vitro testing system	24
3.3	Stereotaxic head holder	25
4.1	Sample intensity images and intensity vs. phase delay graph for <i>in vitro</i> experiments	30
4.2	Sample intensity images and intensity vs. phase delay graph for in vivo	31
	experiments	
4.3	Sample PO <sub>2</sub> and R <sup>2</sup> maps for <i>in vitro</i> experiments	32
4.4	In vitro calibration curve	33
4.5	Average R <sup>2</sup> value versus SNR for gain settings 10, 100, and 255	33
4.6	Sample PO <sub>2</sub> and R <sup>2</sup> maps for <i>in vivo</i> experiments	35
4.7	Sample graphs of in vivo data, taken from Mouse 7a vein	37
4 8	Map R <sup>2</sup> value versus SNR in vein, artery, and tissue for all animals tested	39

4.9 Delta PO <sub>2</sub> versus image number for Mouse 4a	40
4.10 Trypsin digestion slides of control and damaged mouse retinas	43
4.11 Trypsin digestion of the mouse retina, viewed at 4x, 10x, and 20x	44
magnification	
B.1 "Retina" front panel	57
B.2 "Show Intensity Images" screen	58
B.3 "Graph Region" screen	59
B.4 "Calculate Maps" screen	60

## 1. INTRODUCTION

Retinal hypoxia has been implicated as a causal factor in the development of numerous eye diseases, including diabetic retinopathy, retinopathy of prematurity, and glaucoma. Recently, a phosphorescence lifetime imaging technique has been developed for measuring oxygen tension in the eye that has important implications for the study retinal oxygenation in mouse models of these serious diseases. Optimizing this phosphorescence lifetime imaging technique for use in the mouse eye will allow for more complete, accurate, and useful studies of the oxygen tension in normal and diseased mouse retinas.

Phosphorescence lifetime imaging has received considerable attention in the literature as a method for measuring oxygen tension *in vivo* [Shonat, 1997]. This technique involves the injection of a phosphorescent probe into animal vasculature and the subsequent excitation of this probe with light. From its excited state, the probe phosphoresces and can be quenched by oxygen. The degree of quenching and, hence, the concentration of oxygen, can be determined by measuring the phosphorescence lifetime. When the excitation light is modulated sinusoidally, the phosphorescence is emitted at the same frequency, but with a phase delay resulting from the finite lifetime of the phosphorescence. Using a phase-sensitive detector, such as a camera's image intensifier, phase and, therefore, lifetime, can be determined. Using the intensity of phosphorescence reaching the camera at a series of intensifier phase delay values, phase shift maps can be created. When known equations are applied to each pixel in these maps, the phase shift maps can be converted to oxygen tension (PO<sub>2</sub>) maps.

Despite the recognition of this technique in the literature [Wilson, 1991 and Shonat, 1992, 1997, 1998], the specific parameters for data collection and analysis in the mouse eye have not been thoroughly investigated. The goal of this project was to examine these parameters in an effort to optimize the phosphorescence lifetime imaging technique for measuring oxygen tension in the mouse retina. The specific aims for achieving the goal of optimization were:

- 1. To calibrate the phosphorescence lifetime imaging system *in vitro* using a probe solution equilibrated at different oxygen concentrations.
- 2. To determine appropriate parameters for optimal excitation of the probe, including wavelength, bandwidth, energy, and power of the excitation light.
- To determine optimal procedures for image collection and analysis, including camera exposure time, intensifier gain, and number of images necessary for fitting.
- 4. To examine, using histological techniques, any potential microvascular damage induced by this measurement.

## 2. BACKGROUND

Phosphorescence lifetime imaging is the marriage of techniques in physiology, imaging, and microscopy. Understanding its application to the normal or diseased eye requires study of eye structure, retinal oxygenation, and the basics of imaging and microscopy. The following sections provide background in these areas, as well as an overview of phosphorescence lifetime imaging in general.

### Oxygen Delivery and Consumption in the Retina

The eye is a unique organ requiring a complex vasculature to deliver adequate oxygen for visual and neural function, while maintaining visual clarity and transparency. Oxygenation in the various parts of the eye, including the retina, reflects the distinctive demands of ocular vascularization.

The retina is located on the back surface of the eye, behind the vitreous. All vertebrate retinas have a layered structure [Dowling, 1987 and Moses, 1987] (Figures 2.1 and 2.2). Two synaptic layers, known as the outer and inner plexiform layers, are stacked between three cellular layers, termed the outer and inner nuclear layer and the ganglion cell layer [Dowling, 1987]. These layers are capped by the pigmented epithelial layer and the inner limiting membrane. The outer nuclear layer contains the cell bodies of the photoreceptors, which are sensitive to light and initiate all visual responses in the retina and the brain [Dowling, 1987 and Moses, 1987]. The inner nuclear layer contains the neuron and glial cell bodies (not shown in the figure), while the ganglion cell layer contains the ganglion cell bodies. The outer plexiform layer is the site of the synaptic reactions of photoreceptors, horizontal cells, and bipolar neurons. The inner plexiform

layer houses the synaptic interactions involving bipolar neurons, amacrine cells, and ganglion cells [Moses, 1987].

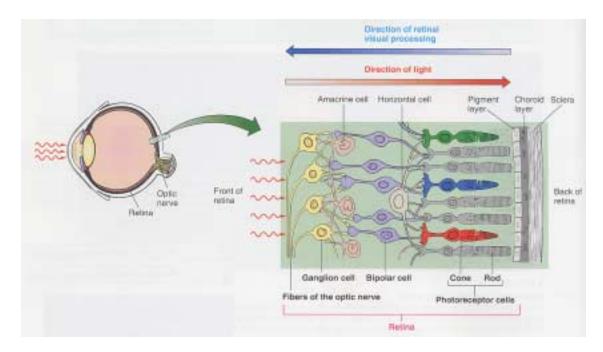


Figure 2.1-Cutaway view of retinal layers. Light enters from the front of the retina and travels through the layers to the photoreceptors. Visual information travels from the photoreceptors to the bipolar cells and the ganglion cells before traveling down the fibers of the optic nerve to the brain [Sherwood, 2001].

When light enters the eye, it passes through the retina and is captured by the photoreceptors and the outer segments of the pigment-containing cells in the pigment epithelium [Dowling, 1987]. Visual processing then occurs in the opposite direction, passing through the retina to the optic nerve at the front of the retina. The fibers of the optic nerve then transmit the visual signal to the brain.

The retina requires adequate amounts of oxygen for normal function
[Linsenmeier, 1989 and Yu, 2001]. The photoreceptors responsible for collecting light and converting it to an electrical signal contain a large concentration of mitochondria,

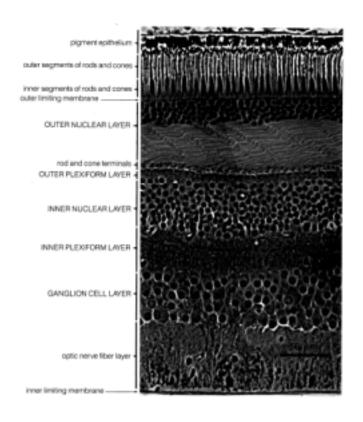


Figure 2.2—The layered structure of the retina [Dowling, 1987].

necessary for producing energy to carry out this function. This large production of energy makes the retina one of the highest oxygen consuming tissues in the body [Yu, 2001]. However, the necessity of transparency in the retina limits extensive vascularization, and the retina has only a simple vasculature radiating from the optic nerve; [Yu, 2001]. This constraint dictates that the extensive oxygen requirements of the retina be met in part by adjacent vasculatures. The avascular parts of the retina, including the photoreceptors and the outer regions, are preferentially supplied with oxygen by the choroidal vasculature, which lies behind the retina [Delori, 1988 and Yu, 2001] (Figure 2.1). This vasculature is characterized by a low vascular resistance and high blood flow rate, with an average PO<sub>2</sub> very close to arterial PO<sub>2</sub> [Linsenmeier, 1989 and 2000] and significantly greater than the PO<sub>2</sub> in the retinal vasculature.

Retinal oxygen consumption is heterogeneous through the different layers of the tissue [Yu, 1999]. Oxygen tension is relatively uniform in the inner retina, reaches a minimum within the outer retina, and rises to a maximum at the tips of the outer segments near the choroid [Linsenmeier, 1986] (Figure 2.2). In regards to oxygen consumption modeling, the avascular outer retina can be broken into three layers: layer 1, consisting of the pigment epithelium and outer segments of the photoreceptors; layer 2, consisting of the inner segments of the photoreceptors; and layer 3, consisting of the outer plexiform layer. Of these three layers, only layer 2 consumes oxygen, as oxygen-dependent mitochondria are most abundant in the inner segments of the photoreceptors [Linsenmeier, 1986 and 2000]. The oxygen consumption of the other two layers is modeled most accurately with values near zero.

The oxygen demands of the inner retina are supplied directly by the retinal circulation. The retinal circulation differs from the choroidal circulation in terms of flow rate and control mechanisms [Linsenmeier, 1986]. There exist two capillary beds in the retina, the outer bed being more venous in nature than the inner layer [Alder, 1983]. The oxygen tension is relatively low between these two beds [Yu, 1999]. The retinal circulation has no autonomic innervation, relying totally on local control mechanisms to regulate distribution of blood flow [Alder, 1997]. The capillary system in the retina is sparse to allow for minimal optical interference and, as such, has a large arteriovenous oxygen difference [Alder, 1997].

The high oxygen demands of the retina, along with its delicate supply mechanisms, make it more vulnerable to vascular deficiencies than most other organs [Yu, 2001]. Neither the retinal nor the choroidal circulation is capable of adequately

compensating for impairment to the other [Alder, 1983]. Thus, damage to either the retinal or choroidal vasculature can be devastating, often resulting in complete loss of vision [Yu, 2001]. Problems with retinal oxygen supply are often treated with panretinal photocoagulation. This technique, in which a laser is applied to broad areas of the retina, destroys photoreceptors in the peripheral retina and is thought to increase the oxygen flux from the choroid to the inner retina and thereby compensate for a decrease in retinal circulation. Less oxygen is consumed in the partially burned outer retina, allowing for increased oxygen supplied to the inner retina [Stefansson, 1981].

## Oxygen Measurements in the Eye

Many different techniques have been developed for measuring oxygen tension in the eye. However, most of these techniques have significant limitations, particularly in applications to the small mouse eye.

Oxygen-sensitive microelectrodes have been used extensively in animal models for generating oxygen profiles in the eye. While their use has offered many insights into ocular oxygenation, this method is highly invasive; the insertion of the electrode into the eye and the subsequent withdrawal of the electrode with oxygen tension measurements taken at specified points can cause significant trauma. Each introduction of the electrode offers only a one-dimensional oxygen profile for the region of insertion. Electrodes must also be recalibrated following each profile measurement. The invasive nature of the microelectrode prevents its ready application in clinical settings (due to the necessity of surgical intervention), or to mice (due to the small size of the eye) [Ito, 2001].

Retinal vessel oximetry has been used in humans to determine oxygen saturation of blood [Delori, 1988]. This technique is based on the fact that the light absorbing properties of blood (absorbance spectrum) depends on the amount of oxygen bound to hemoglobin. While the technique may be used to accurately determine oxygen tensions under ideal conditions, measurements are adversely affected by a number of factors including eye pigmentation, turbidity of ocular media, and irregular retinal topography [Delori, 1988]. It is also an indirect measure of oxygen tension.

MRI-based methods have also been used to survey oxygen characteristics of the retinal surface [Ito, 2001]. This method is unhindered by optical properties and eye size, but it requires the use of a perfluorocarbon droplet situated in the preretinal vitreous space, thus limiting its application in human subjects.

Light-based methods for exploring oxygen tensions in the eye have gained recent prominence. Some fluorescent and phosphorescent compounds (see Fig. 2.4) have been discovered to be sensitive to oxygen; when oxygen collides with a light-emitting compound in its excited state, it quenches the molecule and prevents light emission. The use of fluorescence to determine PO<sub>2</sub> is limited due to relatively low sensitivity of fluorescent molecules to oxygen [Vanderkooi, 1987]; fluorophores remain in the excited state for a relatively short period of time (nanoseconds to microseconds), and thus have limited opportunity to collide with oxygen molecules, particularly at low PO<sub>2</sub>s. Changes in turbidity of the suspending medium also affect fluorescence measurements. In contrast, phosphorescent probes are not affected by blood flow, and have relatively long lifetimes (microseconds to seconds), thereby increasing the likelihood of collision with oxygen molecules in the blood.

## **Imaging and Microscopy**

Standard research microscopes and low power objectives can be used for viewing the small mouse eye and its vasculature. Major parts of the microscope optical train include the light source, a dichromatic beam splitter (for fluorescence and phosphorescence microscopy), the objective lens, the ocular, and the camera or observer's eye (Figure 2.3). An image is produced and focused to infinity by the

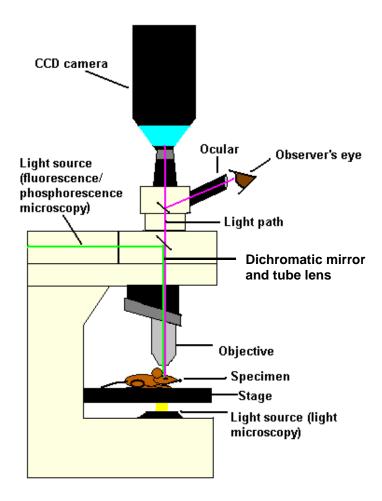


Figure 2.3-Optical train of a microscope. The specimen is illuminated by one of the light sources, and the image of the specimen travels along the optical train to the camera and/or the observer's eye.

objective lens conjugate with the specimen. A very high quality, diffraction-limited image is produced with a modern, high-numerical aperture plan-apochromatic objective

lens [Inoue, 1997]. A tube lens then focuses the image onto a target. When a charge-coupled device (CCD) camera is used, that target consists of a large array of photodiodes deposited on a silicon substrate. Each sensor element on the CCD camera is a silicon photodiode built into the silicon chip, isolated electrically from its neighbors by a channel stop [Inoue, 1997]. The image may also be projected to the eye.

## Phosphorescence Lifetime Imaging of Oxygen Tension

Phosphorescence lifetime imaging has been recognized in the literature as a technique for measuring oxygen tension in the vasculature [Wilson, 1991 and Shonat, 1992, 1997, 1998]. This technique can be applied to determine oxygen tensions in the mouse retina and in such a case is based on excitation of a phosphorescent probe and subsequent quenching of phosphorescence by intravascular oxygen. The probe is bolus-injected intravenously, and equilibrates in the bloodstream. It may then be excited by light delivered through the eye. When excited, the probe molecules phosphoresce, and are quenched when they collide with oxygen molecules. The frequency of collision and, hence, the oxygen concentration, may then be determined by computing the lifetime of the phosphorescence decay. The probe remains exclusively in the vasculature in the eye due to the blood-retinal barrier.

The phosphorescent probe generally used is palladium *meso-tetra* [4 carboxyphenyl] porphrine. This probe is sensitive to oxygen in physiological concentrations when bound to excess albumin. It is excited at 422 and 524 nm, and emits phosphorescence at 698 nm, a wavelength in the near-infrared range where the retinal tissue absorbs minimally [Shonat, 1992 and Lo, 1996].

Phosphorescence lifetime imaging requires a unique microscopic instrument (Figure 2.4). An illuminating beam is emitted by a xenon arc lamp, sinusoidally modulated using an optical chopper, and a particular wavelength ( $524 \pm 20$  nm) is selected by a monochromator. The light is then low-pass filtered and reflected down into the objective by a dichromatic mirror (pass>575 nm). This light excites phosphorescent molecules in the vasculature to their triplet states, and phosphorescence is emitted during the decay of these molecules back to the ground state. This emitted light then passes

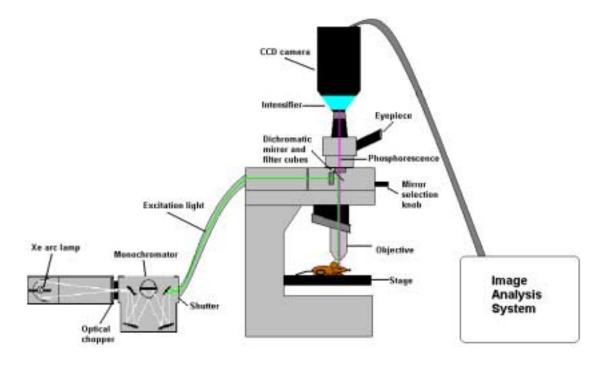


Figure 2.4-The phosphorescence lifetime imaging system. White light is emitted by the xenon arc lamp and sinusoidally modulated by the optical chopper. The monochromator selects a particular wavelength of light, which is directed to the eye by a dichromatic mirror. Phosphorescence is produced by probe in the eye, and travels to the CCD camera.

straight through the dichromatic mirror to the intensifier, which amplifies the relatively weak phosphorescent signal before transmitting it to the CCD camera. The intensifier is also used for the phase-sensitive detection of phosphorescence lifetimes, which will be

explained below. The image is then conducted to the PC-based image analysis system. This technique represents one of the few modes of microscopy in which the illuminating excitation wavelength differs from the wavelength of emitted light [Inoue, 1997]. Due to the relative weakness of the emitted light, high-sensitivity photodetectors and high light-gathering optics are required. These include objectives with high numerical aperture-to-magnification ratios and high transmission for the relevant wavelengths [Inoue, 1997]. Phosphorescence is defined as the emission of light during a transition from an excited triplet state to the ground state. The energy diagram in Figure 2.5 illustrates this phenomenon. The three singlet states (ground, first, and second) are depicted by S<sub>0</sub>, S<sub>1</sub>, and S<sub>2</sub>, respectively. In each of these states, the molecule may exist in a number of vibrational energy levels, indicated by 0, 1, 2, etc. [Lakowicz, 1999]. Photons are depicted by lightning bolts. The vertical lines represent possible transitions between states, illustrating the instantaneous nature of light absorption.

When a fluorescent or phosphorescent molecule absorbs a photon, it is excited to a higher vibrational level of S<sub>1</sub> or S<sub>2</sub>. Fluorophores then rapidly relax to the lowest vibrational level of S<sub>1</sub>, a process called internal conversion (Figure 2.4) [Lakowicz, 1999]. The molecule will then return to the ground state at any of the vibrational energy levels, quickly relaxing to the lowest level. During the decay to the ground state, the molecule emits of photon in the form of fluorescence.

Excitation to the triplet state  $(T_1)$  involves a spin conversion from the  $S_1$  state, resulting in a state with unpaired spins—a phenomenon termed intersystem crossing (Figure 2.4) [Turro, 1978 and Lakowicz, 1999]. In this excited state, the two electrons are each in a different orbital, and thus the Pauli exclusion principle does not require their

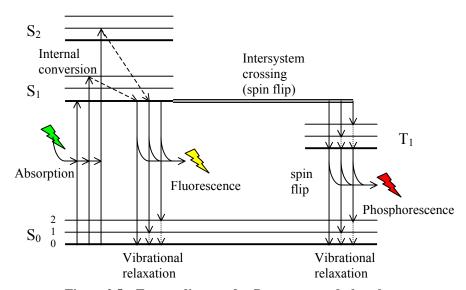


Figure 2.5—Energy diagram for fluorescent and phosphorescent molecules.  $S_0$ ,  $S_1$ , and  $S_2$ , depict ground, first, and second singlet states, respectively.  $T_1$  depicts the triplet state. Each state has representative vibrational states indicated by 0, 1, and 2. Solid vertical lines arrows represent transitions between states, dashed arrows represent vibrational relaxation within states, and lightning bolts represent photons. A molecule is excited from the ground state to any of the vibrational levels of the singlet state, and then decays to the lowest vibrational state in  $S_1$ . Fluorescent molecules will then decay down to the ground state with the emission of fluorescence, with a total reaction time on the order of ns to us. Phosphorescent molecules undergo a spin flip to the triplet state. then decay to the ground state with a spin flip and phosphorescence emission, with a total reaction time of the order of us to s. Once in the ground state, molecules will relax to the lowest energy level (0). Adapted from Lakowicz, 1999 and Vanderkooi, 1990.

spins to be paired. The energy required to produce this excited state is determined by the equation

$$\Delta E = E_2 - E_1 = hv$$

where h is Planck's constant,  $\upsilon$  is the frequency of the excitation light, and  $E_2$  and  $E_1$  are the energies of a single molecule in the initial and final states [Turro, 1978]. Like the singlet state, the triplet state is a metastable species, and will decay to the ground state after a finite time, emitting a photon in the form of phosphorescence. However, the decay from the triplet state takes a relatively long time (microseconds to seconds) when

compared with decay from the singlet state (nanoseconds to microseconds) due to the quantum mechanically forbidden spin flip completed during the decay.

When a large number of phosphorescent molecules are excited simultaneously, the resultant light emission is the sum of the individual photon emissions, and can be represented by the function:

$$I(t) = I_0 \exp(-t/\tau)$$

where I(t) is the phosphorescence intensity as a function of time (t),  $I_0$  is the initial, maximum intensity at t = 0, and  $\tau$  is the lifetime of the decay [Shonat, 1995].

In phosphorescence the excitation and emission wavelengths differ, and neither is exact; the numerous possible vibrational states create a range of wavelengths that may be absorbed or emitted, with a relative maximum wavelength resulting from conversions between the most common states. The excitation spectrum for palladium *meso-tetra* [4-carboxyphenyl] porphrine, the phosphorescent probe used in this study, has maxima at 420 and 524 nm. Due to the absorption of excitation light by blood, the volume of excitation, defined as the excitation area times the penetration depth, is ten times smaller at 420 nm than at 524, and the total quantity of probe excited is reduced [Shonat, 1995]. The emission is maximal at 687 nm, regardless of what wavelength is used for excitation; decay always occurs from the lowest vibrational level of the triplet state resulting in a consistent emission spectrum [Lo, 1996 and Vanderkooi, 1990].

When the phosphorescent probe is excited by light that has been sinusoidally modulated, the phosphorescence emitted will have the same frequency, but will have lower amplitude and be delayed in phase by an angle  $\theta$ .  $\theta$  is related to the probe lifetime,  $\tau$ , by the following equation:

$$\tan \theta = \omega \tau$$

where  $\omega$  is the excitation frequency [Shonat, 1997].

A phosphorescent molecule that has been excited to the triplet state may transfer its energy to another molecule without light emission, a phenomenon termed *quenching* (Figure 2.6). Such interactions between phosphors and their environment are common; the spin-forbidden transition from the triplet state to the ground has a relatively long lifetime, and increases the probability of contact between molecules [Vanderkooi, 1990].

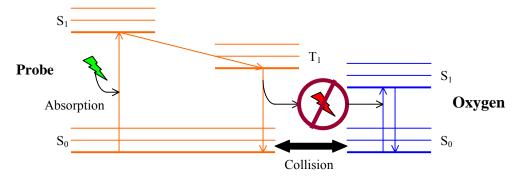


Figure 2.5—Quenching of the phosphorescent probe by oxygen. 6When the two molecules collide, the decaying probe gives its energy to oxygen instead of giving it off as phosphorescence. This results in a singlet oxygen molecule, which decays to the ground state within microseconds.

In blood, the only significant quenching agent is oxygen [Wilson, 1991]. The degree of quenching of the phosphorescent molecule depends on the concentration of oxygen in its vicinity [Shonat, 1992]. The efficiency of phosphorescence quenching is governed by the frequency of collision between the excited triplet state molecule and the quencher before the phosphor returns to the ground state. This relationship is represented by the Stern-Volmer equation:

$$\tau_o \, / \, \tau = 1 + k_Q \tau_0 [\mathrm{PO}_2]$$

where  $\tau_0$  is the lifetime in the absence of oxygen,  $k_Q$  is the bimolecular rate constant (or quenching constant), and [PO<sub>2</sub>] is the oxygen concentration [Vanderkooi, 1987, Shonat, 1995 and 1997, and Lo, 1996]. In a zero oxygen environment,  $\tau = \tau_0$  and the lifetime is a maximum.

Quenching reactions form excited singlet oxygen (Figure 2.5), which may react with unsaturated double bonds in lipids to form peroxides. These peroxides destructively alter amino acids and nucleic acids. However, destruction of biological tissue by these reactions is mitigated by the fact that singlet oxygen decays to the ground state within microseconds, and any chemical reactions must occur by collision with the singlet-state molecule before it decays [Vanderkooi, 1987]. However, the potential for vascular damage must always be considered when using these probes for *in vivo* applications.

Palladium meso-tetra porphrine must be mixed with excess albumin prior to injection for phosphorescence quenching studies. This complex has several properties essential to accurate phosphorescence lifetime imaging: the sensitivity to quenching of albumin-bound probe by oxygen is independent of the suspending medium or probe concentration in solution, self-quenching of the probe is eliminated, and the sensitivity to oxygen is increased since the binding to albumin decreases  $k_Q$  [Vanderkooi, 1987 and Shonat, 1995]. As long as albumin is present in excess of the probe, the probe/albumin complex may be suspended in saline and injected directly into the femoral vein, and will show no decrease in phosphorescence intensity over several hours [Wilson, 1991].

Calibration of the probe for determining oxygen concentration in the vasculature is absolute—calibration depends only on the phosphor and its molecular environment,

which remain constant for such experiments [Lo, 1996]. Once  $\tau_0$  and  $k_Q$  are known ex vivo, they apply  $in\ vivo$  and recalibration is not necessary [Vanderkooi, 1987].

From phosphorescence lifetime,  $PO_2$  can be calculated. A phase-sensitive measure of this phosphorescence lifetime is possible when the delivered excitation light and the sensitivity of the collection system (intensifier) can be independently modulated and the phase relationship between these two elements can be accurately varied [Shonat, 1997]. Intensity images may then be taken with increasing intensifier phase delays relative to excitation phase, and a graph of intensity versus phase delay constructed. This graph may be used in conjunction with the following equation to determine the phosphorescence phase delay,  $\theta$ :

$$I(\theta_D) = k[Pd]\{1+ m_D m cos(\theta - \theta_D)\}$$

where  $I(\theta_D)$  is the intensity as a function of known phase delay, k is a constant, [Pd] is the probe concentration,  $\theta_D$  is the phase delay of the intensifier sensitivity,  $m_D$  is the modulation of the emission, and

$$m = (1 + \omega^2 \tau^2)^{-1/2}$$
.

However, since this equation is nonlinear, applying it to each pixel in an image is computationally difficult. A linearized form of the equation was developed by Lakowicz [1992] by applying the trigonometric identity for subtraction of cosine terms and combining the fitting parameters into linear coefficients:

$$I(\theta_D) = a_0 + a_1 \cos \theta_D + b_1 \sin \theta_D$$

where a fit to the equation can be determined by the evaluation of  $a_0$ ,  $a_1$ , and  $b_1$  using linear regression.  $\theta$  is then determined as:

$$\tan^{-1}(b_1/a_1)$$

and may be used to determine  $\tau$  for each pixel. This value of  $\tau$  is used in the Stern-Volmer equation to calculate PO<sub>2</sub> maps (Figure 2.7).

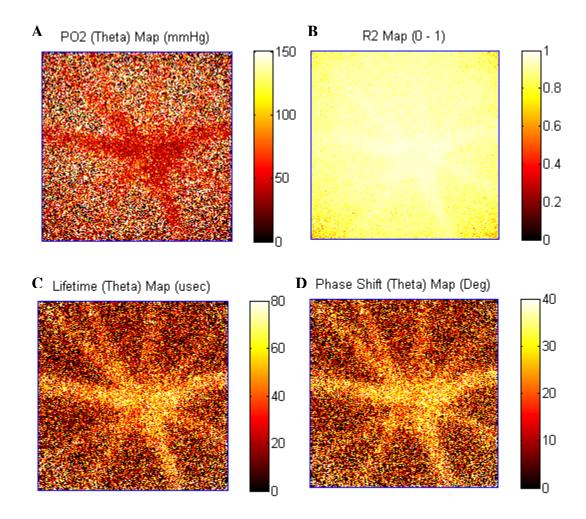


Figure 2.7—Maps of the mouse retina. The  $PO_2$  map (A) is created using the Stern-Volmer equation. The parameters for the equation are calculated by fitting a series of intensity images to a linear equation  $(B \text{ shows the } R^2 \text{ for this fit in every pixel})$ , which is used to determine phase shift (D). Phase shift is then used to calculate lifetime (C).

Certain hardware and software elements and an electronic interface are required for the generation of PO<sub>2</sub> maps (Figure 2.8). The program used for data collection,

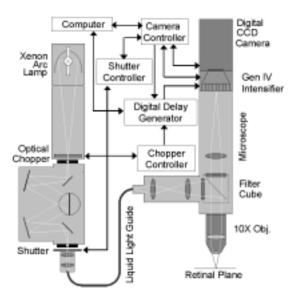


Figure 2.8—Schematic diagram of the phosphorescence lifetime imaging system.

WinViewNT (Roper Scientific, Trenton, NJ), allows for control of the digital delay generator (Stanford Research Systems, Sunnyvale, CA) and the camera and its intensifier (Roper Scientific, Trenton, NJ). The delay generator sets the phase delay of the intensifier relative to the optical chopper. The optical chopper controller (Photon Technology, Brunswick, NJ) rotates the chopper disc at 1.6 kHz, and sinusoidally modulates the light produced by the Xenon arc lamp. The light passes through a monochromator (Photon Technology), which selects the wavelength used for excitation (524±20 nm). A shutter (Vincent Associates, Rochester, NY), which is directly connected to the camera control mechanism, operates in parallel with the camera, opening only during camera exposure and blocking the excitation light when the camera shutter is closed. The light passes through a focusing lens and an interference filter, is reflected off a dichromatic mirror, and is concentrated by an infinity-corrected objective to reach the retinal plane [Shonat, 1992 and 1995]. Light emitted from the eye is collected by the objective and sent to the dichromatic mirror, where wavelengths longer

than the cut-off wavelength of 630 nm pass through to the intensifier to the CCD camera [Shonat, 1992]. The camera delivers each image to the WinViewNT program, where the entire series may be stored as a single binary data file.

Advantages of phosphorescence lifetime imaging of oxygen tension are numerous. Recalibration of the probe is not required. The response time is very short, and signal acquisition and calculation are rapid. Data analysis is also relatively simple, since the dependence of phosphorescence lifetime on oxygen pressure follows a well-defined physical relationship, which can be expressed with simple equations [Lo, 1996].

Difficulties with the phosphorescence lifetime imaging technique mainly involve the possible effects of the excitation on the tissue. The excitation of the phosphorescent probe within the blood vessels of the eye and subsequent quenching by oxygen creates oxygen free radicals, which are toxic to the vessels and tissue. Extensive excitation of the probe decreases the amount of oxygen available to the eye, and can cause significant damage. To limit tissue damage, the concentration of the probe and the duration of exposure to excitation light should be kept to a minimum [Shonat, 1995].

To utilize the phosphorescence lifetime imaging system to its fullest potential, the existing structure was calibrated using an *in vitro* system to ensure that oxygen maps report accurate PO<sub>2</sub> values. Acquisition parameters, including camera exposure time, intensifier settings, power of excitation light, and number of images necessary for determining phase shift were determined for *in vivo* experiments. Histological techniques were used in an attempt to assess any microvascular damage induced by the measurement.

## 3. METHODS

Despite its potential usefulness in the characterization of oxygen tensions in diabetic retinopathy and other oxygen-related eye diseases, the specific parameters for phosphorescence lifetime imaging in the mouse eye have not yet been determined. The primary goal of this project was to determine these parameters. To this end, *in vitro* and *in vivo* experiments were conducted, and appropriate gains, exposure times, and other imaging considerations were examined.

## Data Acquisition and Analysis

Phosphorescence intensity images were collected using the WinViewNT software package (see Background). For each data set, a series of 15 to 30 images was taken at increasing phase delays, and stored as a single binary data file. Data analysis for all *in vitro* and *in vivo* experiments was done using Microsoft Excel, SigmaPlot, and a program in MatLab called "Retina," developed by Ross Shonat (see Appendix B).

Three experiments at each gain and exposure time were performed. Map  $R^2$  values, indicating the fit to the equation  $I(\theta_D) = a_0 + a_1 \cos\theta_D + b_1 \sin\theta_D$ , were used as an indication of the quality of the oxygen maps.  $PO_2$  means and standard deviations for specified regions were calculated using the "Retina" program.

## In Vitro Experiments

An *in vitro* system was constructed to calibrate the phosphorescence lifetime imaging system and to determine approximate gain settings and exposure times required to produce acceptable oxygen maps. The system, pictured in Figure 3.1, included a



Figure 3.1—In vitro system. The system consists of an oxygenator connected to a gas mixer, a peristaltic pump used for circulating probe solution inside the system, and a square glass capillary tube situated under the microscope objective used for measuring the  $PO_2$  of the solution. The parts are connected with Tygon® microbore tubing, which may be disconnected at various junctions and injected with solution using a 22-gauge needle and syringe.

length of Tygon® tubing, into which a probe solution, consisting of 12 ml albumin stock solution, 148 mg NaCl, 216 mg glucose, and 10 µl probe was injected. A peristaltic pump was used to circulate the fluid through the system. The phosphorescent solution flowed through an oxygenator (consisting of a length of plastic tubing, inlaid with a Plexiglas rod wrapped with oxygen-permeable silastic tubing, and capped at each end by a rubber stopper with an inlet connector for the gas mixer and an outlet for exhaust), used to apply gas mixtures with known oxygen concentrations. Upon leaving the oxygenator,

the solution flowed through a square glass capillary tube situated under the phosphorescence lifetime imaging system. The phosphorescence lifetime was then measured as previously described, and a  $PO_2$  map was generated. The correspondence between the  $PO_2$  values indicated by the map and those applied using the gas mixer and oxygenator was used to calibrate the system to provide accurate measures of  $PO_2$  within the vasculature.

Signal-to-noise ratios (SNR) were used to determine appropriate gain settings and exposure times. The probe was equilibrated at a physiological oxygen concentration of 40 mm Hg (5% oxygen applied using the gas mixer and oxygenator). Exposure times were tested at random in an attempt to achieve a maximal range of SNR for camera intensifier gain settings 10, 100, and 255. Exposure times yielding SNR of approximately 2 and approximately 225 were noted for each gain. Phosphorescence lifetime images were then taken at a range of ten exposure times equally spaced between the time yielding SNR  $\approx$  2 and the time yielding SNR  $\approx$  225.  $R^2$  maps, which demonstrate the integrity of the fit between the phosphorescence intensity data and the equation  $I(\theta_D) = a_0 + a_1 \cos\theta_D + b_1 \sin\theta_D$ , were then created. From these maps, the average  $R^2$  value for the entire capillary tube was determined. These values were plotted versus SNR for each gain setting

The *in vitro* system was also used to calibrate the phosphorescence lifetime imaging system against known oxygen concentrations. Oxygen concentrations in the physiological range of zero to 100 mm Hg were tested. To obtain concentrations in this range, the oxygenator was used to apply gas mixtures between one and 12 percent  $O_2$  balanced with  $N_2$ . A zero oxygen environment was obtained by adding probe solution

and a pinch of glucose oxidase to a closed cuvette to prevent leakage of environmental oxygen into the system (Figure 3.2). At each oxygen concentration, ten image sets were taken at each of four gain settings (100, 70, 40 and 10). Exposure times were 0.23, 0.47, 0.83, and 1.0 seconds, respectively, and were selected based on the fact that they yield SNRs between 3 and 15. After each exposure, the objective was blocked with white paper to produce intensity images with a theoretical phase delay of zero and a modulation of one (reflected images). These data were used to determine the intrinsic phase delay and modulation of the instrument.

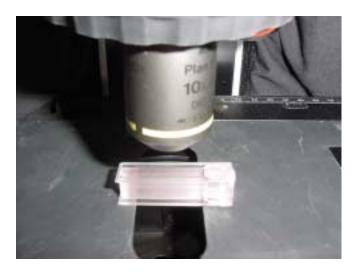


Figure 3.2—Zero-oxygen *in vitro* testing system. Cuvette is filled with glucose-containing probe solution, to which glucose oxidase is added to remove all oxygen.

## In Vivo Oxygen Mapping

All animal experiments were performed in accordance with WPI's Institutional Animal Care and Use Committee (IACUC) protocols and the Association for Research in Vision and Ophthalmology statement for the Use of Animals in Ophthalmic and Vision Research. Mice were anesthetized prior to all experiments with a solution of 125 µl

Avertin and 4.875 ml saline, in the amount of 0.25 ml/10 g body weight (adjusted as needed). When fully anesthetized, one eye per mouse was dilated with Mydriacyl (1%). Mice were fixed in a stereotaxic head holder (Figure 3.3) to prevent movement and assist placement during experimentation. A drop of Goniosoft ophthalmic ointment was placed on the dilated eye, and a small piece of microscope coverglass was situated on top of the layer of Goniosoft to negate the refractive power of the cornea.

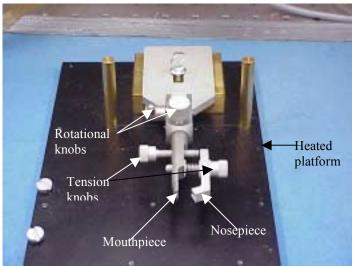


Figure 3.3—Stereotaxic head holder. Mouse rests on a heated platform, designed to maintain body heat while animal is under anesthesia. The mouthpiece is inserted into the animal's mouth, and the nosepiece is tightened onto the nose with the tension knobs. The rotational knobs are loosened to allow proper positioning of the head so the eye may be viewed, and tightened to prevent movement once the proper position is achieved.

Probe solution was introduced through the femoral vein by venous puncture. A small patch of skin was removed above the vessel, and a solution of 10 mg/ml Pd *mesotetra* [4-carboxyphenyl] porphrine in bovine serum albumin was bolus injected in the amount of 10 mg/kg body weight<sup>1</sup>. Following injection, the vein was cauterized to

<sup>&</sup>lt;sup>1</sup> Dosages of 5 mg/kg and 15 mg/kg were also tested; however, the lower dose yielded relatively faint intensity images, while the higher dose resulted in damage to the retinal vessels with relatively little light exposure.

prevent bleeding. The mouse was then placed under a dissecting microscope, and the position of the head was adjusted such that the retinal blood vessels radiating from the optic nerve were visible. Power density of the excitation light (mJ/cm<sup>2</sup>) was measured prior to data collection using a photodetector and power/energy meter (Newport Corporation, Irvine, CA).

Eight mice, labeled 1a-8a, were prepared and tested at gains 10, 40, 70, and 100, as determined by the *in vitro* experiments. Exposure times were selected based on preliminary *in vivo* tests; times yielding signal-to noise ratios between 3 and 15 without exceeding 1.0 second were used (Table 3.1). Fifteen images per set, determined during *in vitro* experiments to be adequate, were taken beginning with an intensifier delay of 5 μs and continuing at 20 μs increments. Experiments were performed in triplicate for each gain and exposure time setting. The sequence of data collection was varied in each mouse (see Appendix E).

Gain	Exposure Times (seconds)
100	0.6, 0.145, 0.23, 0.315, 0.4
70	0.15, 0.31, 0.47, 0.63, 0.79
40	0.32, 0.49, 0.66, 0.83, 1.0
10	0.4, 0.55, 0.7, 0.85, 1.0

Table 3.1—Gain settings and exposure times used for *in vivo* experiments.

Regions of interest in a vein, an artery, and a section of tissue were then selected for each mouse. The "Retina" program (Appendix B) was used to analyze these different and distinct regions. A maximum  $PO_2$  of 150 was used in the analysis, and all pixels exceeding this value were rejected as physiologically impossible. The following parameters were noted for each region:

- Fitting parameters a<sub>0</sub>, a<sub>1</sub>, and b<sub>1</sub>
- Phase shift (θ)
- Modulation (m)
- PO<sub>2</sub> mean and standard deviation
- R<sup>2</sup> mean and standard deviation
- Number of pixels in the selected region of interest
- Number of pixels from the selected region of interest used for calculations

  Signal-to-noise was calculated as a<sub>0</sub> (the DC fitting term) divided by the average intensity

  with the microscope objective's shutter closed (camera dark noise). Accumulated energy

  deposition at each point in the experiment was calculated as excitation light power

  (measured with a power/energy meter) divided by excitation light area multiplied by

  cumulative exposure time. The analysis was then repeated using a smaller number of the

  images (7), beginning with the first and continuing with every other image in each set to

  maintain uniform phase delay increments.

## **Histology**

Histology was used as a potential method for determining any damage to the mouse eye incurred during phosphorescence lifetime imaging, and, potentially, as a method for correlating physical damage caused by disease with the PO<sub>2</sub> maps. No standard technique for conducting histology on the mouse retina exists, so the assistance of Dr. Robert Frank of the Kresge Eye Institute, Wayne State University, Detroit, MI, was sought. His expertise in performing trypsin digestion and periodic acid solution (PAS)/hematoxylin staining on rat retinas was well known, and personal communication with him and personnel in his lab indicated that this technique could be successfully

applied to the mouse retina. A visit to his lab allowed the intricacies of the technique to be learned, and a protocol for conducting trypsin digestion and PAS/Hematoxylin staining on the mouse retina was developed (see Appendices C and D).

To induce damage following *in vivo* calibration experiments, probe-injected (10 mg/kg) mice were exposed continuously to 524 nm excitation light for an extended period of time on a single eye. Following continuous exposure for an hour, mice were removed to a dissecting microscope. Complete retinal vascular damage was confirmed by the absence of blood flow in retinal vessels (vessels appearing white in color, rather than the normal red). Eyes were removed and retinas were digested and stained, with the non-exposed eye serving as a control.

# 4. RESULTS

# Phosphorescence Intensity

Phosphorescence intensity images were acquired, and graphs of intensity vs. phase delay created for each *in vitro* and *in vivo* experiment. Sample data appears in Tables 4.1 and 4.2, and sample images and curves appear in Figures 4.1 and 4.2.

Image	Phase Delay	Intensity	Intensity
Number	(Radians)	Average	Standard Dev.
2	14.4	941	213
3	25.9	975	222
4	37.4	987	224
5	49.0	985	224
6	60.5	980	224
7	72.0	950	218
8	83.5	923	212
9	95.0	886	203
10	106.6	840	194
11	118.1	788	184
12	129.6	719	170
13	141.1	665	159
14	152.6	604	146
15	164.2	549	134

Table 4.1—Sample data for in vitro image set.

Image	Phase Delay	Artery Intensity	Artery Intensity St. Dev.	Vein Intensity	Vein Intensity	Tissue Intensity	Tissue Intensity
Number	(Radians)	Average		Average	St. Dev.	Average	St.Dev.
2	14.4	655	30	1150	114	372	32
3	25.9	654	41	1164	121	370	28
4	37.4	640	31	1165	119	357	29
5	49.0	619	35	1135	112	342	31
6	60.5	594	29	1106	109	323	28
7	72.0	564	30	1052	105	302	267
8	83.5	532	27	1008	102	279	24
9	95.0	482	30	936	98	254	22
10	106.6	444	29	878	94	228	20
11	118.1	403	24	810	82	202	20
12	129.6	353	22	730	80	178	16
13	141.1	325	24	655	73	155	16
14	152.6	275	16	589	63	134	13
15	164.2	248	19	522	57	118	12

Table 4.2—Sample data for in vivo image set.

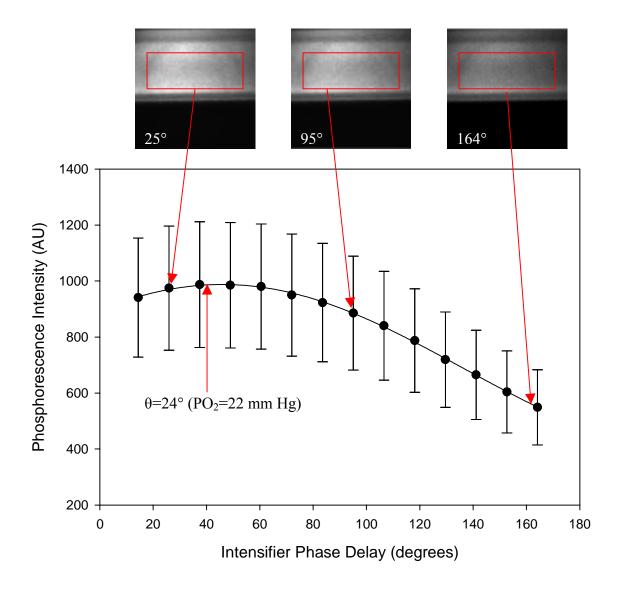


Figure 4.1—Sample intensity images and intensity vs. phase delay graph for *in vitro* experiments. Intensity images corresponding to phase delays of  $25^{\circ}$ ,  $95^{\circ}$ ,  $25^{\circ}$ , and  $164^{\circ}$ , are shown. The region of interest used for intensity averaging is indicated by the red line in each image. The maximum value on the graph, corresponding to the phase delay, and used to calculate  $PO_2$ , is also indicated.

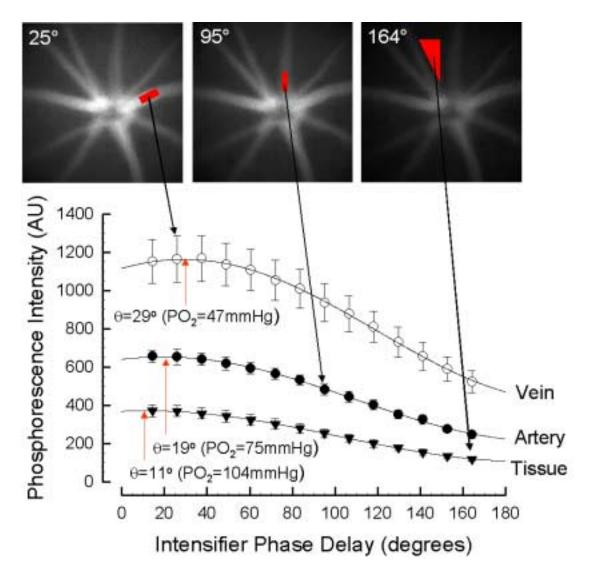


Figure 4.2—Sample intensity images and intensity vs. phase delay graph for *in vivo* experiments. Intensity images corresponding to phase delays of  $25^{\circ}$ ,  $95^{\circ}$ ,  $25^{\circ}$ , and  $164^{\circ}$ , are shown. The region of interest used for intensity averaging is indicated by the red region in each image—vein, artery, and tissue were selected for each animal tested. The maximum value on the graph, corresponding to the phase delay, and used to calculate  $PO_2$ , is also indicated.

#### In Vitro Tests

The phosphorescence lifetime imaging system was calibrated using the *in vitro* testing system, described in the methods section. Early experiments identified a drift in the optical chopper phase, which was rectified with a change in hardware. Experiments

with a blocked objective and no phosphorescence verified that the instrument did not produce significantly different results at different gains, exposure times, or total experiment times. However, an intrinsic phase error of 0.80 and modulation error of 0.67 were discovered. The phase error was subtracted from all subsequent data sets, and the modulation error was divided. Following this correction, PO<sub>2</sub> and R<sup>2</sup> maps (where R<sup>2</sup> is a measure of the fit of the intensity images to the specified equation) were created for each image set, a sample of which appears Figure 4.3, and a final calibration curve was generated (Figure 4.4).

To determine if map fit was affected by intensity signal-to-noise ratio, average  $R^2$  value for the capillary tube was plotted versus SNR (with SNR calculated as the average intensity of images taken at a series of 30 delay settings between 10 and 300  $\mu$ s divided by the average intensity of images taken with no light entering the camera). The results appear in Figure 4.5.

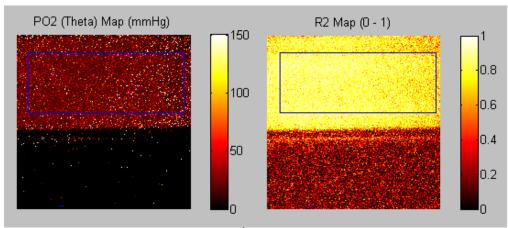


Figure 4.3—Sample PO<sub>2</sub> and R<sup>2</sup> maps for *in vitro* experiments. Regions of interest selected for data analysis in the "Retina" program are delimited by the blue lines.

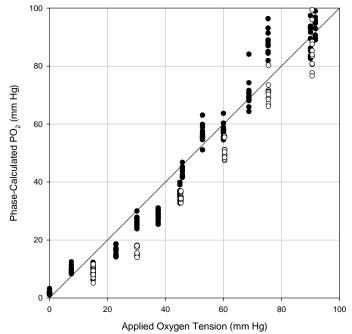


Figure 4.4—In vitro calibration curve. The x-axis represents oxygen concentrations applied with the gas mixer. The y-axis indicated  $PO_2$  as determined by the phosphorescence lifetime imaging system. A line of identity intersects the data, indicating that the system produced accurate  $PO_2$  maps.

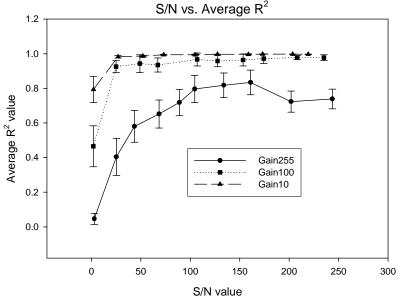


Figure 4.5—Average  $R^2$  value versus SNR for gain settings 10, 100, and 255. Gain 255 gave less than acceptable  $R^2$  values regardless of signal-to noise ratio. Gains 10 and 100 yielded very high  $R^2$  values at SNR>50.

These data indicate that a gain setting of 255 did not produce images with acceptable  $R^2$  values (>0.9), even at high signal-to-noise ratios. In contrast,  $R^2$  values of greater than 0.9 were obtained with gain settings 10 and 100 for all SNR > 50. These results were verified in subsequent experiments (data not shown). As a result, all subsequent experiments were conducted at gain settings between 10 and 100. Since the data indicated that all SNR>50 yield similarly high  $R^2$  values, exposure times resulting in signal-to-noise ratios of 50 or less were used, thereby minimizing excitation light exposure.

### In Vivo Tests

For all image sets with 15 images each, a vein, an artery, and a section of tissue were analyzed (Figure 4.6). In general, PO<sub>2</sub> was highest in the tissue region, and lowest in the veins. For each of these regions, graphs were created for R<sup>2</sup> vs. SNR, PO<sub>2</sub> vs. accumulated energy deposition, and PO<sub>2</sub> vs. SNR. The raw data for each animal appear in Appendix E, and sample data and graphs for a single mouse (Mouse 1a) are shown in Table 4.3 and Figure 4.7. Figure 4.8 contains summary plots of R<sup>2</sup> vs. signal-to-noise ratio for the three regions in all mice. Each data point represents an individual image set.

For all regions, lower gains produced better fits at lower signal-to-noise ratios. All gain settings yielded R<sup>2</sup> values of approximately 0.95, but a gain setting of 100 requires an SNR of greater than 10 to produce this good fit. Conversely, a gain setting of 10 requires an SNR of only 4 to produce an excellent fit. However, it must be considered that achieving an SNR 4 at gain 10 requires an exposure time of 1.0 seconds, while achieving an SNR of 10 at gain 100 requires an exposure time of only 0.4 seconds.

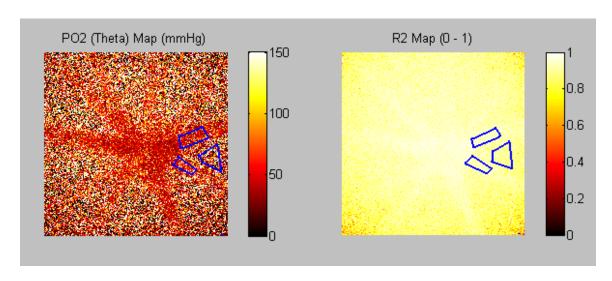
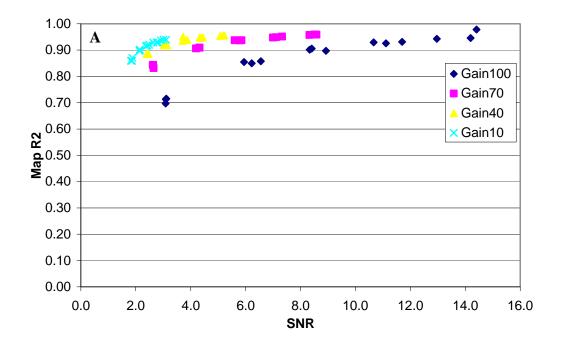


Figure 4.6—Sample  $PO_2$  and  $R^2$  maps for *in vivo* experiments. Regions of interest for vein (top), artery (bottom) and tissue (center) are indicated by the blue lines.

				Accumulated					
	_	Relative		Energy					
	Exposure	Image	Image	Deposition	01.15	PO2	PO2 St.	R2	R2 St.
Gain	Time	Number	Number	(mJ/cm^2)	SNR	Mean	Dev	Mean	Dev
100	0.06	1	1	4.5	3.1	31.3	25.5	0.71	0.11
100	0.06	2	2	9.1	3.1	33.2	24.6	0.70	0.12
100	0.06	3	3	13.6	3.1	39.4	29.7	0.72	0.11
100	0.145	1	4	24.6	6.6	37.3	22.3	0.86	0.06
100	0.145	2	5	35.6	6.2	38.1	23.5	0.85	0.06
100	0.145	3	6	46.6	5.9	35.2	20.7	0.85	0.06
100	0.23	1	7	64.1	8.9	40.2	22.2	0.90	0.04
100	0.23	2	8	81.5	8.4	39.4	21.6	0.91	0.04
100	0.23	3	9	99.0	8.3	37.7	19.5	0.90	0.04
100	0.315	1	10	122.8	11.7	36.4	16.2	0.93	0.03
100	0.315	2	11	146.7	11.1	40.4	20.7	0.93	0.03
100	0.315	3	12	170.6	10.7	43.4	19.4	0.93	0.03
100	0.4	1	13	200.9	14.4	37.0	14.1	0.98	0.03
100	0.4	2	14	231.3	14.2	37.1	14.4	0.95	0.02
100	0.4	3	15	261.6	13.0	39.7	17.0	0.94	0.02
70	0.15	1	16	273.0	2.7	47.8	30.2	0.83	0.07
70	0.15	2	17	284.4	2.6	44.2	28.1	0.84	0.07
70	0.15	3	18	295.7	2.6	39.0	25.3	0.84	0.07
70	0.31	1	19	319.2	4.3	41.2	20.9	0.91	0.04
70	0.31	2	20	342.7	4.2	43.5	22.8	0.91	0.04
70	0.31	3	21	366.2	4.3	41.4	22.2	0.91	0.04
70	0.47	1	22	401.9	5.8	41.7	18.6	0.94	0.03
70	0.47	2	23	437.5	5.6	43.4	19.4	0.94	0.03
70	0.47	3	24	473.2	5.8	43.6	20.2	0.94	0.03

70	0.63	1	25	520.9	7.1	44.5	17.8	0.95	0.02
70	0.63	2	26	568.7	7.0	46.1	20.9	0.95	0.02
70	0.63	3	27	616.5	7.3	47.8	19.1	0.95	0.02
70	0.79	1	28	676.4	8.5	46.4	18.0	0.96	0.02
70	0.79	2	29	736.3	8.3	46.9	20.6	0.96	0.02
70	0.79	3	30	796.2	8.6	41.7	15.2	0.96	0.02
40	0.32	1	31	820.4	2.4	42.1	24.5	0.88	0.05
40	0.32	2	32	844.7	2.5	44.2	26.1	0.89	0.05
40	0.32	3	33	869.0	2.4	47.2	26.5	0.89	0.05
40	0.49	1	34	906.1	3.1	41.2	20.9	0.92	0.04
40	0.49	2	35	943.3	3.1	46.8	24.3	0.92	0.03
40	0.49	3	36	980.4	3.0	48.4	25.6	0.92	0.04
40	0.66	1	37	1030.5	3.7	45.5	22.2	0.95	0.03
40	0.66	2	38	1080.5	3.9	43.4	18.8	0.94	0.03
40	0.66	3	39	1130.6	3.7	45.9	20.9	0.94	0.03
40	0.83	1	40	1193.5	4.3	48.0	20.9	0.95	0.02
40	0.83	2	41	1256.4	4.4	44.8	21.1	0.95	0.02
40	0.83	3	42	1319.4	4.4	45.3	19.3	0.95	0.02
40	1	1	43	1395.2	5.2	45.1	18.3	0.96	0.02
40	1	2	44	1471.0	5.1	42.4	16.3	0.95	0.02
40	1	3	45	1546.9	5.2	44.0	18.1	0.96	0.02
10	0.4	1	46	1577.2	1.8	42.3	24.6	0.86	0.06
10	0.4	2	47	1607.5	1.9	44.6	26.7	0.87	0.05
10	0.4	3	48	1637.9	1.9	45.6	27.3	0.86	0.06
10	0.55	1	49	1679.6	2.1	43.8	22.8	0.90	0.04
10	0.55	2	50	1721.3	2.1	38.2	19.7	0.90	0.04
10	0.55	3	51	1763.0	2.1	42.9	23.9	0.90	0.04
10	0.7	1	52	1816.1	2.4	42.3	21.3	0.91	0.04
10	0.7	2	53	1869.1	2.5	40.6	21.4	0.92	0.03
10	0.7	3	54	1922.2	2.4	44.4	21.3	0.92	0.04
10	0.85	1	55	1986.7	2.6	43.8	21.1	0.93	0.03
10	0.85	2	56	2051.1	2.8	41.7	19.7	0.93	0.03
10	0.85	3	57	2115.6	2.8	43.3	20.2	0.93	0.03
10	1	1	58	2191.4	3.0	43.5	20.2	0.94	0.03
10	1	2	59	2267.2	3.1	45.1	19.5	0.94	0.03
10	1	3	60	2343.0	2.9	46.1	20.9	0.94	0.03

Table 4.3—Sample raw data for in vivo experiments, from Mouse 1a vein. Data were calculated from  $PO_2$  and  $R^2$  maps and intensity images using the "Retina" program.



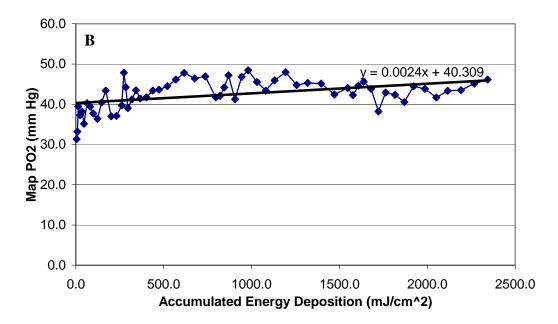
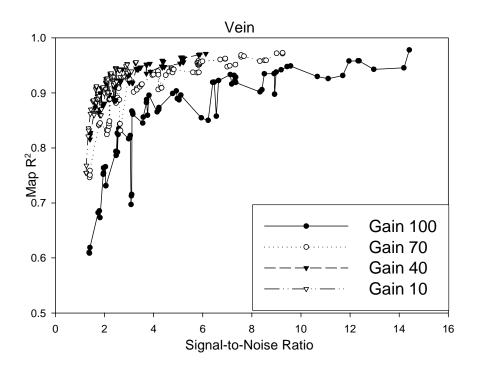
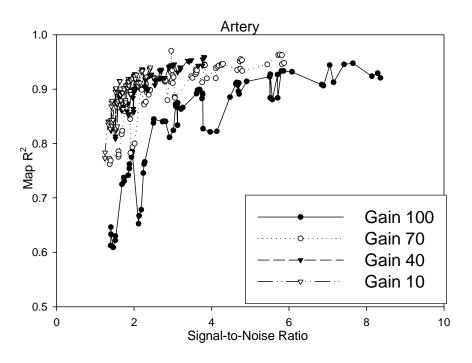


Figure 4.7—Sample graphs of *in vivo* data, taken from Mouse 1a vein. Panel A represents a typical graph of  $R^2$  value vs. SNR, where  $R^2$  value increases slightly with increasing SNR. Panel B shows a typical map  $PO_2$  vs. accumulated energy deposition graph, where the slope of the trendline is not statistically different from zero in the negative direction (one-tailed Student's t-test, p>0.05).





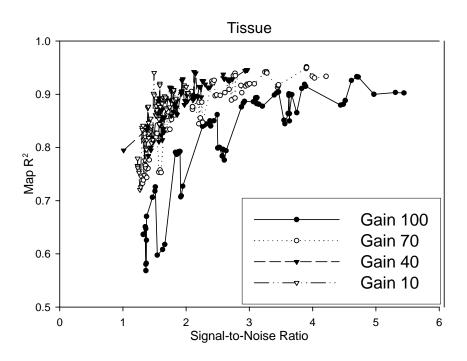


Figure 4.8—Map  $R^2$  value versus SNR in vein, artery, and tissue for all animals tested. Each point represents an individual image set and  $R^2$  map.

Composite graphs of PO<sub>2</sub> vs. accumulated energy deposition and vs. signal-to-noise were not created, as differences in oxygen tensions in individual mice made such general comparisons inappropriate. However, graphs of these parameters for individual mice appear in Appendix E. For all animals, the slope of the linear best-fit lines on these plots is not significantly different from zero in the negative direction (one-tailed Student's t-test, p>0.05), indicating that PO<sub>2</sub> was not affected by increasing energy deposition or SNR.

Results of analysis of image sets with seven images were compared to those obtained with 15 images to determine if fewer images (which would result in decreased light exposure and less possible physiological damage) could produce accurate maps. A parameter termed "Delta PO<sub>2</sub>," defined as the PO<sub>2</sub> calculated with 15 images minus that

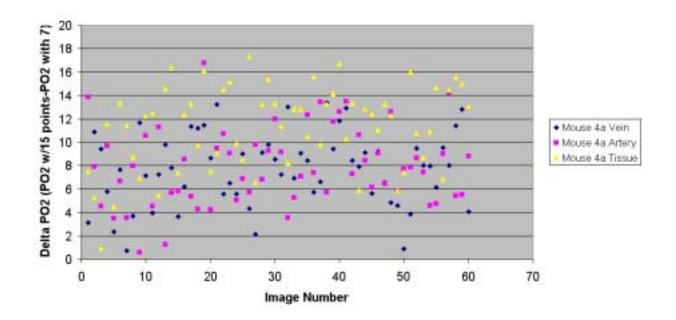


Figure 4.9—Delta  $PO_2$  versus image number for Mouse 4a.  $PO_2$  differs by as much as 17 mm Hg when calculated with the fewer number of images, indicating that seven images are too few for calculating  $PO_2$  accurately.

Mouse	Vessel	Average Delta PO2	Delta PO2 St.Dev.
1	Vein	-0.6	3
1	Artery	2.1	3.9
1	Tissue	5.7	3.3
3	Vein	3.7	2.8
3	Artery	7.1	2.5
3	Tissue	9.8	1.8
4	Vein	7.7	3.1
4	Artery	7.9	3.3
4	Tissue	11.3	3.6

Table 4.4—Summary of delta  $PO_2$  mean and standard deviation for Mice 1a, 3a, and 4a. Delta  $PO_2$  is significantly different from zero in most cases, indicating that the use of seven images does not produce accurate  $PO_2$  values.

calculated with seven, was used to examine possible error incurred using fewer images. Sample results appear in Figure 4.9 and Table 4.4. PO<sub>2</sub> differed significantly when

calculated with seven images in some cases, indicating that seven images is too few for calculating accurate PO<sub>2</sub> values.

## Histology

Trypsin digestion and PAS/Hematoxylin staining (see Appendices C and D) were performed on mouse eyes visibly damaged by light exposure, and on unexposed control eyes from the same mouse. No apparent differences were observed between the two types of retinas during the digestion procedure, with the exception that the photoreceptors of the damaged retinas appeared darker in color than those of the controls.

Trypsin digestion of the mouse retina proved to be an extremely difficult, lengthy, and frustrating process with little reproducibility. The retinas often did not digest completely, requiring extensive mechanical dissection to remove the inner limiting membrane and cellular debris, often resulting in damage to the vessel bed. Digesting for longer periods in an attempt to correct this problem resulted in the dissolution of the entire retina, including the vasculature. A mounting of the entire, intact vascular bed onto a slide was never accomplished.

Even somewhat successful digestions, in which large sections of the vasculature were mounted onto slides, yielded questionable results when stained (Figure 4.10).

While the photographs in the first row appear to show flatter, denser arteries and veins in the damaged eye (panel B) when compared with the control (panel A), this phenomenon cannot be seen in the second or third rows (photographs of different mice). The large, dark blue areas in these photographs represent sections of cellular debris that were not cleared away. As is evident in the pictures, these sections interfere with visualization of the vessels, particularly the capillary beds. However, removing such debris was often

impossible without destroying the vessels themselves. While it may be stated that the large vessels in eyes exposed to large amounts of excitation light had a flatter appearance than those of their unexposed counterparts, the evidence is largely inconclusive.

Additionally, no apparent changes in the capillary structure are visible.

As faulty technique may have been responsible for the poor quality of the mounts, the procedure was also performed on a healthy rat retina. Trypsin digestion of the rat retina is a widely accepted procedure, yielding excellent results when performed properly. Results of this digestion appear in Figure 4.11. The entire vascular bed was successfully mounted in nearly intact form, and the capillary structure is more clearly visible at high magnification. The success of this digestion indicates that faulty technique is not the cause of the poor quality of the mouse digests.

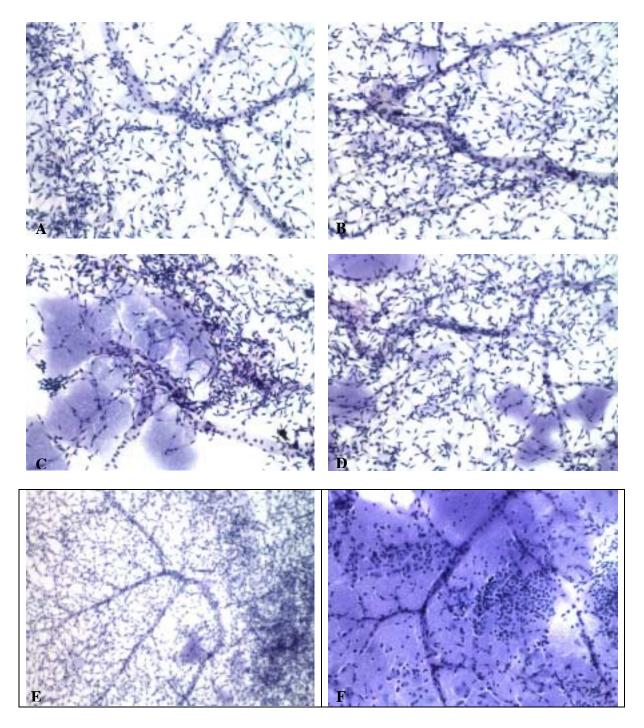


Figure 4.10—Trypsin digestion slides of control (left column) and damaged (right column) mouse retinas. The damaged retina in panel B appears to have lost some of its structural integrity when compared with its control in panel A—the large vessels appear flatter, and the nuclei (blue stain) appear denser within the vessels. However, the same direct comparison is not possible in the subsequent panels due to damage to the retinal vessels incurred during dissection, and dark staining of the cellular debris not removed during the trypsin digestion procedure.

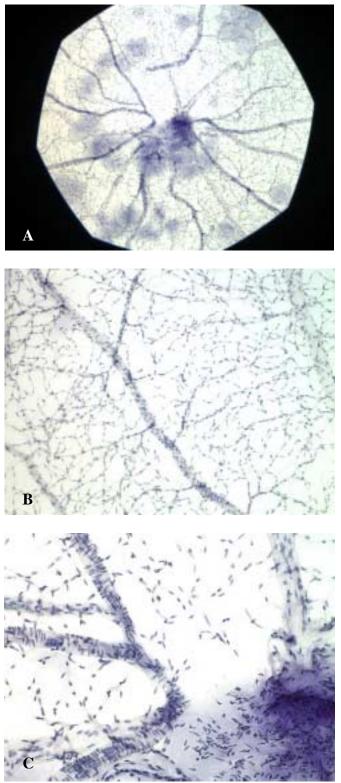


Figure 4.11—Trypsin digestion of the rat retina, viewed at 4x (A), 10x (B), and 20x (C) magnification. The vessel bed is nearly intact, and the capillaries are significantly more visible when compared with the mouse digests (Figure 4.1).

### 5. DISCUSSION

## Significance of Results

The first aim of this project was to calibrate the phosphorescence lifetime imaging system against known oxygen concentrations. This was achieved using the *in vitro* calibration system, shown in Figure 4.1. For the physiologic range of oxygen concentrations, the instrument and data analysis program produce accurate PO<sub>2</sub> maps.

The second aim of determining optimal parameters for probe excitation was achieved during *in vivo* experiments. Wavelength and bandwidth of 524±20 nm, as recommended in the literature, yielded acceptable maps. A decrease in PO<sub>2</sub> was used as an indicator of vessel damage; vessels damaged using this technique demonstrate a decrease in blood flow, which would subsequently decrease PO<sub>2</sub>. Setting energy and power to keep accumulated energy deposition below 2500 mJ/cm<sup>2</sup> prevented damage in the eye, as analyzed using observation of vessels and lack of a decrease in average PO<sub>2</sub> over the course of image collection.

Qualitatively, the relationship between PO<sub>2</sub> values in the different regions analyzed (vein, artery, and tissue) made logical sense. The physiological structure of the retina, with the high-PO<sub>2</sub> choroidal vasculature lying behind the lower-PO<sub>2</sub> retinal vasculature, caused some interference in phosphorescence images. In the major blood vessels, the light-absorbing properties of hemoglobin prevented the excitation light from reaching the probe within the choroidal vasculature, so the true PO<sub>2</sub> of the retinal vessels was determined. However, this effect was reduced in the capillary beds, which lie in the tissue sections analyzed—the excitation light was allowed to reach the choroid, and

phosphorescence was emitted from this oxygen-rich vasculature, yielding high PO<sub>2</sub> map values.

Relationships between camera exposure time, intensifier gain, and the quality of oxygen maps was also achieved with *in vivo* experiments. Signal-to-noise ratios of phosphorescence intensity images were determined to be dependent on camera intensifier gain settings. Low gain settings yielded better fits, and, therefore, better oxygen maps at lower signal-to-noise ratios, but at the cost of longer exposure times. When creating oxygen maps, the quality of the maps necessary must be weighed against the ability of the eye to withstand lengthy exposure to excitation light, the effect of longer exposure times on total experiment time, and the necessity for following rapid physiological changes.

The minimum number of images necessary to produce acceptable oxygen maps was determined to be near 15. Using 15 intensity images at incremented phase delays produced fits comparable to those obtained using 30 images. Seven images proved to be too few, as the delineation between vessels in the oxygen maps grew faint.

It was not possible to determine the level of damage caused by experimentation using trypsin digestion. This histological technique did not allow for viewing of the capillary structure in sufficient detail to analyze damage to vessel walls. The inability to see any changes in the capillary structure in retinal vasculatures that are decisively damaged renders trypsin digestion an unacceptable method for study of the mouse eye.

#### Future Work

Additional *in vitro* calibration studies should be performed to explain the variation in instrument PO<sub>2</sub> readings for identical applied oxygen concentrations. While the calibration curve shows relatively good correlation between instrument and applied oxygen, additional experiments may identify areas for improvement. Some non-linearity in the calibration curve may be present, and must be accounted for.

Data from three individual mice (2a, 6a, and 7a) were not included in summary analyses due to inadequate physiological control during experimentation. Likely changes in blood pressure and respiration rate during the course of experiments caused variations in intensity images, and, hence, inadequate sine-wave fits and poor oxygen maps. Such problems may have been prevented by a physiological control system to monitor blood pressure, ensure adequate respiration, and continuously maintain level of anesthesia. Implementing such a system will increase efficiency of experiments by allowing for greater frequency of experimental success.

Experiments determining the threshold of accumulated energy deposition for damage to retinal blood vessels would be beneficial. In this study, no experiments were carried out in which damage to blood vessels occurred—all animals maintained blood vessel structure and oxygen levels. Determining the level of light exposure needed to cause damage would allow for recommendations for maximum light exposure levels to be made. Additionally, the issue of excitation light modulation frequency was not addressed. Changes in modulation frequency could cause significant changes in quality of oxygen maps, and should be investigated.

Further analysis of the number of images necessary for creating good quality oxygen maps would be beneficial. It was determined that seven images are too few for producing accurate maps when compared with results using 15 images; however, numbers between seven and 15 were not examined. Additional *in vivo* experiments using different image numbers would allow the determination of the absolute minimum number of images necessary for accurate maps, and possibly allow for a decrease in light exposure to animals during experiments.

As trypsin digestion proved to be an unacceptable method for histologically examining the mouse eye, other methods should be investigated. Changes in capillary structure are of particular interest in diabetic retinopathy, a disease whose first clinical signs manifest in these minute vessels. The lack of capillary definition in the photographs shown in Figure 4.5 makes it unlikely that trypsin digestion and PAS/Hematoxylin staining will be of use in further mouse model study. Laver et al [1993] confirm that while retinal mounts of the type used in this study demonstrate the microaneurysms present in diabetic retinopathy, they did not provide a clear view of the capillaries. They also claim that, even under ideal conditions, it is difficult to obtain good quality trypsin digestions of mouse retinas. Cuthbertson et al [1986] also verify this claim. Both of these studies recommend the use of elastase, rather than trypsin, for digesting the mouse retina. Analysis of eyes subjected to the phosphorescence lifetime imaging technique using elastase digestion and staining may be of benefit.

#### **Conclusions**

The specific aims for achieving the goal of optimization of the phosphorescence lifetime imaging system for the mouse eye were calibration of the system, determination of probe excitation parameters, determination of image collection and analysis parameters, and examination of microvascular damage using histology. Calibration was accomplished using an *in vitro* system to correlate instrument-derived oxygen tensions with known concentrations. Probe excitation parameters were studied indirectly through the determination of accumulated energy deposition during series of phosphorescence lifetime imaging experiments. Image collection and analysis parameters were studied in depth, with the final determination that lower intensifier gains produced better maps at lower signal-to-noise ratios, but higher gain settings allowed reasonably good maps to be created with shorter exposure times. Gain and exposure time settings for specific experiments may be determined using the graphs in Figure 4.8 as a guide. Seven was determined to be too few images for creating clear, precise oxygen maps—the number necessary is closer to fifteen. The aim of using histology to examine damage caused by probe excitation was not achieved, but recommendations for performing this procedure more effectively were made.

This work demonstrates that the phosphorescence lifetime imaging instrumentation and technique may be used for studying oxygen tensions in the mouse eye. The determination of the optimal parameters for conducting such experiments will allow for the investigation of how changes in retinal oxygen tensions correlate with the progression of numerous ocular diseases, such as diabetic retinopathy, retinopathy of prematurity, and glaucoma.

#### References

- Aiello, L.P., T.W. Gardner, G.L. King, G. Blankenship, J.D. Cavallerano, F.L. Ferris, R. Klein. 1998. Diabetic Retinopathy. *Diabetes Care*, 21:143-156.
- Aiello, L.P., E.A. Pierce, E.D. Foley, H. Takagaki, H. Chen, L. Riddle, N. Ferrara, G.L. King, and L.E.H. Smith. 1995. Suppression of retinal neovascularization *in vivo* by inhibition of vascular endothelial growth facto (VEGF) using soluble VEGF-receptor chimeric proteins. *Proceedings of the National Academy of Science, USA*, 92:10457-10461.
- Alder, V.A., S.J. Cringle, and M. Brown. 1987. The effect of regional retinal photocoagulation on vitreal oxygen tension. *Ivestigative Ophthalmology and Visual Science*, 28:1078-1085.
- Alder, V.A., S.J. Cringle, and I.J. Constable. 1983. The retinal oxygen profile in cats. *Investigative Ophthalmology and Visual Science*, 24:30-36.
- Alder, V.A., E.N. Su, D.Y. Yu, S.J. Cringle, P.K. Yu. 1997. Diabetic retinopathy: Early functional changes. *Clinical and Experimental Pharmacology and Physiology*, 24:785-788.
- Alm, A. and A. Bill. 1972. The oxygen supply to the retina, I. Effects of changes in intraocular and arterial blood pressures, and in arterial pO<sub>2</sub> and pCO<sub>2</sub> on the oxygen tension in the vitreous body of the cat. *Acta Physiologica Scandanavia*, 84:261-274.
- Amin, R.H., R.N. Frank, A. Kennedy, D. Eliott, J.E. Puklin, G.W. Abrams. 1997. Vascular endothelial growth factor is present in glial cells of the retina and optic nerve of human subjects with nonproliferative diabetic retinopathy. *Investigative Ophthalmology and Visual Science*, 38:36-47.
- Andreani, D., G. Crepaldi, U. DiMario, G. Pozza. <u>Diabetic Complications: Early Diagnosis and Treatment.</u> 1987. Chichester: John Wiley & Sons, Inc.
- Araki, E., M.A. Lipes, M.-E. Patti, J.C. Bruning, B. Haag, III, R.S. Johnson, and C.R. Kahn. 1994. Alternative pathway of insulin signaling in mice with targeted disruption of the IRS-1 gene. *Nature*, 372:186-190.
- Benson, W., G. Brown, W. Tasman. 1988. <u>Diabetes and its Ocular Complications</u>. Philadelphia: Harcourt Brace Jovanovich, Inc.
- Berkowitz, B.A., R.A. Kowluru, R.N. Frank, T.S. Kern, T.C.Hohman, M. Prakash. 1999. Subnormal retinal oxygenation response precedes diabetic-like retinopathy. *Investigative Ophthalmology and Visual Science*, 40:2100-2105.

Crabbe, M.J.C. 1987. <u>Diabetic Complications: Scientific and Clinical Aspects</u>. London: Churchill Linvingstone.

Cuthbertson, R.A., T.E. Mandel. 1986. Anatomy of the mouse retina: Endothelial cell-pericyte ratio and capillary distribution. *Investigative Ophthalmology and Visual Science*, 27:1659-1664.

Davison, J.K. 2000. <u>Clinical Diabetes Mellitus: A Problem-Oriented Approach</u>. New York: Thieme Medical Publishers, Inc.

Delori, F.C. 1988. Noninvasive technique for oximetry of blood in retinal vessels. *Applied Optics*, 27:1113-1125.

Diabetes Control and Complications Trial Research Group. 1998. Early worsening of diabetic retinopathy in the diabetes control and complications trial. *Archives of Ophthalmology*, 116:874-886.

Ditzel, J. and E. Standl. 1975. The problem of tissue oxygenation in diabetes mellitus I. Its relation to the early functional changes in the microcirculation of diabetic subjects. *Acta Medica Scandanavia*, 578 (Supplementum):49-58.

Dowling, J.E. <u>The Retina: An Approachable Part of the Brain.</u> 1987. Cambridge: The Belknap Press of Harvard University Press.

Ernest, J.T., T.K. Goldstick, and R.L. Engerman. 1983. Hyperglycemia impairs retinal oxygen autoregulation in normal and diabetic dogs. *Investigative Ophthalmology and Visual Science*, 24:985-989.

Frank, R.N. 1991. On the pathogenesis of diabetic retinopathy: A 1990 update. *Ophthalmology*, 98:586-593.

Grunwald, J.E., C.E. Riva, J.Baine, and A.J. Brucker. 1992. Total retinal volumetric blood flow rate in diabetic patients with poor glycemic control. *Investigative Ophthalmology and Visual Science*, 33:356-363.

Grunwald, J.E., C.E. Riva, A.J. Brucker, S.H. Sinclair, and B.L. Petrig. 1984. Altered retinal vascular response to 100% oxygen breathing in diabetes mellitus. *Ophthalmology*, 91:1447-1452.

Grunwald, J.E., C.E. Riva, A.J. Brucker, S.H. Sinclair, and B.L. Petrig. 1986. Effect of panretinal photocoagulation on retinal blood flow in proliferative diabetic retinaopathy. *Ophthalmology*, 93:590-595.

Guillan, M.-T., E. Hummler, E. Schaerer, J.-Y. Wu, M.J. Birnbaum, F. Beerman, A. Schmidt, N. Deriaz, and B. Thorens. 1997. Early diabetes and abnormal postnatal pancreatic islet development in mice lacking Glut-2. *Nature Genetics*, 17:327-330.

Hawes, N.L., R.S. Smith, B. Chang, M. Davisson, J.R. Hackenlively, S.W.M. John. 1999. Mouse fundus photography and angiography: a catalogue of normal and mutant phenotypes. *Molecular Vision*, 5:22-29.

Inoue, S. and K.R. Spring. 1997. *Video Microscopy: The Fundamentals*, Second Edition. New York: Plenum Press.

Ito, Y. and B.A. Berkowitz. 2001. MR studies of retinal oxygenation. *Vision Research*, 41:1307-1311.

Kern, T.S., R.L. Engerman. 1995. Galactose-induced retinal microangiopathy in rats. *Investigative Ophthalmology and Visual Science*, 36:490-496.

Kern, T.S., R.L. Engerman. 1996. A mouse model of diabetic retinopathy. *Archives of Ophthalmology*, 114:986-990.

Kern, T.S., J. Tang, M. Mizutani, R.A. Kowluru, R.H. Nagara, G. Romeo, F. Podesta, M. Lorenzi. 2000. Response of capillary cell death to aminoguanidine predicts the development of retinopathy: Comparison of diabetes and galactosemia. *Investigative Ophthalmology and Visual Science*, 41:3972-3978.

Kuwabara, T., D.G. Cogan. Studies of retinal vascular patterns: Part I, Normal architecture. 1960. *Archives of Ophthalmology*, 64:904-911.

Lakowicz, J.R. 1999. <u>Principles of Fluorescence Spectroscopy, Second Edition</u>. New York: Kluwer Academic/Plenum Publishers.

Lakowicz, J.R., and K.W. Berndt. 1991. Lifetime-selective fluorescence imaging using an rf phase-sensitive camera. *Review of Scientific Instruments*, 62:1727-1734.

Lakowicz, J.R., H. Szmacinski, K. Nowaczyk, K.W. Brerndt, and M. Johnson. 1992. Fluorescence lifetime imaging. *Analytical Biochemistry*, 202:316-330.

Laver, N.M., W.G. Robison, B.A. Pfeffer. 1993. Novel procedures for isolating intact retinal vascular beds from diabetic humans and animal models. *Investigative Ophthalmology and Visual Science*, 34:2097-2104.

Linsenmeier, R.A. 1986. Effects of light and darkness on oxygen distribution and consumption in the cat retina. *Journal of General Physiology*, 88:521-542.

Linsenmeier, R.A., R.D. Braun, M.A. McRipley, L.A. Padnick, J. Ahmed, D.L. Hatchell, D.S. McLeod, G.A. Lutty. 1998. Retinal hypoxia in long-term diabetic cats. *Investigative Ophthalmology and Visual Science*, 39:1647-1657.

Linsenmeier, R.A., L. Padnick-Silver. 2000. Metabolic dependence of photoreceptors on the choroids in the normal and detached retina. *Investigative Ophthalmology and Visual Science*, 41:3117-3123.

Linsenmeier, R.A. and C.M. Yancey. 1989. Effects of hyperoxia on the oxygen distribution in the intact cat retina. *Investigative Ophthalmology and Visual Science*, 30:612-618.

Lo, L.-W., C.J. Koch, and D.F. Wilson. 1996. Calibration of oxygen-dependent quenching of the phosphorescence of Pd-meso-tetra(4-carboxyphenyl) porphine: A phosphor with general application for measuring oxygen concentration in biological systems. *Analytical Biochemistry*, 236:153-160.

Molnar, I., S. Poitry, M. Tsacopoulos, N. Gilodi, and P.M. Leuenberger. 1985. Effect of laser photocoagulation on oxygenation of the retina in miniature pigs. *Investigative Ophthalmology and Visual Science*, 26:1410-1414.

Moses, R.A., Hart, W.A. 1987. <u>Adler's Physiology of the Eye: Clinical Applications</u>. St. Louis: The C.V. Mosby Company.

Patz, A. 1980. Studies on retinal neovascularization: Fiedenwald lecture. *Investigative Ophthalmology and Visual Science*, 19:1133-1138.

Pierce, E.A., R.L. Avery, E.D. Foley, and L.H. Smith. 1995. Vascular endothelial growth factor/vascular permeability factor expression in a mouse model for retinal neovascularization. *Proceedings of the National Academy of Science, USA*, 92:905-909.

Sakagami, K., T. Kodama, D.G. Puro. 2001. PDGF-induced coupling of function with metabolism in microvascular pericytes of the retina. *Investigative Ophthalmology and Visual Science*, 42:1939-1944.

Sherwood, L. 2001. <u>Human Physiology: From Cells to Systems</u>. Pacific Grove, CA: Brooks/Cole.

Shonat, R.D. Personal communication. 1/15/01-4/1/01.

Shonat, R.D. and P.C. Johnson. 1997. Oxygen tension gradients and heterogeneity in the venous microcirculation: A phosphorescence quenching study. *American Journal of Physiology*, 272:H2233-H2240.

Shonat, R.D., K.N. Richmond, P.C. Johnson. 1995. Phosphorescence quenching and the microcirculation: An automated mutilpoint oxygen tension measuring instrument. *Review of Scientific Instruments*. 66:5075-5084.

- Shonat, R.D., E.S. Wachman, W. Niu, A.P. Koretsky, D.L. Farkas. 1997. Near-simultaneous hemoglobin saturation and oxygen tension maps in the mouse brain using an AOTF microscope. *Biophysical Journal*, 73:1223-1231.
- Shonat, R.D., E.S. Wachman, W. Niu, A.P. Koretsky, D.L. Farkas. 1998. Near-simultaneous hemoglobin saturation and oxygen tension maps in the mouse cortex during amphetamine stimulation. *Oxygen Transport to Tissue*, 20:149-158.
- Shonat, R.D., D.F. Wilson, C.E. Riva, and S.D. Cranstoun. 1992. Effect of acute increases in intraocular pressure on intravascular optic nerve head tension in cats. *Investigative Ophthalmology and Visual Science*, 33:3174-3180.
- Shonat, R.D., D.F. Wilson, C.E. Riva, M. Pawlowski. 1992. Oxygen distribution in the retinal and choroidal vessels of the cat as measured by a new phosphorescence imaging method. *Applied Optics*, 31:3711-3718.
- Stefansson, E. 1990. Oxygen and diabetic eye disease. *Graefe's Archive of Clinical and Experimental Ophthalmology*, 228:120-123.
- Stefansson, E., D.L. Hatchell, B.L. Fisher, F.S. Sutherland, and R. Machemer. 1986. Panretinal photocoagulation and retinal oxygenation in normal and diabetic cats. *American Journal of Ophthalmology*, 101:657-664.
- Stefansson, E. M.B. Landers, III, and M.L. Wolbarsht. 1981. Increased retinal oxygen supply following pan-retinal photocoagulation and vitrectomy and lensectomy. *Transactions of the American Ophthalmological Society*, 79:307-334.
- Stefansson, E., R.L. Novack, and D.L. Hatchell. 1990. Vitrectomy prevents retinal hypoxia in branch retinal vein occlusion. *Investigative Ophthalmology and Visual Science*, 31:284-289.
- Stenbit, A.E., T.-S. Tsao, J. Lu, R. Burcelin, D.L. Geenen, S.M. Factor, K. Houseknecht, E.B. Katz, and M.J. Charron. 1997. GLUT4 heterozygous knockout mice develop muscle insulin resistance and diabetes. *Nature Medicine*, 3:1096-1101.
- Sussman, K.E., B. Draznin, W.E. James. 1987. <u>Clinical Guide to Diabetes Mellitus</u>. New York: Alan R. Liss, Inc.
- Tamemoto, H., T. Kadowaki, K. Tobe, T. Yagi, H. Sakura, T. Hayakawa, Y. Terauchi, K. Veki, Y. Kaburagi, S. Satoh, H. Sekihara, S. Yoshioka, H. Horikoshi, Y. Furuta, Y. Ikawa, M. Kasuga, Y. Yazaki, and S. Alzawa. 1994. Insulin resistance and growth retardation in mice lacking insulin receptor substrate-1. *Nature*, 372:182-186.
- Terauchi, Y., K. Iwamoto, H. Tamenoto, K. Komeda, C. Ishii, Y. Kanazawa, N. Asanuma, T. Aizawa, Y. Akanuma, K. Yasuda, T. Kodama, K, Tobe, Y. Yazaki, and T. Kadowaki. 1997. Development of non-insulin-dependent diabetes mellitus in the double

knockout mice with disruption of insulin substrate-1 and  $\beta$ -cell glucokinase genes: Genetic reconstitution of diabetes as a polygenic disease. *The Journal of Clinical Investigation*, 99:861-866.

Vanderkooi, J.M. 1990. Fluorescence and Phosphorescence. Lecture notes, University of Pennsylvania, Philadelphia, PA.

Vanderkooi, J.M., G. Maniara, T.J. Green, and D.F. Wilson. 1987. An optical method for measurement of dioxygen concentration based upon quenching of phosphorescence. *The Journal of Biological Chemistry*, 262:5476-5482.

Wachman, E.S., W.-H. Niu, and D.L. Farkas. 1996. Imaging acousto-optic tunable filter with 0.35-micrometer spatial resolution. *Applied Optics*, 35:5220-5226.

Watkins, P.J., P.L. Drury, S.L. Howell. 1996. <u>Diabetes and its Management</u>. Oxford: Blackwell Science, Ltd.

Wilson, D.F., A. Pastuszko, J.E. DiGiacomo, M. Pawlowski, R. Schneiderman, and M. Delivoria-Papadopoulos. 1991. Effect of hyperventilation on oxygenation of the brain cortex of newborn piglets. *Journal of Applied Physiology*, 70:2691-2696.

Withers, D.J., J.S. Gutierrez, H. Towery, D.J. Burks, J.M. Ren, S. Previs, Y. Zhang, D. Bernal, S. Pons, G.I. Shulman, S. Bonner-Weir, M.F. White. 1999. Disruption of IRS-2 causes type 2 diabetes in mice. *Nature*, 391:900-904.

Yamaoka, T., C. Nishimura, K. Yamashita, M. Itakura, T. Yamada, J. Fujimoto, and Y. Kokai. 1995. Acute onset of diabetic pathological changes in transgenic mice with human aldose reductase cDNA. *Diabetologia*, 38:255-261.

Yu, D.-Y. and S.J. Cringle. 2001. Oxygen distribution and consumption within the retina in vascularized and avascular retinas and in animal models of retinal disease. *Progress in Retinal and Eye Research*, 20:175-208.

Yu, D.-Y., S.J. Cringle, V. Alder, E.N. Su. 1999. Intraretinal oxygen distribution in the rat with graded systemic hyperoxia and hypercapnia. *Investigative Ophthalmology and Visual Science*, 40:2082-2087.

# Appendix A: Pd-Meso-Tetra (4-carboxyphenyl) Porphrine Probe Solution

- 1. Measure 50mg Pd-meso-tetra (4-carboxyphenyl) porphrine (Porphryin Products, Logan, UT) in a 1.5 ml microcentrifuge tube.
- 2. Add 500 µl 0.5N NaOH—probe dissolves in basic solution.
- 3. Warm under tap water until dissolved. Centrifuge.
- 4. Make a 1.25x albumin salt solution (25 ml)
  - a. Weigh 253.8 mg NaCl (FW = 58.44).
  - b. Add distilled/deionized water to 25 ml.
  - c. Pour salt water into a wide-mouth container, ad stirring rod and place on magnetic stir plate.
  - d. Add 1.88g albumin, bovine fraction V (Sigma, St. Louis, MO), taking care not to let the albumin touch the sides of the container.
  - e. Stir gently to dissolve (takes a few hours).
- 5. Slowly mix 4 ml albumin salt solution and all of the probe/NaOH solution.
- 6. Adjust pH to 7.4 with Tris(hydroxymethyl)aminomethane base (Aldrich Chemical Company, Milwaukee, WI) and HCl as needed. If albumin precipitates, pH is too low and Tris should be added.
- 7. Aliquot into 100 µl portions and store at -20°C.
- 8. Final solution is Pd-porphyrin (10 mg/ml) in BSA (60 mg/ml) 0.9% NaCl (Shonat 2001).

### Appendix B: "Retina" Program

The front panel of this program accepts as inputs  $\tau_o$ ,  $k_Q$ , modulation frequency and pulse time of excitation light, the name of the file containing the series of intensity images, and the number of intensity images to be used for fitting. It also allows the user to input a phase error, which is subtracted from the calculated phase delay, and a modulation error, which is divided into the calculated modulation. Averaging filters may be applied using the "Phos Filter" box. A region of interest (ROI) may then be selected within the intensity images, and a graph of phosphorescence intensity versus phase shift may be calculated and fit to the equation  $I(\theta_D) = a_0 + a_1 \sin\theta_D + b_1 \cos\theta_D$ . The parameters  $\theta$ ,  $\tau$ , and [PO<sub>2</sub>] are calculated (see Background), and the fitting parameters k,  $m_D$ , m, and  $R^2$  are also output. The program may also be used to create a number of maps using the intensity images, including PO<sub>2</sub> and  $R^2$  maps. The mapping function also allows ROI selection, and outputs the mean, standard deviation, maximum, and minimum values within the ROI.

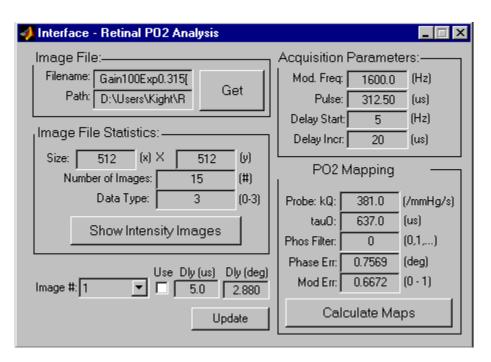


Figure B.1—"Retina" front panel. Phosphorescence intensity image files are input using the "Get" button. Individual images used for graphing and mapping are selected at the bottom of the panel—in this particular case, image #1 is not selected. The mapping parameters may be input using the PC keyboard. Once all parameters are correct, the "Show Intensity Images" and "Calculate Maps" buttons may be used.

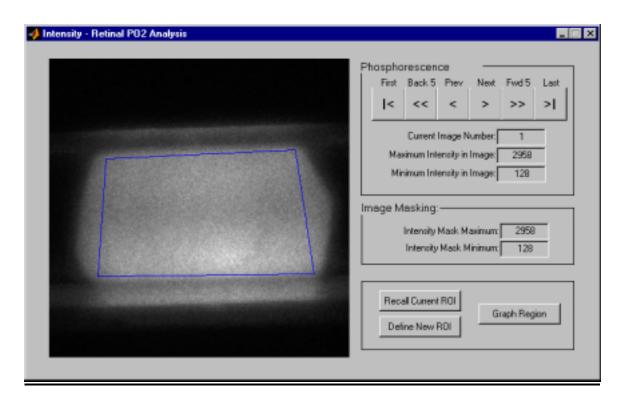


Figure B.2—"Show Intensity Images" screen. Individual intensity images may be viewed using the buttons at the top of the screen. An ROI may be selected by pressing one of the buttons at the bottom, and using the mouse to define a region on the image—the ROI selected in this image appears in blue. A graph of intensity versus phase delay for the ROI may be created by pressing the "Graph Region" button.

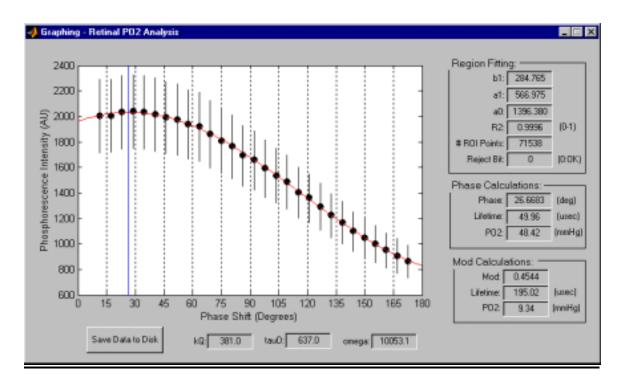


Figure B.3—"Graph Region" screen. Phosphorescence is plotted versus phase delay for the images and ROI selected. Relevant fitting and calculated parameters are output on the right. The blue line represents the curve maximum, which indicates the phosphorescence phase delay  $(\theta)$  also output on the right.

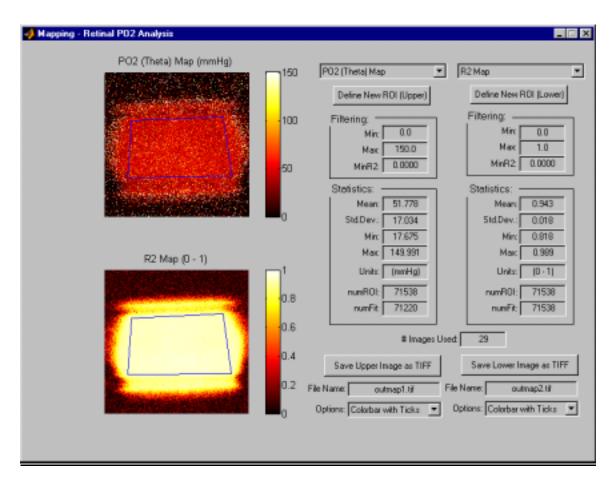


Figure B.4—"Calculate Maps" screen. A number of different maps may be created using the pull-down menus at the top. Filtering parameters may be input to reduce extraneous pixels in the images. Statistics are output in the right center of the screen.

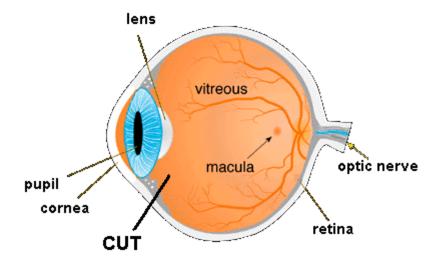
# **Appendix C: Procedure for Trypsin Digestion of the Retina**

Note: All procedures should be performed in a clean, dust-free environment to prevent contamination of samples. Procedures on the eye and retina should be performed under a dissecting microscope when necessary.

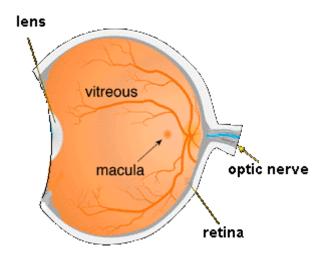
- 1. Remove eyes from animal and fix in 10% buffered formalin for a minimum of 5 days and a maximum of 10-12 days. After 10-12 days, transfer eyes from the fixative into phosphate-buffered saline and store at 4°C.
- 2. Prepare trypsin digestion buffer:
  - a. Weigh out 18.2 g Tris base (MW 121).
  - b. Add approximately 800 ml deionized water.
  - c. Create a 0.2 M NaF (MW 42) solution using the following formula to determine the weight of NaF to be added:

42 x (volume of tris/water solution in L) x 0.2 = weight of NaF in grams

- d. Add this measured weight of NaF to the tris/water solution.
- e. Bring this solution to pH 7.8 using concentrated HCl.
- f. Store refrigerated.
- 3. Prepare trypsin digestion solution:
  - a. Weigh out 0.3 g crude trypsin 1:250 powder (it is absolutely necessary to use crude trypsin—pure trypsin will not digest the retina).
  - b. Add trypsin digestion buffer to make 10 ml. Shake or vortex to completely dissolve the trypsin in the buffer.
  - c. Centrifuge or filter the solution to remove the sediment.
  - d. Either make this solution fresh each day, or aliquot 5-10 ml portions and store frozen.
- 4. Transfer eyes to a 50-ml beaker of distilled water. Change the water once by carefully pouring the water out of the beaker (do not pour out the eyes), and refilling the beaker.
- 5. Place one eye in a petri dish filled with distilled water, and remove excess tissue from around the eyeball.
- 6. Place the eye in a sized tray to hold it in place, and use a razor blade to make a small initial cut just below the limbus, as indicated on the diagram below:



7. Beginning at the initial cut, use tweezers and scissors to completely remove the anterior segment from the eyes, leaving only a cup containing the retina:



- 8. Return the eye to the water-filled petri dish, and pop out the lens with a sweep of curved scissors or forceps.
- 9. Hold the sclera (the outside cup of the remaining eyeball) with a pair of forceps, and use curved scissors or forceps to carefully free the retina from the eye. Take care not to tear the retina during this process. The sclera may be cut to facilitate removal of the retina.
- 10. Use an appropriately sized piece of glass tubing with a pipet bulb on the end to aspirate the retina and transfer it to a 50-ml beaker of distilled water.
- 11. Allow the retina to soak for 1-2 hours, changing the water 4 or 5 times. Take care not to pour the retina down the drain when changing the water.

- 12. Transfer the retina to a glass test tube (NOT plastic—the retina will stick to it) using the Pasteur pipette, and remove the water with a dropper. Add 5-10 ml trypsin digestion solution to the test tube. Place the tube in a 37°C shaker water bath at 40-60 cycles per minute.
- 13. Allow the retina to digest for and hour and a half to an hour and forty-five minutes. Diseased or damaged retinas may take longer to digest. Avoid over-digestion—this will cause the vessels in the retina to fall apart. If under-digested, the retina may be returned to the trypsin solution for further digestion.
- 14. Transfer the retina to a petri dish of distilled water with the Pasteur pipette. Do not throw away the trypsin solution. Three layers of the retina should be visible: the jelly-like inner limiting membrane (which is clear, and may not be visible unless the petri dish is agitated), the clear/whitish vascular layer, and the tan photoreceptor layer. Grasp the inner limiting membrane with forceps, and use scissors to free it from the retina. The membrane will be sticky and difficult to deal with. Be sure all of this membrane is removed, and wipe it away from the forceps on a paper towel.
- 15. Use a Pasteur pipette with an eyelash cemented to the tip to beat the photoreceptors away from the retina. Use the curved surface of the eyelash, never the tip, as the tip may damage the blood vessels. Continue manipulating the retina with the eyelash to remove all cellular debris, frequently dipping the eyelash in the trypsin solution to prevent it from sticking to the retina.
- 16. Once all debris is removed, the vasculature will remain. It will be nearly transparent. Place a microscope slide in a separate petri dish, and fill the dish with enough water adequately cover the slide. Aspirate the retinal vessels and deposit them on the slide. Using the eyelash, carefully unfold the vessels and very gently press them onto the slide. If necessary, cut the vessels so they lie flat. Slowly remove the water from the petri dish using a peristaltic pump set a low speed.
- 17. Allow the vessels to air-dry overnight.
- 18. Mount and stain the retinas using the Procedure for Hematoxylin Staining of Trypsin Digests.

## **Appendix D: Procedure for Hematoxylin Staining of Trypsin Digests**

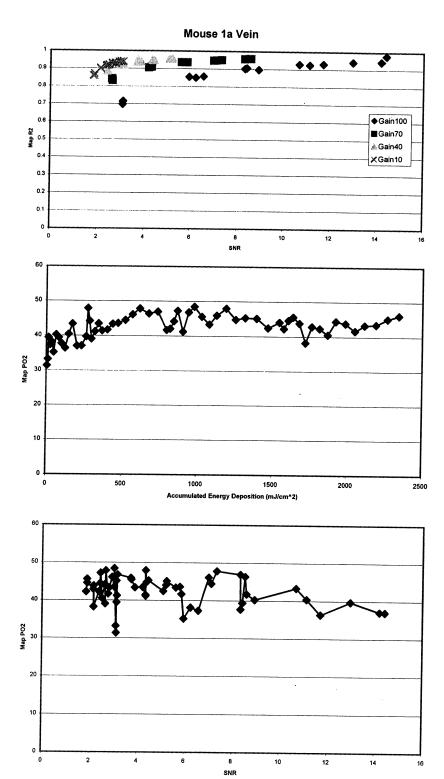
- 1. After mounting retinas onto slides, allow to air-dry overnight.
- 2. Prepare periodic acid solution:
  - a. Weigh out 0.8 g reagent grade periodic acid.
  - b. Add 20 ml distilled water. Agitate to dissolve.
  - c. Add 10 ml 0.2M sodium acetate.
  - d. Add 70 ml 95% ethanol (66.5 ml EtOH + 3.5 ml water).
  - e. Swirl to mix. Make this solution fresh each day it is used. Store refrigerated when not in use.
- 3. Place slides in slide staining tray.
- 4. Stain the slides with the following solutions by using one reagent bottle for each step. Pour the reagent into the staining tray, allow to sit for the specified time, and then return the reagent to the bottle (except where specified).
  - a. 70% ethanol—5 minutes
  - b. Periodic acid solution—5 minutes
  - c. 70% ethanol, 3 changes (3 reagent bottles)—2 minutes each
  - d. Rinse in distilled water (discard water)
  - e. Schiff's reagent—25 minutes (Schiff's reagent is light sensitive. Place slides in a drawer or other dark area when soaking in this reagent.)
  - f. Running tap water—20 minutes
  - g. Hematoxylin—10 minutes (Hematoxylin is light sensitive. Place slides in a drawer or other dark area when soaking in this reagent)
  - h. Running tap water—20 minutes
  - i. 95% ethanol, 3 changes—2 minutes each
  - j. 100% ethanol, 3 changes—2 minutes each
  - k. Xylene, 3 changes—2 minutes each
  - 1. Drop Permount or Histoclad onto each stained retina and apply a cover glass.

Vessel walls will appear magenta, and nuclei will be blue.

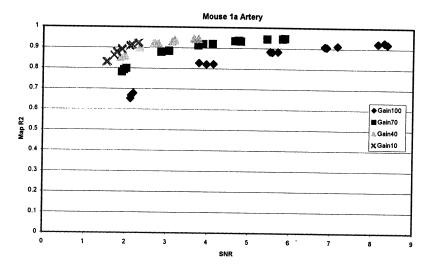
## **Appendix E: Data Tables and Graphs**

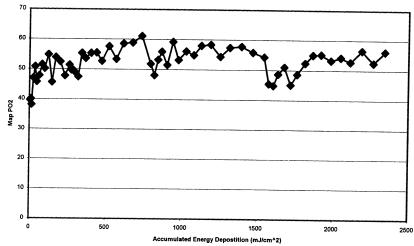
The following are Microsoft Excel spreadsheets used for analysis of data obtained during *in vivo* experiments. Data are organized by animal number and vessel type, and listed in the order images were taken. Map R<sup>2</sup> vs. SNR graphs were not created for Mouse 6a because the animal died during experimentation, and insufficient data were acquired at each gain setting to allow for statistical significance. The data from this mouse are not included in the summary graphs in the Results section. Additionally, data from Mice 2a and 7a are not included, as excessive head movement and drastic changes in the blood flow during image acquisition prevented the creation of satisfactory oxygen maps

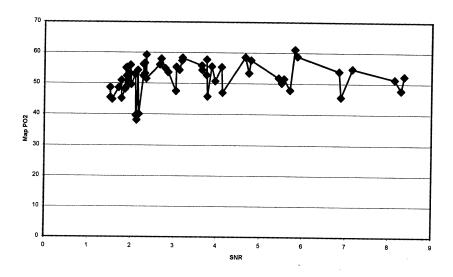
Gain		Exposure 1	Relative Irr Cun	nulativ	e A coumula	4. CND	DOO Marro	D00.0/ -		
	100	0.06	1	1 Iuia				PO2 St. De		R2 St. Dev
	100	0.06	2	2				25.532	0.7126	0.1108
	100	0.06	3	3					0.697	0.1198
	100	0.145	1	4					0.7154	0.1148
	100	0.145	2	5				22.3232	0.8576	0.0617
	100	0.145	3	6				23.4717	0.85	0.0649
	100	0.23	1	7				20.675	0.8547	0.0612
	100	0.23	2	8				22.1909	0.8975	0.0415
	100	0.23	3	9			39.3985	21.5983	0.9058	0.0409
	100	0.315	1	10				19.4958	0.9017	0.0428
	100	0.315	2	11			36.3694	16.1542	0.9314	0.0289
	100	0.315	3	12	146.7248 170.6102		40.4209	20.7441	0.926	0.0333
	100	0.4	1	13	200.9409		43.3651	19.3882	0.9297	0.0312
	100	0.4	2	14			37.0123	14.0576	0.9778	0.0252
	100	0.4	3	15	231.2717		37.0853	14.4383	0.9456	0.0246
	70	0.15	1	16	261.6024		39.713	17.0262	0.9426	0.0249
	70	0.15	2	17	272.9764 284.3504		47.847	30.1669	0.8315	0.0711
	70	0.15	3	18	295.7244		44.2218	28.1264	0.8433	0.0681
	70	0.31	1	19			39.0434	25.3113	0.8436	0.0667
	70	0.31	2		319.2307		41.1906	20.8689	0.9089	0.0392
	70	0.31	3	20	342.737		43.4629	22.788	0.9061	0.0389
	70	0.37	1	21 22	366.2433		41.4235	22.1984	0.9092	0.0389
	70	0.47	2		401.8819		41.7067	18.6205	0.9373	0.0283
	70	0.47	3	23 24	437.5205		43.386	19.3558	0.9371	0.0266
	70	0.47	1		473.1591	5.777164	43.5985	20.2452	0.9367	0.0277
	70	0.63	2	25	520.9299		44.4771	17.7629	0.9491	0.0221
	70	0.63	3	26 27	568.7008		46.1181	20.8784	0.9474	0.0219
	70	0.79	1	28	616.4717	7.332793	47.8064	19.0871	0.9513	0.0209
	70	0.79	2		676.3748	8.517693	46.3823	17.9728	0.959	0.0173
	70	0.79	3	29 30	736.278	8.327271	46.9208	20.5558	0.9576	0.0183
	40	0.73	1	31	796.1811	8.581879	41.7116	15.173	0.9589	0.0173
	40	0.32	2	32	820.4457	2.3966	42.0659	24.4672	0.8847	0.0493
	40	0.32	3	33	844.7102	2.461529	44.1889	26.0651	0.8858	0.0484
	40	0.49	1	34	868.9748	2.430371	47.2164	26.4607	0.8874	0.0481
	40	0.49	2	35	906.1299		41.2365	20.8511	0.9193	0.0359
	40	0.49	3	36	943.285 980.4402	3.148657	46.8152	24.2926	0.9178	0.0346
	40	0.43	1	37		3.011221	48.4096	25.5742	0.9182	0.0351
	40	0.66	2	38	1030.486 1080.531	3.724993	45.5322	22.1523	0.951	0.0285
	40	0.66	3	39		3.875971	43.3804	18.7779	0.9388	0.0255
	40	0.83	1	40	1130.577	3.704214	45.9238	20.9077	0.9352	0.0282
	40	0.83	2	41	1193.513	4.3264	47.9599	20.8675	0.9482	0.0235
	40	0.83	3		1230.45	4.359643	44.7594	21.1474	0.9464	0.0231
	40	1	1	43	1319.386		45.2842	19.3097	0.9476	0.0228
	40	1	2	43 44	1395.213		45.1115	18.2914	0.9558	0.0199
	40	1	3		1471.039	5.075257	42.44	16.2557	0.9535	0.0196
	10	0.4	1		1546.866 1577.197	5.1926	44.0404	18.0572	0.9561	0.019
	10	0.4	2		1607.528	1.826257	42.2584	24.6142	0.8597	0.0586
	10	0.4	3			1.8781	44.597	26.6512	0.8703	0.0548
	10	0.55	1		1637.858 1679.563	1.867364	45.5887	27.2643	0.8593	0.0611
	10	0.55	2		1721.268	2.143657	43.8342	22.756	0.9022	0.0408
	10	0.55	3				38.2199	19.6557	0.9008	0.0416
	10	0.33	3 1		1762.972	2.13575	42.8878	23.885	0.8968	0.0432
	10	0.7	2	52 53		2.370264	42.3321	21.2545	0.9146	0.0377
	10	0.7	3		1869.13 1922.209	2.490007	40.5599	21.3576	0.9205	0.0334
	10	0.85	3 1				44.4406	21.3127	0.9176	0.0351
	10	0.85	2			2.640707	43.8111	21.1277	0.9287	0.0305
	10	0.85	3		2051.114		41.6892	19.7134	0.9286	0.0303
	10	0.03	1		2115.567 2191.394	2.802221	43.3271	20.2275	0.9296	0.0308
	10	1	2	50 <i>i</i>	2191.394		43.5173	20.1546	0.9393	0.0267
	10	1	3		2207.22 2343.047		45.124	19.5174	0.9392	0.0268
	. •	•	5	00 4	LU4U.U4/	2.321/43	46.1122	20.9077	0.9368	0.0286



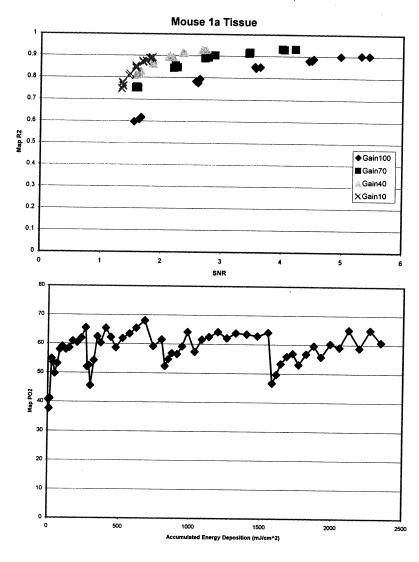
Gain		Exposure 1	Relative Irr Cun	oulativ	e Accumula	t, CND	DO2 Mass	D00 01 D	D0.44	
	100	0.06	1	1			39.6745	PO2 St. D€		R2 St. Dev
	100	0.06	2	2					0.6522	0.1285
	100	0.06	3	3					0.6784	0.1227
	100	0.145	1	4					0.6672	0.1207
	100	0.145	2	5				26.6557	0.8224	0.0674
	100	0.145	3	6				28.0794	0.8212	0.0728
	100	0.23	1	7			45.7589	27.8362	0.8271	0.0678
	100	0.23	2	8		5.56675	47.8422	24.8418	0.8838	0.0517
	100	0.23	3	9			51.5178	27.2305	0.8808	0.0527
	100	0.315	1	10			50.132	27.91	0.8838	0.0496
	100	0.315	2	11			54.7994	26.7813	0.9127	0.0367
	100	0.315	3	12			45.6133	22.3398	0.9061	0.0425
	100	0.4	1	13	200.9409		53.9341	28.3479	0.9082	0.0406
	100	0.4	2	14			52.4021	24.9794	0.9206	0.0339
	100	0.4	3	15	261.6024		47.7886	24.5135	0.9293	0.03
	70	0.15	1	16	272.9764		51.3911	22.8888	0.9238	0.0354
	70	0.15	2	17	284.3504		49.7236	30.6369	0.7933	0.0876
	70	0.15	3	18	295.7244		49.6578	29.4232	0.7997	0.0844
	70	0.31	1	19	319.2307		49.0474	30.8991	0.7826	0.0909
	70	0.31	2	20	342.737		47.4786	25.4282	0.8859	0.0464
	70	0.31	3	21	366.2433		55.3046	29.7117	0.8839	0.0535
	70	0.47	1	22			53.6004	28.1099	0.8794	0.0496
	70	0.47	2	23	401.8819		55.3252	27.091	0.9201	0.0345
	70	0.47	3	23	437.5205 473.1591		55.4945	27.3316	0.9197	0.0359
	70	0.63	1	25	520.9299		52.6991	26.1164	0.9123	0.0397
	70	0.63	2	26	568.7008		57.5879	25.8847	0.9333	0.0287
	70	0.63	3	27	616.4717		53.3979	26.6935	0.9374	0.0255
	70	0.79	1	28	676.3748		58.5217	25.3551	0.9352	0.0295
	70	0.79	2	29	736.278	5.870486	58.8598	24.5303	0.9481	0.024
	70	0.79	3	30	796.1811	5.816621	61.0782	27.4807	0.9457	0.0256
	40	0.32	1	31	820.4457	5.4385	51.7926	22.0157	0.9454	0.0249
	40	0.32	2	32	844.7102	1.861457	48.0736	27.1763	0.8527	0.0637
	40	0.32	3	33	868.9748	1.979321	53.192	29.4465	0.8637	0.0571
	40	0.49	1	34	906.1299	1.989986	55.9282	30.5722	0.8579	0.0615
	40	0.49	2	35	943.285	2.353907	51.4996	28.2755	0.8985	0.0459
	40	0.49	3	36	980.4402	2.353586 2.325614	59.2062	30.1828	0.9001	0.0429
	40	0.66	1	37	1030.486	2.323614	53.1608	27.416	0.8982	0.0471
	40	0.66	2	38	1080.531	2.794857	56.065	27.771	0.9191	0.035
	40	0.66	3	39	1130.577	2.794657	54.8396	25.4769	0.9208	0.0351
	40	0.83	1	40	1193.513	3.196864	57.9637 58.3452	27.121	0.9205	0.0344
	40	0.83	2	41		3.124921	54.3426	26.2303	0.9365	0.0274
	40	0.83	3	42	1319.386		57.3821	25.1233	0.9312	0.028
	40	1	1	43	1395.213	3.765514	57.7478	25.6143	0.9399	0.0309
	40	1	2	44	1471.039		55.7926	24.1372	0.9435	0.0244
	40	1	3	45	1546.866		54.3109	25.5267	0.9433	0.0256
	10	0.4	1	46	1577.197	1.525221	45.3989	29.2702	0.9431	0.0252
	10	0.4	2	47	1607.528	1.564357		26.9337	0.8276	0.0683
	10	0.4	3		1637.858	1.519693	44.8093	26.6422	0.8318	0.0717
	10	0.55	1		1679.563	1.778971	48.6575 50.9847	28.3567	0.8315	0.0718
	10	0.55	2		1721.268	1.78155	45.0981	26.245	0.88	0.0498
	10	0.55	3		1762.972	1.716043	48.5902	25.7877	0.8759	0.0543
	10	0.7	1		1816.051	1.902929		26.9661	0.8632	0.0565
	10	0.7	2	53	1869.13	1.889071	52.3737 55.0306	26.1536	0.8964	0.0442
	10	0.7	3		1922.209	1.91365	55.2284	29.0283 28.9121	0.8917	0.0487
	10	0.85	1			2.104971			0.891	0.046
	10	0.85	2		2051.114	2.104971	53.2896 54.2392	36.4084	0.9117	0.038
	10	0.85	3		2115.567		54.2392 52.8082	27.1513	0.912	0.0382
	10	1	1		2191.394		56.5722	25.88	0.9059	0.0394
	10	1	2	59	2267.22		52.437	26.3641	0.923	0.033
	0	1	3		2343.047		56.1862	25.3322	0.9196	0.0343
•	-	•	-	00 /	20.071	2.200014	JJ. 1002	27.8662	0.9216	0.0327

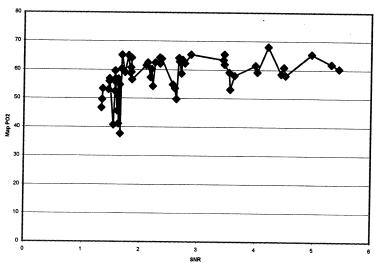




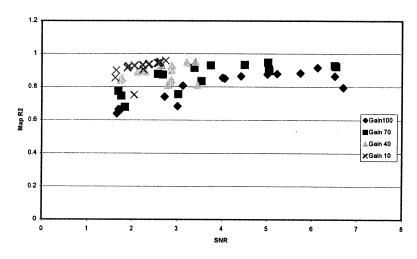


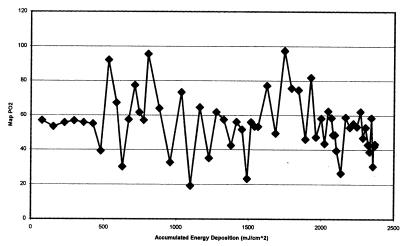
Gain			Relative Im Cu	ımulativ			PO2 Mean	PO2 St. D€	R2 Mean	R2 St. Dev
	100	0.06	1		1 4.54960		40.7296	32.7735	0.5973	0.1516
	100	0.06	2		9.09921			29.7527	0.6174	0.1511
	100	0.06	3		3 13.6488			31.8999	0.608	0.1545
	100	0.145	1		4 24.643		54.8134	30.8204	0.7835	0.0935
	100	0.145	2	5			53.5213	29.5981	0.7761	0.0881
	100	0.145	3	6			49.7479	30.9323	0.7937	0.0862
	100	0.23	1	7			53.1262	28.7827	0.8444	0.069
	100	0.23	2	8			57.9677	30.3869	0.8496	0.0662
	100	0.23	3	ç	98.95394	3.544707	59.0769	32.1188	0.851	0.0628
	100	0.315	1	10		4.515664	58.0034	29.9211	0.888	0.052
	100	0.315	2	11	146.7248	4.442821	58.5357	30.2162	0.8795	0.049
	100	0.315	3	12	170.6102	4.487464	60.8815	28.4017	0.8809	0.0531
	100	0.4	1	13	200.9409	5.443357	60.3867	29.2909	0.9023	0.0411
	100	0.4	2	14	231.2717	5.309457	61.9574	28.766	0.9032	0.0427
	100	0.4	3	15	261.6024	4.96845	65.4685	29.9226	0.8998	0.0439
	70	0.15	1	16	272.9764	1.587336	52.0365	30.546	0.7576	0.1023
	70	0.15	2	17	284.3504	1.568971	52.5013	34.5642	0.7532	0.0995
	70	0.15	3	18		1.606071	45.6005	29.0918	0.7527	0.1016
	70	0.31	1	19	319.2307	2.223664	54.2106	30.5602	0.8551	0.0608
	70	0.31	2	20	342.737		62.4493	33.3083	0.8468	0.064
	70	0.31	3	21	366.2433		60.29	31.7032	0.8442	0.0645
	70	0.47	1	22	401.8819		65.3519	30.0085	0.9028	0.0396
	70	0.47	2	23	437.5205	2.77385	62.2263	30.2084	0.8926	0.0479
	70	0.47	3	24	473.1591	2.717093	58.6863	30.1501	0.889	0.0479
	70	0.63	1	25	520.9299	3.460143	61.9075	30.1302	0.9176	0.0351
	70	0.63	2	26	568.7008	3.444807	63.4104	29.7229	0.9127	0.0368
	70	0.63	3	27	616.4717	3.457171	65.4113	31.0919	0.9157	0.0398
	70	0.79	1	28	676.3748	4.215021	68.0487	28.6898	0.9333	0.0293
	70	0.79	2	29	736.278	4.029407	59.1901	28.651	0.9304	0.0291
	70	0.79	3	30	796.1811	3.995114	61.517	27.6931	0.9338	0.0283
	40	0.32	1	31	820.4457	1.570479	52.3609	32.2871	0.8108	0.0203
	40	0.32	2	32	844.7102	1.650093	54.7581	31.4585	0.8286	0.0743
	40	0.32	3	33	868.9748	1.6226	56.8063	31.2912	0.8141	0.0743
	40	0.49	1	34	906.1299	1.858329	56.5369	28.9186	0.8616	0.0585
	40	0.49	2	35	943.285	1.845286	59.1537	31.1602	0.8631	0.0578
	40	0.49	3	36	980.4402	1.850293	64.1368	34.0511	0.8749	0.0543
	40	0.66	1	37	1030.486	2.184379	57.325	28.899	0.8946	0.0343
	40	0.66	2	38	1080.531	2.1062	61.5237	29.8273	0.8943	0.0453
	40	0.66	3	39	1130.577	2.13385	62.4736	29.4271	0.8974	0.0433
	40	0.83	1	40	1193.513	2.341079	64.2323	29.4555	0.9131	0.0376
	40	0.83	2	41	1256.45	2.350821	62.1063	29.1446	0.9124	0.0376
	40	0.83	3	42	1319.386		63.8288	29.727	0.9133	0.0364
	40	1	1	43	1395.213		63.4927	28.0271	0.9285	0.0304
	40	1	2	44	1471.039	2.685343	62.8859	28.4713	0.927	0.032
	40	1	3	45		2.671571	64.0949	28.9529	0.926	0.0324
	10	0.4	1	46	1577.197		46.6725	29.0297	0.7481	0.0324
	10	0.4	2	47	1607.528	1.347264	49.6254	31.4275	0.7758	0.0894
	10	0.4	3	48	1637.858	1.355986	53.3671	31.4607	0.7611	0.0094
	10	0.55	1	49		1.471607	55.9165	32.442	0.7011	
	10	0.55	2	50		1.474186	56.8763	31.7184	0.8143	0.0753
	10	0.55	3	51		1.453136	53.0637	30.3818		0.0785
	10	0.7	1	52	1816.051	1.574557	56.8056	31.7091	0.8081 0.8441	0.081
	10	0.7	2	53	1869.13	1.569671	59.5999	33.0134	0.853	0.0659 0.0636
	10	0.7	3			1.570557		30.5754	0.833	
	10	0.85	1			1.680764		32.5642	0.8739	0.0663
	10	0.85	2			1.738907		31.2603	0.8758	0.0526
	10	0.85	3					32.3143	0.8713	0.0534
	10	1	1			1.832129		31.6698	0.8893	0.0565
	10	1	2	59				32.1015		0.0477
	10	1	3				60.7875	30.033	0.8885	0.0492
			=				50.7075	50.055	0.8919	0.0466

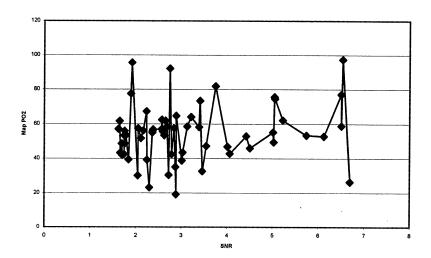




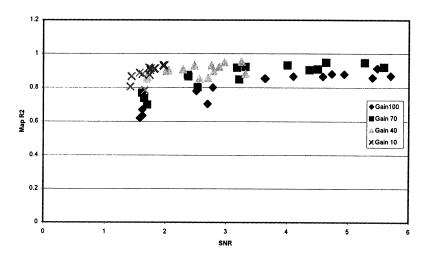
Gain		Exposure 1	Relative Im	Cumulativ	e Accumula	h SNR	PO2 Mean	PO2 St. De	DO Mass	D0 04 D
	10	1	1	1			56.9668	24.9118		R2 St. Dev
	10	1	2	2					0.9447	0.0243
	10	1	3	3					0.95	0.0218
	10	0.85	1	4					0.945	0.0235
	10	0.85	2	5					0.938	0.0276
	10	0.85	3	6				25.8445	0.9358	0.0279
	10	0.7	1	7			55.0178	25.472	0.9351	0.0274
	10	0.7	2	8			39.2874	20.6761	0.9064	0.0397
	10	0.7	3	9			92.0398	29.2817	0.9585	0.018
	10	0.55	1	10			67.2148	28.7629	0.9326	0.0286
	10	0.55	2	11	670.7185		30.059	22.1446	0.7523	0.0931
	10	0.55	3	12			57.4077	24.3672	0.9279	0.0305
	10	0.4	1	13	712.878		77.4367	31.5587	0.9144	0.0374
	10	0.4	2	14	743.5394		61.6264	30.6959	0.8999	0.0441
	10	0.4	3		774.2008		57.0768	30.1289	0.855	0.0619
	40	1		15	804.8622		95.5203	30.0823	0.9257	0.032
	40	1	1	16	881.5157		63.9841	26.6199	0.9475	0.0234
	40		2	17	958.1693	3.45935	32.5992	20.3859	0.8099	0.0851
		1	3	18	1034.823		73.3564	28.6087	0.9513	0.0209
	40	0.83	1	19	1098.445	2.8844	19.1281	6.4826	0.9011	0.0376
	40	0.83	2	20	1162.068		64.6346	29.1275	0.9263	0.0313
	40	0.83	3	21	1225.69	2.870486	35.0474	20.3473	0.8429	0.0602
	40	0.66	1	22	1276.281	2.651079	61.856	28.3074	0.9312	0.0313
	40	0.66	2	23	1326.873	2.839107	57.4792	30.4785	0.8298	0.069
	40	0.66	3	24	1377.464	2.785543	42.3912	26.1678	0.8109	0.0773
	40	0.49	1	25	1415.024		56.1517	28.2674	0.9009	0.0429
	40	0.49	2	26	1452.585	2.111593	51.7288	28.3655	0.89	0.0468
	40	0.49	3	27	1490.145	2.295193	23.1599	8.9142	0.8924	0.0369
	40	0.32	1	28	1514.674	1.75465	55.9479	31.176	0.8513	0.0649
	40	0.32	2	29	1539.203	1.783964	53.4429	30.3767	0.8514	0.0646
	40	0.32	3	30	1563.732	1.745214	53.3338	30.6464	0.8398	0.0682
	70	0.79	1	31	1624.289	6.506057	77.0831	29.6504	0.9282	0.0283
	70	0.79	2	32	1684.845	5.0259	49.4505	20.1898	0.9477	0.0242
	70	0.79	3	33	1745.401	6.536979	97.367	27.0013	0.9225	0.0348
	70	0.63	1	34	1793.693	5.04235	75.6431	31.7865	0.908	0.0406
	70	0.63	2	35	1841.985	5.0521	74.589	32.8444	0.8976	0.0434
	70	0.63	3	36	1890.276	4.505064	46.0104	21.0133	0.9333	0.0295
	70	0.47	1	37	1926.304	3.751429	81.8249	30.4107	0.9306	0.0293
	70	0.47	2	38	1962.331	3.547986	47.2302	27.093	0.835	0.0722
	70	0.47	3	39	1998.358	3.389336	58.1711	28.1642	0.9146	0.0351
	70	0.31	1	40	2022.12	3.027236	43.4873	28.8962	0.7554	0.1014
	70	0.31	2	41	2045.883		62.3756	30.7723	0.8782	0.0545
	70	0.31	3		2069.646		58.4532	30.3622	0.8737	0.0558
•	70	0.15	1		2081.144		48.6087	31.8396	0.7462	0.0987
	70	0.15	2			1.692293	48.6453	31.4387	0.7737	0.0954
	70	0.15	3	45	2104.14	1.83745	39.4355	29.1474	0.6785	0.0934
10	00	0.4	1			6.696186	26.3566	17.8298	0.7967	0.1209
10	00	0.4	2			6.508757	58.8378	31.5043	0.7907	0.0794
10	00	0.4	3			6.120893	52.869	26.7578	0.9158	0.0625
10	00	0.315	1	49	2220.27		55.1505	28.8766	0.8759	
	00	0.315	2		2244.416		53.4063	28.1759		0.0542
	00	0.315	3		2268.562		62.1295	30.7703	0.8827	0.0525
	00	0.23	1		2286.192		46.8359		0.8792	0.0549
10		0.23	2		2303.822		52.9312	25.9023 27.955	0.8547	0.0613
10		0.23	3		2321.453				0.8644	0.0623
10		0.145	1		2332.567		42.847 38.760	25.2951	0.8506	0.0644
10		0.145	2		2343.682		38.769	28.2024	0.6833	0.1238
10		0.145	3		2354.797		58.433	33.2484	0.8073	0.0815
10		0.06	1				30.3368	24.683	0.74	0.1022
10		0.06	2			1.739021	42.4631	31.2443	0.6594	0.1363
10		0.06	3					29.2385	0.6642	0.1333
	-	3.50	3	00 /	2000.034	1.658679	43.2512	30.8114	0.6386	0.1328

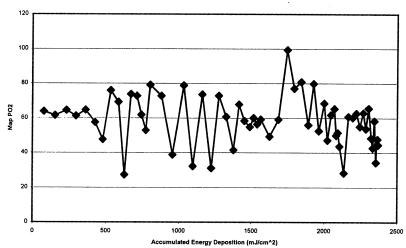


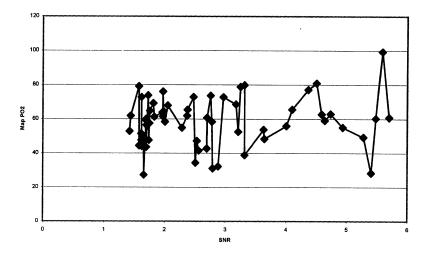




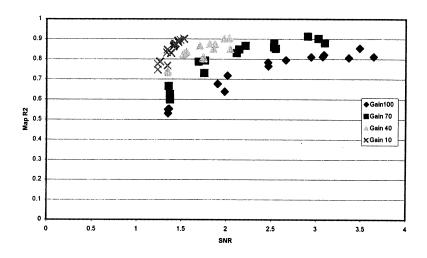
Gain		Exposure 1	Relative Im	Cumulative	Accumulat	SNR	PO2 Mean	PO2 St. D€	R2 Mean	R2 St. Dev
	10	1	1	1			63.843	29.4655	0.9319	0.0334
	10	1	2	2				28.009	0.9319	0.0294
	10	1	3	3			64.4603	28.7177	0.9297	0.0301
	10	0.85	1	4			61.2324	28.6511	0.9138	0.0395
	10	0.85	2	5			64.7109	31.0928	0.9145	0.0391
	10	0.85	3	6			57.5263	28.2588	0.9024	0.042
	10	0.7	1	7			47.6373	27.9232	0.8744	0.0516
	10	0.7	2	8			75.9263	30.7795	0.926	0.0305
	10	0.7	3	9			69.1917	30.4249	0.9097	0.0376
	10	0.55	1	10		1.656264	27.2656	18.3756	0.7847	0.0887
	10	0.55	2	11			73.8256	29.2442	0.9187	0.0346
	10	0.55	3	12			72.7801	34.0154	0.8799	0.0496
	10	0.4	1	13			61.8509	32.7413	0.8674	0.0558
	10	0.4	2	14			52.8608	31.4433	0.8061	0.0330
	10	0.4	3	15			79.0714	30.4531	0.8867	0.0021
	40	1	1	16			72.7498	28.3305	0.9479	0.0251
	40	1	2	17			38.8248	20.5448	0.8827	0.0231
	40	1	3	18	1034.823		78.7902	28.1636	0.9528	0.0214
	40	0.83	1	19	1098.445		32.1917	11.8859	0.922	0.0214
	40	0.83	2	20	1162.068	2.758043	73.5797	30.5994	0.9323	0.0301
	40	0.83	3	21	1225.69	2.793179	31.0872	13.675	0.8948	
	40	0.66	1	22	1276.281	2.476057	72.8878	28.9564	0.0946	0.0421
	40	0.66	2	23	1326.873	2.701136	60.6739	31.9878		0.0293
	40	0.66	3	24	1377.464	2.559514	41.5109	23.7744	0.8571	0.0593
	40	0.49	1	25	1415.024	2.049921	67.8125	31.2995	0.8534	0.0597
	40	0.49	2	26	1452.585	2.005021	58.3659	28.9462	0.9015	0.0413
	40	0.49	3	27	1490.145	2.285964	54.8258	26.417	0.8979	0.0445
	40	0.32	1	28	1514.674	1.694479	60.0485	30.9162	0.9069	0.0379
	40	0.32	2	29	1539.203	1.694564	56.4628		0.8642	0.0575
	40	0.32	3	30	1563.732	1.689943	59.1837	30.6658 31.2848	0.8574	0.0563
	70	0.79	1	31	1624.289	5.278986	49.3071	21.111	0.8521	0.0619
	70	0.79	2	32	1684.845	4.63985	59.0976	25.6647	0.9478	0.0222
	70	0.79	3	33	1745.401	5.590479	99.3124	29.9255	0.9487	0.0223
	70	0.63	1	34	1793.693	4.368914	77.0465		0.9209	0.0336
	70	0.63	2	35	1841.985	4.506579	80.8483	30.174	0.9046	0.0406
	70	0.63	3	36	1890.276	4.006829	55.9467	28.67 25.4203	0.909	0.0376
	70	0.47	1	37	1926.304	3.316593	79.7966		0.9319	0.0305
	70	0.47	2	38	1962.331	3.213107	52.5233	30.2494	0.9221	0.0347
	70	0.47	3	39	1998.358	3.17635	68.4994	28.9354	0.8488	0.0645
	70	0.31	1	40	2022.12	2.529514	47.124	31.7135 29.2947	0.9181	0.0341
	70	0.31	2	41		2.369407	61.8032		0.803	0.0815
	70	0.31	3	42	2069.646		65.2965	29.3746 32.5831	0.8747	0.0538
	70	0.15	1		2081.144	1.650186	49.8913	31.4153	0.8657	0.0531
	70	0.15	2	44	2092.642	1.613364	51.4848	31.0505	0.7378	0.1028
	70	0.15	3	45	2104.14	1.696336	43.5997	29.3534	0.769	0.0927
1	00	0.4	1	46	2134.801	5.40435	28.3451		0.6996	0.1236
	00	0.4	2	47	2165.463	5.701907	60.764	17.7348	0.8587	0.0608
	00	0.4	3		2196.124	5.4807	60.1958	30.1634 29.8244	0.8687	0.0562
	00	0.315	1	49	2220.27	4.58965	62.6501		0.9133	0.0391
	00	0.315	2		2244.416			29.3963	0.8648	0.0601
	00	0.315	3	51	2268.562	4.734857	55.0361	2930209	0.8781	0.0504
	00	0.23	1		2286.192		62.9092	32.8323	0.8807	0.0518
	00	0.23	2	53	2303.822	3.632279 4.102021	53.7823 65.5374	28.3964 32.4188	0.8548	0.0645
	00	0.23	3	54	2321.453	3.645779	48.3405		0.8657	0.0587
	00	0.145	1	55	2332.567	2.694007	40.3405	27.1014	0.8537	0.0637
	00	0.145	2	56	2343.682		58.3201	30.2718	0.7046	0.121
	00	0.145	3	57	2354.797			32.3686	0.8011	0.0831
	00	0.06	1	57 58	2359.396		34.3168	23.7818	0.7796	0.0878
	00	0.06	2	59	2363.995	1.62135 1.6164	44.0424 47.7245	32.2331	0.6346	0.1314
	00	0.06	3		2368.594	1.578414	47.7245	33.0723	0.6695	0.1414
•	-	5.00	5	00	2000.084	1.57 04 14	44.4237	31.7052	0.6199	0.1388

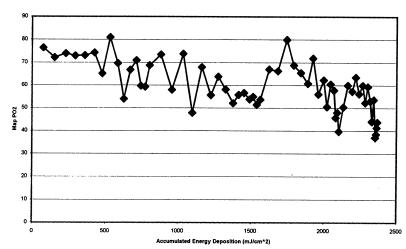


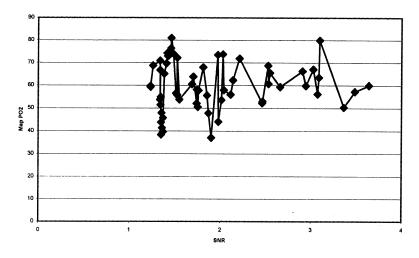




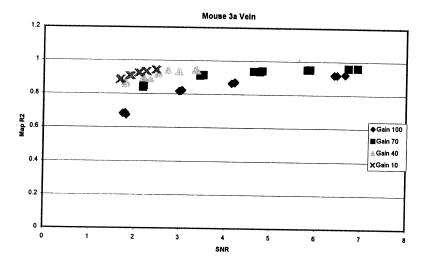
Coin		Evenesure =	l Dalativa la	· Come de tion	. A	CND	DO0 M	DO0 04 D	D0 14	D0 01 D
Gain	10	Exposure 1	Relative Im 1	Cumulative 1	Accumulat 76.65354		76.3928	PO2 St. D€		R2 St. Dev
	10	1			153.3071	1.436314	70.3926	30.9213 30.5176	0.8919 0.9012	0.00473 0.0432
	10	1	3	3	229.9606	1.4857	73.9111	30.829	0.8955	0.0432
	10	0.85		4	295.1161	1.425407	72.9266	31.6653	0.8771	0.0541
	10	0.85		5	360.2717	1.432193	73.0667	32.1045	0.8766	0.0542
	10	0.85		6	425.4272		74.2351	32.7031	0.8701	0.0542
	10	0.7		7	479.0846		65.1099	32.3446	0.8306	0.0722
	10	0.7		8	532.7421	1.4625	80.9474	32.5748	0.8851	0.0501
	10	0.7		9	586.3996	1.408657	69.6301	31.3032	0.8632	0.055
	10	0.55		10	628.5591	1.342364	53.9505	32.1208	0.768	0.0982
	10	0.55		11	670.7185	1.341036	66.7429	32.5805	0.8476	0.0625
	10	0.55	3	12	712.878	1.338143	70.899	33.1039	0.8324	0.0706
	10	0.4	1	13	743.5394	1.2339	59.7068	33.1784	0.7763	0.0936
	10	0.4	2	14	774.2008	1.233364	59.2788	35.4172	0.7465	0.1072
	10	0.4	3	15	804.8622	1.260157	68.7388	35.0929	0.788	0.0875
	40	1	1	16	881.5157	1.973564	73.4267	31.1712	0.9035	0.0414
	40	1	2	17	958.1693	2.041386	57.9837	29.3012	0.8502	0.063
	40	1	3	18	1034.823	2.030379	73.7586	33.0437	0.9045	0.0408
	40	0.83	1	19	1098.445	1.871243	47.8317	26.6129	0.8726	0.0511
	40	0.83	2	20	1162.068	1.813829	67.9583	32.4025	0.876	0.0549
	40	0.83	3	21	1225.69	1.8553	55.6266	31.0701	0.8505	0.0635
	40	0.66	1	22	1276.281	1.704507	63.7792	32.1048	0.8665	0.0602
	40	0.66	2	23	1326.873	1.744179	58.1461	33.0262	0.8035	0.0797
	40	0.66	3	24	1377.464	1.743043	52.1219	30.1629	0.8087	0.079
	40	0.49	1	25	1415.024	1.527579	55.7974	30.0914	0.8285	0.0722
	40	0.49	2	26	1452.585	1.515957	56.6199	31.4221	0.8242	0.0715
	40 40	0.49 0.32	3	27	1490.145	1.552579	53.8295	30.9495	0.837	0.0671
	40	0.32	1 2	28 29	1514.674	1.3469	54.9296	32.7953	0.741	0.1092
	40	0.32	3	30	1539.203 1563.732	1.343586 1.341079	51.4345	32.2577	0.7337	0.1009
	70	0.79	1	31	1624.289	3.025286	53.6587 67.0569	30.4489 30.7179	0.736	0.1046
	70	0.79	2	32	1684.845	2.907457	66.2741	31.2845	0.9028 0.9138	0.0422 0.0381
	70	0.79	3	33	1745.401	3.0976	79.9557	32.3169	0.8809	0.0527
	70	0.63	1	34	1793.693	2.528907	68.7506	32.7587	0.8599	0.059
	70	0.63	2	35	1841.985	2.55015	65.4942	31.425	0.8523	0.0628
	70	0.63	3	36	1890.276	2.532071	60.7547	30.0403	0.8806	0.0507
	70	0.47	1	37	1926.304	2.212671	71.8664	32.8475	0.8668	0.0585
	70	0.47	2	38	1962.331	2.115721	56.0456	31.7302	0.8301	0.0809
	70	0.47	3	39	1998.358	2.142029	62.2864	32.1192	0.8487	0.0663
	70	0.31	1	40	2022.12	1.754457	50.5175	31.5392	0.7311	0.1123
	70	0.31	2	41	2045.883	1.691764	60.5259	33.6843	0.7869	0.0893
	70	0.31	3	42	2069.646	1.761607	57.801	34.1796	0.7924	0.083
	70	0.15	1	43	2081.144	1.372336	45.7276	31.9532	0.6251	0.1445
	70	0.15	2	44	2092.642	1.356721	47.9529	32.5211	0.6658	0.1317
	70	0.15	3	45	2104.14	1.3727	39.705	29.694	0.5985	0.1459
	100	0.4	1		2134.801	3.364136	50.3808	31.2987	0.8062	0.0806
	100	0.4	2	47		3.642829	59.9986	31.8627	0.8117	0.0779
	100	0.4	3	48	2196.124	3.486771	57.308	31.9603	0.8542	0.0648
	100	0.315	1	49	2220.27	3.088614	63.5282	33.3704	0.8213	0.077
	100 100	0.315 0.315	2		2244.416	3.073864	56.2492	31.0567	0.8118	0.0764
	100	0.313	1	51 52	2268.562 2286.192	2.944579	59.8996	33.8895	0.8104	0.0853
	100	0.23	2	52	2303.822	2.46305 2.66165	52.3167 59.384	30.5387 31.3286	0.783	0.0926
	100	0.23	3		2321.453	2.466729	53.065	33.5954	0.7951 0.7645	0.086
	100	0.145	1	55	2332.567	1.982157	44.0428	32.8061	0.7645 0.6381	0.0954
	100	0.145	2		2343.682	2.014993	53.622	34.9182	0.0361	0.141 0.1083
	100	0.145	3	57	2354.797	1.903579	37.0593	26.1343	0.7176	0.1063
	100	0.06	1		2359.396	1.350243	38.4301	31.0432	0.5496	0.1272
	100	0.06	2		2363.995	1.360879	41.3349	32.6684	0.5525	0.1510
	100	0.06	3		2368.594	1.350971	43.8024	32.0532	0.5329	0.1724
								· <b></b>		

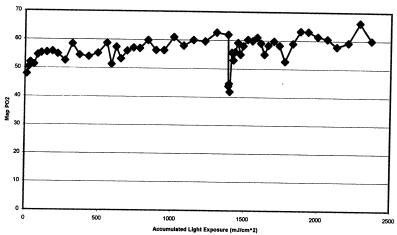


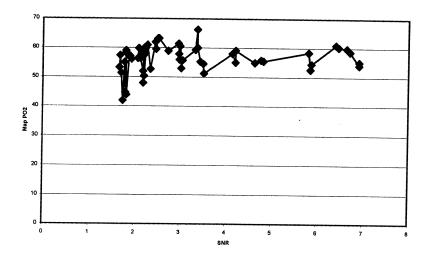




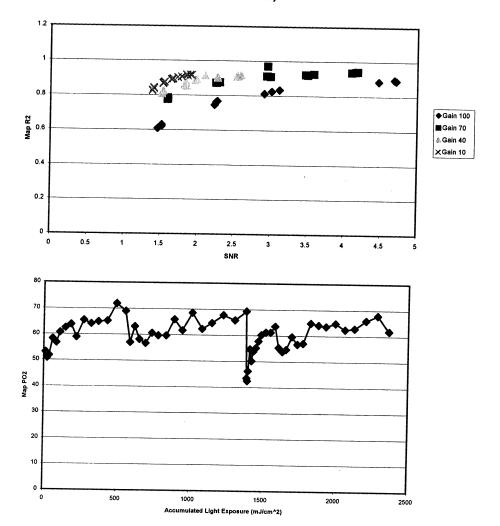
70	Gain		Exposure 1	Relative Im	Cumulative	: Accumulat	SNR	PO2 Mean	PO2 St De	R2 Mean	R2 St. Dev
70 0.15 2 2 23.70472 2.03107 50.3199 29.1613 0.8465 0.06 70 0.31 1 4 60.05197 3.525743 51.2359 23.7558 0.9158 0.03 70 0.31 2 5 84.54685 3.504614 54.5836 27.2598 0.9149 0.03 70 0.31 3 6 109.0417 3.46257 55.261 28.412 0.9112 0.9112 70 0.47 1 7 146.1791 4.821871 55.5287 25.3589 0.9424 0.0 70 0.47 2 8 188.3.165 4.7070214 55.8262 25.546 0.937 70 0.47 3 9 220.4539 4.634579 54.9351 25.2639 0.9387 0.02 70 0.63 1 10 270.2339 58.81957 52.6345 22.5569 0.9514 70 0.63 2 11 320.0138 58.1957 52.6345 22.5569 0.951 0.02 70 0.63 2 11 320.0138 58.1957 52.6345 22.5569 0.951 0.02 70 0.63 3 11 02.70.2339 58.81957 52.6345 22.5569 0.951 0.02 70 0.63 2 11 320.0138 58.1957 52.6345 22.5569 0.951 0.02 70 0.79 1 1 34.32.2161 6.919107 54.0441 20.5884 0.9616 0.01 70 0.79 2 1 14 496.6386 6.919107 54.0441 20.5884 0.9616 0.01 70 0.79 3 15 557.061 6.71752 158.759 22.8178 0.9663 0.01 70 0.79 3 15 557.061 6.71752 158.759 22.7578 0.9623 0.01 70 0.79 1 16 686673 1.706557 51.3835 27.1548 0.8885 0.04 10 0.4 1 16 588.6673 1.706557 51.3835 27.1549 0.888 0.04 10 0.4 2 17 690.5386 1.92114 55.992 2.92778 0.9869 0.02 10 0.55 1 19 695.3386 1.92115 50.958 28.8127 0.9869 0.04 10 0.4 3 18 651.8799 1.664493 53.279 29.6827 0.8823 0.05 10 0.55 1 19 695.3386 1.92115 50.958 28.8127 0.9869 0.04 10 0.55 1 19 695.3386 1.92115 50.958 28.8127 0.9869 0.04 10 0.55 1 19 695.3386 1.92115 50.958 28.8127 0.9869 0.04 10 0.77 2 23 892.878 2.122993 56.3792 25.677 0.9267 0.03 10 0.70 2 28 872.559 1.873829 56.9792 27.4311 0.909 0.04 10 0.70 2 28 872.559 1.873829 56.9792 27.5507 0.9267 0.03 10 0.70 2 28 892.8088 2.86803 0.9246 0.03 10 0.70 2 27 28 892.711 57.1476 28.8026 0.9544 0.03 10 0.71 2 28 875.669 2.08164 89.828 28.8063 0.9246 0.03 10 0.75 3 24 48.189 2.47879 1.58979 2.6677 0.9267 0.03 10 0.75 3 24 48.189 2.47879 1.58979 2.5677 0.9267 0.03 10 0.76 3 3 400.949 1.743571 4.1789 3.11779 0.6864 0.044 0.049 1.4888 2.2898 3.17841 0.9353 0.0224 0.0324 0.0324 1.4888 3.8688 3.8688 3.8688 3.9288 3.8688 0.9442 0.0224 0.033 0.056 0.0684 3.9898 3.9898 3.0684 0.0686 0.9488 0.0684 0.0686 3 1.											0.0675
70 0.15 3 3 3.555709 2.183993 5.19934 29.5881 0.8393 0.02 70 0.31 1 4 60.05197 3.522743 51.2359 23.7558 0.9156 0.03 70 0.31 2 5 84.54685 3.504614 54.5836 27.2998 0.9149 0.03 70 0.31 3 6 109.0417 3.442267 55.2661 28.412 0.9112 0.03 70 0.47 1 7 146.1791 4.821871 55.5287 25.5569 0.944 0.03 70 0.47 2 8 183.3165 4.770214 55.8252 25.549 0.937 0.02 70 0.47 3 9 220.4539 4.634579 54.9351 25.5287 25.559 0.944 0.03 70 0.63 1 10 270.2339 5.851957 52.6345 22.5959 0.951 0.02 70 0.63 1 10 270.2339 5.851957 52.6346 22.5959 0.951 0.02 70 0.63 3 11 320.0138 5.812757 58.4187 24.7065 0.9509 0.02 70 0.63 3 12 369.7937 5.872314 54.5329 23.8966 0.9528 0.02 70 0.79 1 13 432.2161 6.919107 54.0441 20.5884 0.9616 0.01 70 0.79 2 14 494.6336 6.919114 55.192 22.6778 0.9603 0.02 70 0.79 3 15 557.061 6.717521 58.7159 22.7817 0.9606 0.01 70 0.79 3 15 557.061 6.717521 58.7159 22.7817 0.9606 0.01 70 0.4 2 17 620.2736 1.680679 57.3794 30.7194 0.889 0.04 10 0.4 2 17 620.2736 1.680679 57.3794 30.7194 0.889 0.04 10 0.4 3 18 6518.799 1.664493 53.279 28.6827 0.8923 0.05 10 0.55 1 19 695.3366 1.92815 56.0958 28.1527 0.9089 0.04 10 0.55 2 20 738.7972 1.889471 57.1476 28.0226 0.9081 0.03 10 0.55 3 21 782.2559 1.873629 2.68079 27.4311 0.909 0.04 10 0.7 1 22 837.5669 2.088164 59.828 28.6603 0.9246 0.03 10 0.70 2 23 892.678 2.122993 56.3792 2.5677 0.9267 0.03 10 0.75 3 24 948.189 2.067364 56.3792 2.5677 0.9267 0.03 10 0.85 1 25 1015.352 2.277836 60.9335 2.1199 0.9355 0.02 10 0.76 3 392.678 2.245657 59.9621 28.2941 0.9355 0.02 10 0.77 3 24 948.189 2.067364 56.3792 2.5677 0.9369 0.04 10 0.7 1 22 837.5669 2.088164 59.828 28.6603 0.9246 0.03 10 0.85 3 27 1149.679 2.245557 59.9621 28.2941 0.9355 0.02 10 0.75 3 24 948.189 2.067364 56.3792 2.7931 0.9059 0.04 10 0.76 3 392.678 2.245657 59.9621 28.2941 0.9355 0.02 10 0.76 3 3 140.949 1.743571 41.9367 31.799 0.02 10 0.76 3 3 149.845 3.045 3											
TO											
70 0.31 2 5 84.54685 3.504814 54.8386 27.2988 0.9149 0.03 70 0.47 1 7 146.1791 4.821871 55.5287 25.3589 0.9424 0.0 70 0.47 2 8 183.3165 4.770214 55.5287 25.3589 0.9424 0.0 70 0.47 3 9 220.4539 4.634579 54.9351 25.2639 0.937 0.0 70 0.63 1 10 270.2339 5.851987 52.6348 22.5959 0.951 0.0 70 0.63 2 11 320.0138 5.812757 58.4187 24.7065 0.9509 0.0 70 0.63 3 11 320.0138 5.812757 58.4187 24.7065 0.9509 0.0 70 0.63 3 12 369.7937 5.872314 54.5329 23.8966 0.9528 0.0 70 0.63 3 12 369.7937 5.872314 54.5329 23.8966 0.9528 0.0 70 0.79 1 13 432.2161 6.919107 54.0441 20.5884 0.9616 0.0 70 0.79 2 14 494.6386 6.919114 55.192 22.6778 0.9623 0.0 70 0.79 3 15 557.061 6.717821 58.7159 22.7817 0.9606 0.0 71 0.0 4 1 16 588.6673 1.706557 53.395 27.1548 0.8885 0.0 71 0.0 4 2 17 620.2736 1.680679 57.3794 30.7194 0.889 0.0 71 0.0 4 2 17 620.2736 1.680679 57.3794 30.7194 0.889 0.0 71 0.0 55 1 19 695.3366 1.92815 56.0958 28.1527 0.9089 0.0 71 0.0 55 1 19 695.3366 1.92815 56.0958 28.1527 0.9089 0.0 71 0.0 55 2 20 738.792 1.889471 57.1476 28.0226 0.9081 0.0 71 0.0 7 1 22 837.5669 2.088164 59.828 28.8663 0.9246 0.03 71 0.0 7 2 23 892.678 2.122993 56.9799 27.4311 0.9090 0.0 71 0.0 85 1 25 1015.352 2.277836 6.0958 28.1527 0.9089 0.0 71 0.0 85 2 26 108.516 2.227836 6.0958 28.1527 0.9089 0.0 71 0.0 85 3 27 149.679 2.245857 59.9821 28.9941 0.0 71 0.0 85 3 27 149.679 2.245857 59.9821 28.9941 0.0 71 0.0 85 3 27 149.679 2.245857 59.9821 28.2941 0.9335 0.02 71 0.0 85 3 27 149.679 2.245857 59.9821 28.2941 0.9355 0.02 71 0.0 85 3 27 149.679 2.245857 59.9821 28.2941 0.9355 0.02 71 0.0 85 3 27 149.679 2.245857 59.9821 28.2941 0.9355 0.02 71 0.0 85 3 27 149.679 2.245857 59.9821 28.2941 0.9355 0.02 71 0.0 85 3 27 149.679 2.245857 59.9821 28.2941 0.9355 0.02 71 0.0 85 3 27 149.679 2.245857 59.9821 28.2941 0.9355 0.02 71 0.0 85 3 27 149.679 2.245857 59.9821 28.2941 0.9355 0.02 71 0.0 85 3 27 149.679 2.245857 59.9821 28.2941 0.9355 0.02 71 0.0 85 3 27 149.679 2.245857 59.9821 28.2941 0.9355 0.02 71 0.0 85 3 27 149.679 2.245857 59.9821 28.2941 0.9355 0.02 71 0.0 8											
70         0.31         3         6         109.0417         3.442257         55.2681         28.412         0.9412         0.03           70         0.47         2         8         183.3165         4.770214         55.8252         25.589         0.9424         0.0           70         0.47         2         8         183.3165         4.770214         55.8252         25.589         0.937         0.0           70         0.47         3         9         220.4539         4.634579         54.9351         25.26349         0.937         0.0           70         0.63         2         11         320.0138         5.812757         58.4187         24.7065         0.9509         0.02           70         0.79         1         13         432.2161         6.919114         51.5292         22.6778         0.9623         0.01           70         0.79         2         14         494.6386         6.919114         55.192         22.6778         0.9623         0.01           70         0.79         3         15         557.061         6.717521         58.7159         22.7781         0.960         0.01           10         0.4         1					-						
TO											
70											
70 0.47 3 9 9 220.4539 46.34579 54.9351 25.2639 0.9387 0.02 70 0.63 1 10 270.2339 5.851957 52.6345 22.5959 0.951 0.02 70 0.63 3 12 369.7937 5.872314 54.5229 23.8966 0.9528 0.02 70 0.79 1 13 432.2161 6.919107 54.0441 20.5884 0.9616 0.01 70 0.79 2 14 494.6386 6.919114 55.192 22.6778 0.9623 0.01 70 0.79 3 15 557.081 6.717521 58.7159 22.7817 0.9606 0.01 70 0.79 3 15 557.081 6.717521 58.7159 22.7817 0.9606 0.01 10 0.4 1 16 588.6673 1.706557 51.3835 27.1548 0.8885 0.04 11 0.4 2 17 620.2736 1.680679 57.3794 30.7194 0.889 0.04 11 0.4 3 18 651.8799 1.664493 53.279 9.6827 0.8823 0.05 11 0.055 1 19 695.3386 1.92815 56.0958 28.1527 0.9089 0.04 10 0.555 1 19 695.3386 1.92815 56.0958 28.1527 0.9089 0.04 10 0.55 1 12 2837.5669 2.08164 59.828 28.8603 0.9246 0.03 10 0.7 1 22 837.5669 2.08164 59.828 28.8603 0.9246 0.03 10 0.7 2 23 892.878 2.122993 56.3792 25.6970 9.0267 0.03 10 0.7 2 23 892.878 2.12293 56.3792 25.6970 0.9254 0.03 10 0.85 1 25 1015.352 2.277836 60.9353 26.1129 0.9359 0.02 10 0.85 3 27 1149.679 2.245657 59.9621 28.2941 0.9359 0.02 10 0.85 3 27 1149.679 2.245657 59.9621 28.2941 0.9359 0.02 10 0.85 3 27 1149.679 2.245657 59.9621 28.2941 0.9359 0.02 10 0.85 3 27 1349.679 2.245657 59.9621 28.2941 0.9359 0.02 10 0.06 1 31 1391.467 1.819057 43.8867 27.79793 0.6734 0.12 10 0.06 1 31 1391.467 1.819057 43.8867 27.79793 0.6734 0.12 10 0.145 1 3 30 1386.766 2.452829 61.9379 28.1479 0.9442 0.02 10 0.145 1 3 36 1435.321 2.994279 55.9265 32.2057 0.8682 0.05 10 0.06 2 32 1396.208 1.795079 44.7178 31.7791 0.9442 0.02 10 0.06 1 31 1391.467 1.819057 43.8867 27.9793 0.6734 0.12 10 0.06 1 31 1391.467 1.819057 43.8867 27.9793 0.6734 0.12 10 0.06 2 32 1396.208 1.795079 55.9465 32.2057 0.8686 0.006 10 0.04 2 44 1655.305 6.645643 59.8131 29.5968 0.9224 0.073 10 0.06 3 33 1400.949 1.743571 4.9367 31.0853 0.6224 0.073 10 0.06 1 31 1391.467 1.819057 43.8867 27.9793 0.6734 0.02 10 0.06 3 33 1400.949 1.743571 5.9962 29.7689 0.8655 0.056 10 0.04 2 4 1655.055 6.645643 59.8131 29.5968 0.9224 0.093 10 0.04 2 4 1655.055 6.645643 59.8131 29.5968 0.											0.025
70											0.028
70         0.63         2         11         320.0138         5.812757         58.4187         24.7085         0.9528         0.02           70         0.63         3         12         369.7937         5.872314         54.5329         23.8966         0.9928         0.02           70         0.79         1         13         432.2161         6.919107         54.0441         20.5884         0.9823         0.01           70         0.79         2         14         494.6386         6.919107         55.192         22.7817         0.9606         0.01           10         0.4         1         16         588.6673         1.706557         51.3835         27.1548         0.8865         0.04           10         0.4         2         17         620.2736         1.680679         57.3794         30.7194         0.8889         0.04           10         0.55         1         19         695,3386         1.92815         56.0958         28.1527         0.9089         0.04           10         0.55         2         738,7921         1.899471         57.1476         28.0226         0.9081         0.03           10         0.55         3         21					-						
70 0.63 3 12 369.7937 5.872314 54.5329 23.8966 0.9528 0.02 70 0.79 1 1 13 432.2161 6.919107 54.0441 20.5884 0.9616 0.01 70 0.79 2 14 494.6386 6.919114 55.192 22.6778 0.9623 0.01 70 0.79 3 15 557.061 6.717521 58.7159 22.7817 0.9606 0.01 10 0.4 1 16 588.6673 1.706557 51.3835 27.1548 0.8885 0.04 110 0.4 2 17 620.2736 1.680679 57.3794 30.7194 0.889 0.04 110 0.4 3 18 651.8799 1.664493 53.279 29.6827 0.8823 0.05 110 0.55 1 19 695.3336 1.92815 56.0958 28.1527 0.9089 0.04 110 0.55 2 20 738.7972 1.899471 57.1476 28.0226 0.9081 0.03 110 0.55 3 21 782.2559 1.873829 56.9709 27.4311 0.9099 0.04 110 0.07 1 22 837.5669 2.088164 59.828 28.8603 0.9246 0.03 110 0.7 2 23 892.878 2.122993 56.3792 25.677 0.9267 0.03 110 0.7 3 24 948.189 2.067364 56.3792 26.0962 0.9254 0.03 110 0.85 1 25 1015.352 2.277836 60.9353 26.1129 0.9359 0.02 110 0.85 3 27 1149.679 2.245657 59.9621 28.2941 0.9355 0.02 110 0.85 3 27 1149.679 2.245657 59.9621 28.2941 0.9355 0.02 110 1 1 28 1228.695 2.467307 59.5544 24.8666 0.9458 0.02 110 1 1 28 1228.695 2.467307 59.5544 24.8666 0.9458 0.02 110 1 1 28 1228.695 2.467307 59.5544 24.8666 0.9458 0.02 110 1 1 28 1228.695 2.467307 59.5544 24.8666 0.9458 0.02 110 0.06 1 31 1391.467 1.819057 34.8867 27.79793 0.6734 0.12 110 0.06 2 32 1396.081 1.743571 41.9367 31.4977 0.6821 0.12 110 0.145 3 36 1435.321 2.994279 55.9265 32.2057 0.9445 0.02 110 0.145 3 36 1435.321 2.994279 55.9265 32.2057 0.8166 0.07 110 0.04 2 41 1553.055 6.646643 59.833 31.7841 0.8181 0.07 110 0.04 3 41.12.406 3.050093 55.7372 31.0853 0.8224 0.07 110 0.04 3 41.12.406 4.67607 60.2619 29.7560 0.8655 0.056 110 0.04 3 42 1584.661 6.408 61.028 31.7841 0.9859 0.02 110 0.06 3 33 1400.949 1.743571 41.9367 31.4977 0.6821 0.12 110 0.06 3 33 1400.949 1.743571 41.9367 31.0853 0.8224 0.07 110 0.06 4 3 41.12.406 3.050093 55.7372 31.0853 0.8224 0.07 110 0.06 6 1 31 1.950.661 1.805307 58.2878 31.7841 0.9199 0.034 110 0.06 1 31 1.950.661 1.805307 58.2878 31.0853 0.8224 0.07 110 0.06 1 31 1.950.661 1.805307 58.2878 31.0853 0.8224 0.07 110 0.06 1 4 1 4 1635.231 1.77959 5											
70         0.79         1         13         432.2161         6.919107         54.0441         20.5884         0.9616         0.01           70         0.79         3         14         494.6386         6.919114         55.192         22.6778         0.9623         0.01           70         0.79         3         15         557.061         6.717521         55.192         22.6777         0.9606         0.01           10         0.4         1         16         588.6673         1.706557         51.3835         27.1548         0.8835         0.04           10         0.4         3         18         651.8799         1.684493         53.279         29.6827         0.8823         0.05           10         0.55         1         19         695.3386         1.92815         56.0958         28.1527         0.9989         0.04           10         0.55         3         21         782.2559         1.873829         56.9709         27.4311         0.909         0.04           10         0.7         1         22         387.5669         2.08164         56.3792         26.0962         0.9254         0.03           10         0.7         3											0.0222
70         0.79         2         14         494.6386         6.919114         55.192         22.8778         0.9623         0.01           70         0.79         3         15         557.061         6.717521         58.7159         22.7817         0.9606         0.01           10         0.4         1         16         588.6673         1.706557         51.3835         27.1548         0.8885         0.04           10         0.4         2         17         620.2736         1.680679         57.3794         30.7194         0.889         0.04           10         0.55         1         19         695.3386         1.92815         56.0988         28.1527         0.9089         0.04           10         0.55         2         20         738.7972         1.899471         57.1476         28.0226         0.9081         0.03           10         0.55         3         21         782.2559         1.873829         56.9709         27.4311         0.909         0.04           10         0.7         1         22         837.5669         2.08164         59.828         28.8603         0.9224         0.03           10         0.7         3											0.0207
70         0.79         3         15         557.061         6.717521         58.7159         22.7817         0.9606         0.01           10         0.4         1         16         588.6673         1.706575         51.3835         27.1548         0.8885         0.04           10         0.4         2         17         620.2736         1.680679         57.3794         30.7194         0.889         0.04           10         0.4         3         18         651.8799         1.664493         53.279         29.8627         0.9081         0.03           10         0.55         2         0.738.7972         1.899471         57.1476         28.0226         0.9081         0.03           10         0.55         3         21         782.2559         18.99471         57.1476         28.0226         0.9081         0.03           10         0.55         3         21         782.2559         8.088164         59.828         28.8603         0.9246         0.03           10         0.7         2         23         892.878         2.12293         56.3792         25.677         0.9267         0.03           10         0.85         1         25											0.0163
10											0.0166
10											0.0172
10											0.0478
10         0.55         1         19         695,3386         1.92815         56.0958         28.1527         0.9089         0.04           10         0.555         2         20         738.7972         1.899471         57.1476         28.0226         0.9081         0.03           10         0.555         3         21         782.2559         1.873829         56.9709         27.4311         0.909         0.04           10         0.7         1         22         837.5669         2.088164         59.828         28.8603         0.9246         0.03           10         0.7         2         23         892.878         2.122993         56.3792         25.677         0.9267         0.03           10         0.85         1         25         1015.352         2.277836         60.9353         26.1129         0.9359         0.02           10         0.85         2         26         1082.516         2.234364         57.9947         28.8706         0.9339         0.02           10         1         1         28         1228.695         2.467307         59.5544         24.8666         0.9458         0.02           10         1         1											0.0459
10         0.55         2         20         738.7972         1.899471         57.1476         28.0226         0.9081         0.03           10         0.55         3         21         782.2559         1.873829         56.9709         27.4311         0.909         0.04           10         0.7         1         22         837.5669         2.088164         59.828         28.8603         0.9267         0.03           10         0.7         2         23         892.878         2.122993         56.3792         25.677         0.9267         0.03           10         0.85         1         25         1015.352         2.277836         60.9353         26.1129         0.9359         0.03           10         0.85         2         26         1082.516         2.234364         57.9947         25.8706         0.9339         0.02           10         0.85         3         27         1149.679         2.245657         59.9621         28.9411         0.9355         0.02           10         1         2         29         1307.711         2.499221         62.7205         27.5507         0.9435         0.02           10         1         2											0.0509
10         0.55         3         21         782,2559         1.873829         56,9709         27,4311         0,909         0.04           10         0.77         1         22         837,5669         2.088164         59,628         28,8603         0,9246         0.03           10         0.77         3         24         948,189         2.067364         56,3792         25,677         0,9257         0.03           10         0.85         1         25         1015,352         2.277836         60,9353         26,1129         0,9359         0.02           10         0.85         2         26         1082,516         2.234364         57,9947         25,8706         0,9339         0.02           10         0.85         3         27         1149,679         2.245657         59,9621         28,2941         0,9359         0.02           10         1         1         28         1228,695         2.467307         59,5544         24,8666         0,9458         0.02           10         1         3         30         1386,726         2.452829         61,9379         28,1479         0,9442         0.02           10         1         31											0.0403
10         0.7         1         22         837.5669         2.088164         59.828         28.8603         0.9246         0.03           10         0.7         2         23         892.878         2.122993         56.3792         26.0767         0.9267         0.9267         0.03           10         0.85         1         25         1015.352         2.277836         60.9353         26.1129         0.9359         0.02           10         0.85         1         25         1015.352         2.277836         60.9353         26.1129         0.9359         0.02           10         0.85         3         27         1149.679         2.245657         59.9621         28.2941         0.9355         0.02           10         1         1         28         1228.695         2.467307         59.5544         24.8666         0.9458         0.02           10         1         1         2         29         1307.711         2.499221         62.7205         27.5507         0.9435         0.02           10         1         3         30         1386.726         2.452829         61.9379         28.1479         0.9442         0.02           100											0.0394
10         0.7         2         23         892.878         2.122993         56.3792         25.677         0.9267         0.03           10         0.7         3         24         948.189         2.067364         56.3792         26.0962         0.9254         0.03           10         0.85         1         25         1015.352         2.277836         60.9353         26.1129         0.9359         0.02           10         0.85         2         26         1082.516         2.234364         57.9947         25.8706         0.9339         0.02           10         0.85         3         27         1149.679         2.245657         59.9621         28.2941         0.9355         0.02           10         1         1         28         1228.695         2.467307         59.5544         24.8666         0.9458         0.02           10         1         2         29         1307.711         2.499221         62.7205         27.5507         0.9442         0.02           10         0         0.06         1         31         1391.467         1.819057         43.8867         27.9793         0.6734         0.12           100         0.06											0.0407
10         0.7         3         24         948.189         2.067364         56.3792         26.0962         0.9254         0.03           10         0.85         1         25         1015.352         2.277836         60.9353         26.1129         0.9359         0.02           10         0.85         2         26         1082.516         2.234364         57.9947         25.8706         0.9339         0.02           10         1         1         28         1228.695         2.467307         59.5544         24.8666         0.9458         0.02           10         1         1         28         1228.695         2.467307         59.5544         24.8666         0.9458         0.02           10         1         3         30         1386.726         2.452829         61.9379         28.1479         0.9442         0.02           100         0.06         1         31         1391.467         1.819057         43.8867         27.9793         0.6734         0.12           100         0.06         3         33         1400.949         1.743571         41.9367         31.4777         0.6821         0.12           100         0.145         1 <td></td> <td>0.0325</td>											0.0325
10         0.85         1         25         1015.352         2.277836         60.9353         26.1129         0.9359         0.02           10         0.85         2         26         1082.516         2.234364         57.9947         25.8706         0.9339         0.02           10         0.85         3         27         1149.679         2.245657         59.9621         28.2941         0.9355         0.02           10         1         1         28         1228.695         2.467307         59.5544         24.8666         0.9458         0.02           10         1         2         29         1307.711         2.499221         62.7205         27.5507         0.9435         0.02           10         0         1         31         1391.467         1.819057         43.8867         27.9793         0.6734         0.12           100         0.06         2         32         1396.208         1.795079         44.7178         31.4977         0.6821         0.12           100         0.046         3         33         1400.949         1.743571         41.9367         31.4977         0.6821         0.12           100         0.145         1											0.0318
10 0.85 2 26 1082.516 2.234364 57.9947 25.8706 0.9339 0.02 10 0.85 3 27 1149.679 2.245657 59.9621 28.2941 0.9355 0.021 10 1 1 28 1228.695 2.467307 59.5544 24.8666 0.9458 0.022 10 1 2 29 1307.711 2.499221 62.7205 27.5507 0.9435 0.021 10 1 3 30 1386.726 2.452829 61.9379 28.1479 0.9442 0.024 110 0.06 1 31 1391.467 1.819057 44.8667 27.9793 0.6734 0.122 110 0.06 2 32 1396.208 1.795079 44.7178 31.1779 0.6854 0.117 110 0.06 3 33 1400.949 1.743571 41.9367 31.4977 0.6821 0.122 110 0.145 1 34 1412.406 3.050093 55.7372 31.0853 0.8224 0.074 110 0.145 2 35 1423.864 3.024393 55.29883 31.7841 0.8181 0.0774 110 0.145 3 36 1435.321 2.984279 55.9265 32.2057 0.8166 0.0754 110 0.23 1 37 1453.495 4.213486 59.1371 30.6578 0.8732 0.0554 110 0.23 3 39 1489.842 4.143693 58.0294 29.7669 0.8655 0.0564 110 0.23 3 39 1489.842 4.143693 58.0294 29.7669 0.8655 0.0564 110 0.4 1 40 1521.448 6.467607 60.2619 28.5224 0.9195 0.033 110 0.4 2 41 1553.055 6.645643 59.8131 29.5968 0.9224 0.031 110 0.4 3 42 1584.661 6.408 61.0283 28.4155 0.9192 0.034 110 0.4 1 46 1699.234 1.779579 55.816 30.6342 0.8695 0.0564 110 0.32 2 44 1635.231 1.779579 55.816 30.8622 0.8646 0.0564 0.049 1 46 1699.234 2.1976979 59.7527 29.3753 0.8972 0.044 11 0.49 2 47 1737.951 2.191464 58.2094 29.7669 0.8555 0.0564 0.049 1 46 1689.234 2.197093 59.7527 29.3753 0.8972 0.044 11 0.049 2 47 1737.951 2.191464 58.2094 29.7669 0.8595 0.0564 0.066 1 49 1828.819 2.736057 58.9415 25.6724 0.9429 0.024 11 0.066 3 51 1933.12 2.504579 63.169 29.452 0.99229 0.033 11 0.066 3 51 1933.12 2.504579 63.169 29.452 0.99229 0.033 11 0.066 3 51 1933.12 2.504579 63.169 29.452 0.99229 0.033 11 0.066 3 51 1933.12 2.504579 63.169 29.452 0.99229 0.033 11 0.066 3 51 1933.12 2.504579 63.169 29.452 0.99229 0.033 11 0.066 3 51 1933.12 2.504579 63.169 29.452 0.99229 0.033 11 0.066 3 51 1933.12 2.504579 63.169 29.452 0.99229 0.033 11 0.083 3 54 2129.869 2.974129 57.8912 2.9452 0.99230 0.032 11 0.083 3 54 2129.869 2.974129 57.8912 2.504540 0.9355 0.028 11 1 2 2 56 2287.901 3.379264 66.2786 27.7106 0.9447 0.024											0.0325
10 0.85 3 27 1149.679 2.245657 59.9621 28.2941 0.9355 0.022   10 1 1 28 1228.695 2.467307 59.5544 24.8666 0.9458 0.022   10 1 2 29 1307.711 2.499221 62.7205 27.5507 0.9435 0.022   10 1 3 30 1386.726 2.452829 61.9379 28.1479 0.9442 0.024   10 0.06 1 31 1391.467 1.819057 43.8867 27.9793 0.6734 0.122   100 0.06 2 32 1396.208 1.795079 44.7178 31.1779 0.6854 0.113   100 0.06 3 33 1400.949 1.743571 41.9367 31.4977 0.6821 0.122   100 0.145 1 34 1412.406 3.050093 55.7372 31.0853 0.8224 0.074   100 0.145 2 35 1423.864 3.024393 52.9883 31.7841 0.8181 0.074   100 0.145 3 36 1435.321 2.984279 55.9265 32.2057 0.8166 0.075   100 0.23 1 37 1453.495 4.213486 59.1371 30.6578 0.8732 0.055   100 0.23 2 38 1471.668 4.210864 55.058 28.6067 0.8693 0.056   100 0.23 3 39 1489.842 4.143693 58.0294 29.7669 0.8665 0.056   100 0.4 1 40 1521.448 6.467607 60.2619 28.5224 0.9195 0.033   100 0.4 2 41 1553.055 6.645643 59.8131 29.5968 0.9224 0.034   100 0.4 3 42 1584.661 6.408 61.0283 28.4155 0.9192 0.034   100 0.4 3 42 1584.661 6.408 61.0283 30.6342 0.8695 0.056   100 0.4 3 42 1584.661 6.408 61.0283 30.6342 0.8695 0.056   100 0.4 3 42 1584.661 6.408 61.0283 30.6342 0.8695 0.056   100 0.4 9 2 47 1737.951 2.191464 58.2904 30.1162 0.8855 0.056   100 0.49 1 46 1699.234 2.197093 59.7527 29.3753 0.8972 0.044   0.49 2 47 1737.951 2.191464 58.2904 30.1162 0.8955 0.046   10 0.49 3 48 1776.669 2.348507 52.6866 27.7137 0.8911 0.04   0.66 1 49 1828.819 2.736057 52.6866 27.7137 0.8911 0.04   0.66 2 50 1880.97 2.530343 63.2393 29.452 0.9429 0.023   100 0.66 2 50 1880.97 2.530343 63.2393 29.452 0.9429 0.023   100 0.66 2 50 1880.97 2.530343 60.5353 26.5314 0.9323 0.028   10 0.83 3 54 2129.869 2.976129 57.8912 25.6724 0.9429 0.024   10 0.66 2 50 2287.901 3.379264 66.2786 27.7106 0.9447 0.024   11 55 2208.885 3.334679 59.3173 26.8898 0.9333 0.028   10 0.83 3 54 2129.869 2.976129 57.8912 25.69543 0.9355 0.028   10 0.83 3 54 2129.869 2.974129 57.8912 25.69543 0.9355 0.028   10 0.83 3 54 2129.869 2.976129 57.8912 25.69543 0.9355 0.028   10 0.83 3 54 2129.869 2.97									26.1129	0.9359	0.0279
10         1         1         28         1228.695         2.467307         59.5544         24.8666         0.9458         0.02           10         1         2         29         1307.711         2.499221         62.7205         27.5507         0.9435         0.02           10         1         3         30         1386.726         2.452829         61.9379         28.1479         0.9442         0.02           100         0.06         1         31         1391.467         1.819057         43.8667         27.9793         0.6734         0.12           100         0.06         2         32         1396.208         1.795079         44.7178         31.1779         0.6854         0.11           100         0.145         1         34         1412.406         3.050093         55.7372         31.0853         0.8224         0.07           100         0.145         2         35         1423.864         3.024393         52.9883         31.7841         0.8181         0.07           100         0.145         3         36         1435.321         2.984279         55.9265         32.2057         0.8166         0.075           100         0.23									25.8706	0.9339	0.0276
10         1         2         29         1307.711         2.499221         62.7205         27.5507         0.9435         0.021           10         1         3         30         1386.726         2.452829         61.9379         28.1479         0.9442         0.024           100         0.06         1         31         1391.467         18.19057         43.8867         27.9793         0.6734         0.12           100         0.06         2         32         1396.208         1.795079         44.7178         31.1779         0.6854         0.117           100         0.06         3         33         1400.949         1.743571         41.9367         31.4977         0.6821         0.122           100         0.145         1         34         1412.406         3.050093         55.7372         31.0853         0.8224         0.074           100         0.145         3         36         1435.321         2.984279         55.9265         32.2057         0.8166         0.073           100         0.23         1         37         1453.495         4.213486         59.1371         30.6578         0.8732         0.056           100         0.23								59.9621	28.2941	0.9355	0.0282
10         1         3         30         1386.726         2.452829         61.9379         28.1479         0.9442         0.02           100         0.06         1         31         1391.467         1.819057         43.8867         27.9793         0.6734         0.12           100         0.06         2         32         1396.208         1.795079         44.7178         31.1779         0.6854         0.11           100         0.06         3         33         1400.949         1.743571         41.9367         31.4977         0.6821         0.12           100         0.145         1         34         1412.406         3.050093         55.7372         31.0853         0.8224         0.07           100         0.145         2         35         1423.864         3.024393         52.9883         31.7841         0.8181         0.07           100         0.145         3         36         1435.321         2.984279         55.9265         32.2057         0.8166         0.07           100         0.23         1         37         1453.495         4.213666         59.1371         30.6578         0.8655         0.05           100         0.23									24.8666	0.9458	0.0242
100         0.06         1         31         1391.467         1.819057         43.8867         27.9793         0.6734         0.12           100         0.06         2         32         1396.208         1.795079         44.7178         31.1779         0.6854         0.117           100         0.06         3         33         1400.949         1.743571         41.9367         31.4977         0.6821         0.124           100         0.145         1         34         1412.406         3.05093         55.7372         31.0853         0.8224         0.07           100         0.145         2         35         1423.864         3.024393         52.9853         31.7841         0.8181         0.07           100         0.145         3         36         1435.321         2.984279         55.9265         32.2057         0.8166         0.075           100         0.23         1         37         1453.495         4.213486         59.1371         30.6578         0.8732         0.056           100         0.23         3         39         1489.842         4.143693         58.0294         29.7669         0.8655         0.056           100         0.4							2.499221	62.7205	27.5507	0.9435	0.0251
100         0.06         2         32         1396.208         1.795079         44.7178         31.1779         0.6854         0.111           100         0.06         3         33         1400.949         1.743571         41.9367         31.4977         0.6821         0.124           100         0.145         1         34         1412.406         3.050093         55.7372         31.0853         0.8224         0.074           100         0.145         2         35         1423.864         3.024393         52.9883         31.7841         0.8181         0.075           100         0.145         3         36         1435.321         2.984279         55.9265         32.2057         0.8166         0.075           100         0.23         1         37         1453.495         4.213486         59.1371         30.6578         0.8732         0.055           100         0.23         2         38         1471.668         4.210864         55.058         28.6067         0.8693         0.056           100         0.4         1         40         1521.448         6.457607         60.2619         28.5224         0.9195         0.032           100         0								61.9379	28.1479	0.9442	0.0249
100 0.06 3 33 1400.949 1.743571 41.9367 31.4977 0.6821 0.122 100 0.145 1 34 1412.406 3.050093 55.7372 31.0853 0.8224 0.074 100 0.145 2 35 1423.864 3.024393 52.9883 31.7841 0.8181 0.078 100 0.145 3 36 1435.321 2.984279 55.9265 32.2057 0.8166 0.075 100 0.23 1 37 1453.495 4.213486 59.1371 30.6578 0.8732 0.055 100 0.23 2 38 1471.668 4.210864 55.058 28.6067 0.8693 0.056 100 0.23 3 39 1489.842 4.143693 58.0294 29.7669 0.8655 0.055 100 0.4 1 40 1521.448 6.467607 60.2619 28.5224 0.9195 0.033 100 0.4 2 41 1553.055 6.645643 59.8131 29.5968 0.9224 0.031 100 0.4 3 42 1584.661 6.408 61.0283 28.4155 0.9192 0.034 100 0.32 1 43 1609.946 1.810236 59.0438 30.6342 0.8695 0.056 100 0.32 1 43 1609.946 1.810236 59.0438 30.6342 0.8695 0.056 100 0.32 2 44 1635.231 1.779579 55.081 30.8622 0.8646 0.056 100 0.32 3 45 1660.516 1.805307 58.2978 29.7072 0.8596 0.056 100 0.49 1 46 1699.234 2.197093 59.7527 29.3753 0.8972 0.044 10 0.49 1 46 1699.234 2.197093 59.7527 29.3753 0.8972 0.044 10 0.49 1 46 1699.234 2.197093 59.7527 29.3753 0.8972 0.044 10 0.49 1 46 1699.234 2.197093 59.7527 29.3753 0.8972 0.044 10 0.49 1 48 1776.669 2.348507 52.6866 27.7137 0.8911 0.04 10 0.66 1 49 1828.819 2.736057 58.9415 25.6724 0.9429 0.024 10 0.66 1 49 1828.819 2.736057 58.9415 25.6724 0.9429 0.024 10 0.66 2 50 1880.97 2.550343 63.2393 29.452 0.9229 0.033 10 0.66 3 51 1933.12 2.504579 63.169 29.4751 0.9198 0.034 10 0.66 3 51 1933.12 2.504579 63.169 29.4751 0.9198 0.034 10 0.63 2 53 2064.286 2.998536 60.5353 26.5314 0.9323 0.029 10 0.83 3 54 2129.869 2.974129 57.8912 26.9543 0.9323 0.029 10 0.034 10 0.83 3 54 2129.869 2.974129 57.8912 26.9543 0.9335 0.028 10 0.024 10 0.83 3 54 2129.869 2.974129 57.8912 26.9543 0.9335 0.028 10 0.024 10 0.83 3 54 2129.869 2.974129 57.8912 26.9543 0.9335 0.028 10 0.024 10 0.83 3 54 2129.869 2.974129 57.8912 26.9543 0.9335 0.028 10 0.024 10 0.83 3 54 2129.869 2.974129 57.8912 26.9543 0.9335 0.028 10 0.024 10 0.83 3 54 2129.869 2.974129 57.8912 26.9543 0.9335 0.028 10 0.024 10 0.83 3 54 2129.869 2.974129 57.8912 26.9543 0.9335 0.028								43.8867	27.9793	0.6734	0.1241
100         0.145         1         34         1412.406         3.050093         55.7372         31.0853         0.8224         0.074           100         0.145         2         35         1423.864         3.024393         52.9883         31.7841         0.8181         0.076           100         0.145         3         36         1435.321         2.984279         55.9265         32.2057         0.8166         0.075           100         0.23         1         37         1453.495         4.213486         59.1371         30.6578         0.8732         0.052           100         0.23         2         38         1471.668         4.210864         55.058         28.6067         0.8693         0.056           100         0.23         3         39         1489.842         4.143693         58.0294         29.7669         0.8655         0.056           100         0.4         1         40         1521.448         6.467607         60.2619         28.5224         0.9195         0.032           100         0.4         2         41         1553.055         6.645643         59.8131         29.5968         0.9224         0.031           100         0.							1.795079	44.7178	31.1779	0.6854	0.1178
100         0.145         2         35         1423.864         3.024393         52.9883         31.7841         0.8181         0.078           100         0.145         3         36         1435.321         2.984279         55.9265         32.2057         0.8166         0.078           100         0.23         1         37         1453.495         4.213486         59.1371         30.6578         0.8732         0.052           100         0.23         2         38         1471.668         4.210864         55.058         28.6067         0.8693         0.056           100         0.23         3         39         1489.842         4.143693         58.0294         29.7669         0.8655         0.056           100         0.4         1         40         1521.448         6.467607         60.2619         28.5224         0.9195         0.032           100         0.4         2         41         1553.055         6.645643         59.8131         29.5968         0.9224         0.031           100         0.4         3         42         1584.661         6.408         61.0283         28.4155         0.9192         0.032           40         0.32 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>1.743571</td> <td>41.9367</td> <td>31.4977</td> <td>0.6821</td> <td>0.1249</td>							1.743571	41.9367	31.4977	0.6821	0.1249
100         0.145         3         36         1435.321         2.984279         55.9265         32.2057         0.8166         0.075           100         0.23         1         37         1453.495         4.213486         59.1371         30.6578         0.8732         0.052           100         0.23         2         38         1471.668         4.210864         55.058         28.6067         0.8693         0.056           100         0.23         3         39         1489.842         4.143693         58.0294         29.7669         0.8655         0.058           100         0.4         1         40         1521.448         6.467607         60.2619         28.5224         0.9195         0.033           100         0.4         2         41         1553.055         6.645643         59.8131         29.5968         0.9224         0.031           100         0.4         3         42         1584.661         6.408         61.0283         28.4155         0.9192         0.032           40         0.32         1         43         1609.946         1.810236         59.0438         30.6342         0.8695         0.058           40         0.32							3.050093	55.7372	31.0853	0.8224	0.0743
100         0.23         1         37         1453.495         4.213486         59.1371         30.6578         0.8732         0.052           100         0.23         2         38         1471.668         4.210864         55.058         28.6067         0.8693         0.056           100         0.23         3         39         1489.842         4.143693         58.0294         29.7669         0.8655         0.058           100         0.4         1         40         1521.448         6.467607         60.2619         28.5224         0.9195         0.033           100         0.4         2         41         1553.055         6.645643         59.8131         29.5968         0.9224         0.031           100         0.4         3         42         1584.661         6.408         61.0283         28.4155         0.9192         0.032           40         0.32         1         43         1609.946         1.810236         59.0438         30.6342         0.8695         0.054           40         0.32         2         44         1635.231         1.779579         55.081         30.8622         0.8646         0.056           40         0.49								52.9883	31.7841	0.8181	0.0785
100         0.23         2         38         1471.668         4.210864         55.058         28.6067         0.8693         0.056           100         0.23         3         39         1489.842         4.143693         58.0294         29.7669         0.8655         0.058           100         0.4         1         40         1521.448         6.467607         60.2619         28.5224         0.9195         0.033           100         0.4         2         41         1553.055         6.645643         59.8131         29.5968         0.9224         0.031           100         0.4         3         42         1584.661         6.408         61.0283         28.4155         0.9192         0.032           40         0.32         1         43         1609.946         1.810236         59.0438         30.6342         0.8695         0.054           40         0.32         2         44         1635.231         1.779579         55.081         30.8622         0.8646         0.056           40         0.32         3         45         1660.516         1.805307         58.2978         29.7072         0.8596         0.058           40         0.49							2.984279	55.9265	32.2057	0.8166	0.0796
100         0.23         3         39         1489.842         4.143693         58.0294         29.7669         0.8655         0.058           100         0.4         1         40         1521.448         6.467607         60.2619         28.5224         0.9195         0.033           100         0.4         2         41         1553.055         6.645643         59.8131         29.5968         0.9224         0.031           100         0.4         3         42         1584.661         6.408         61.0283         28.4155         0.9192         0.032           40         0.32         1         43         1609.946         1.810236         59.0438         30.6342         0.8695         0.054           40         0.32         2         44         1635.231         1.779579         55.081         30.8622         0.8646         0.056           40         0.32         3         45         1660.516         1.805307         58.2978         29.7072         0.8596         0.058           40         0.49         1         46         1699.234         2.197093         59.7527         29.3753         0.8972         0.044           40         0.49							4.213486	59.1371	30.6578	0.8732	0.0526
100         0.4         1         40         1521.448         6.467607         60.2619         28.5224         0.9195         0.033           100         0.4         2         41         1553.055         6.645643         59.8131         29.5968         0.9224         0.031           100         0.4         3         42         1584.661         6.408         61.0283         28.4155         0.9192         0.032           40         0.32         1         43         1609.946         1.810236         59.0438         30.6342         0.8695         0.054           40         0.32         2         44         1635.231         1.779579         55.081         30.8622         0.8646         0.056           40         0.32         3         45         1660.516         1.805307         58.2978         29.7072         0.8596         0.056           40         0.49         1         46         1699.234         2.197093         59.7527         29.3753         0.8972         0.044           40         0.49         2         47         1737.951         2.191464         58.2904         30.1162         0.8955         0.045           40         0.49									28.6067	0.8693	0.0568
100         0.4         2         41         1553.055         6.645643         59.8131         29.5968         0.9224         0.031           100         0.4         3         42         1584.661         6.408         61.0283         28.4155         0.9192         0.032           40         0.32         1         43         1609.946         1.810236         59.0438         30.6342         0.8695         0.054           40         0.32         2         44         1635.231         1.779579         55.081         30.8622         0.8646         0.056           40         0.32         3         45         1660.516         1.805307         58.2978         29.7072         0.8596         0.056           40         0.49         1         46         1699.234         2.197093         59.7527         29.3753         0.8972         0.044           40         0.49         2         47         1737.951         2.191464         58.2904         30.1162         0.8955         0.045           40         0.49         3         48         1776.669         2.348507         52.6866         27.7137         0.8911         0.04           40         0.66							4.143693	58.0294	29.7669	0.8655	0.0595
100         0.4         3         42         1584.661         6.408         61.0283         28.4155         0.9192         0.032           40         0.32         1         43         1609.946         1.810236         59.0438         30.6342         0.8695         0.054           40         0.32         2         44         1635.231         1.779579         55.081         30.8622         0.8646         0.056           40         0.32         3         45         1660.516         1.805307         58.2978         29.7072         0.8596         0.056           40         0.49         1         46         1699.234         2.197093         59.7527         29.3753         0.8972         0.045           40         0.49         2         47         1737.951         2.191464         58.2904         30.1162         0.8955         0.045           40         0.49         3         48         1776.669         2.348507         52.6866         27.7137         0.8911         0.04           40         0.66         1         49         1828.819         2.736057         58.9415         25.6724         0.9429         0.024           40         0.66										0.9195	0.0339
40       0.32       1       43       1609.946       1.810236       59.0438       30.6342       0.8695       0.054         40       0.32       2       44       1635.231       1.779579       55.081       30.8622       0.8646       0.056         40       0.32       3       45       1660.516       1.805307       58.2978       29.7072       0.8596       0.058         40       0.49       1       46       1699.234       2.197093       59.7527       29.3753       0.8972       0.045         40       0.49       2       47       1737.951       2.191464       58.2904       30.1162       0.8955       0.045         40       0.49       3       48       1776.669       2.348507       52.6866       27.7137       0.8911       0.04         40       0.66       1       49       1828.819       2.736057       58.9415       25.6724       0.9429       0.024         40       0.66       2       50       1880.97       2.530343       63.2393       29.452       0.9229       0.033         40       0.83       1       52       1998.703       2.964393       61.4156       27.2456       0.9353 <t< td=""><td></td><td></td><td></td><td>_</td><td>41</td><td>1553.055</td><td></td><td>59.8131</td><td>29.5968</td><td>0.9224</td><td>0.0315</td></t<>				_	41	1553.055		59.8131	29.5968	0.9224	0.0315
40       0.32       2       44       1635.231       1.779579       55.081       30.8622       0.8646       0.056         40       0.32       3       45       1660.516       1.805307       58.2978       29.7072       0.8596       0.058         40       0.49       1       46       1699.234       2.197093       59.7527       29.3753       0.8972       0.044         40       0.49       2       47       1737.951       2.191464       58.2904       30.1162       0.8955       0.045         40       0.49       3       48       1776.669       2.348507       52.6866       27.7137       0.8911       0.04         40       0.66       1       49       1828.819       2.736057       58.9415       25.6724       0.9429       0.024         40       0.66       2       50       1880.97       2.530343       63.2393       29.452       0.9229       0.033         40       0.66       3       51       1933.12       2.504579       63.169       29.4751       0.9198       0.034         40       0.83       1       52       1998.703       2.964393       61.4156       27.2456       0.9353	•			3	42		6.408	61.0283	28.4155	0.9192	0.0343
40 0.32 3 45 1660.516 1.805307 58.2978 29.7072 0.8596 0.058 40 0.49 1 46 1699.234 2.197093 59.7527 29.3753 0.8972 0.044 40 0.49 2 47 1737.951 2.191464 58.2904 30.1162 0.8955 0.045 40 0.49 3 48 1776.669 2.348507 52.6866 27.7137 0.8911 0.04 40 0.66 1 49 1828.819 2.736057 58.9415 25.6724 0.9429 0.024 40 0.66 2 50 1880.97 2.530343 63.2393 29.452 0.9229 0.033 40 0.66 3 51 1933.12 2.504579 63.169 29.4751 0.9198 0.034 40 0.83 1 52 1998.703 2.964393 61.4156 27.2456 0.9353 0.028 40 0.83 2 53 2064.286 2.998536 60.5353 26.5314 0.9323 0.029 40 0.83 3 54 2129.869 2.974129 57.8912 26.9543 0.9355 0.028 40 1 1 55 2208.885 3.334679 59.3173 26.1898 0.9434 0.024 40 1 2 56 2287.901 3.379264 66.2786 27.7106 0.9447 0.024					43	1609.946	1.810236	59.0438	30.6342	0.8695	0.0546
40       0.32       3       45       1660.516       1.805307       58.2978       29.7072       0.8596       0.058         40       0.49       1       46       1699.234       2.197093       59.7527       29.3753       0.8972       0.044         40       0.49       2       47       1737.951       2.191464       58.2904       30.1162       0.8955       0.045         40       0.49       3       48       1776.669       2.348507       52.6866       27.7137       0.8911       0.04         40       0.66       1       49       1828.819       2.736057       58.9415       25.6724       0.9429       0.024         40       0.66       2       50       1880.97       2.530343       63.2393       29.452       0.9229       0.033         40       0.66       3       51       1933.12       2.504579       63.169       29.4751       0.9198       0.034         40       0.83       1       52       1998.703       2.964393       61.4156       27.2456       0.9353       0.028         40       0.83       2       53       2064.286       2.998536       60.5353       26.5314       0.9323 <td< td=""><td></td><td></td><td></td><td>2</td><td>44</td><td>1635.231</td><td></td><td>55.081</td><td>30.8622</td><td>0.8646</td><td>0.0564</td></td<>				2	44	1635.231		55.081	30.8622	0.8646	0.0564
40       0.49       1       46       1699.234       2.197093       59.7527       29.3753       0.8972       0.044         40       0.49       2       47       1737.951       2.191464       58.2904       30.1162       0.8955       0.045         40       0.49       3       48       1776.669       2.348507       52.6866       27.7137       0.8911       0.04         40       0.66       1       49       1828.819       2.736057       58.9415       25.6724       0.9429       0.024         40       0.66       2       50       1880.97       2.530343       63.2393       29.452       0.9229       0.033         40       0.66       3       51       1933.12       2.504579       63.169       29.4751       0.9198       0.034         40       0.83       1       52       1998.703       2.964393       61.4156       27.2456       0.9353       0.028         40       0.83       2       53       2064.286       2.998536       60.5353       26.5314       0.9323       0.029         40       0.83       3       54       2129.869       2.974129       57.8912       26.9543       0.9355 <td< td=""><td></td><td></td><td>0.32</td><td>3</td><td>45</td><td>1660.516</td><td>1.805307</td><td>58.2978</td><td>29.7072</td><td>0.8596</td><td>0.0584</td></td<>			0.32	3	45	1660.516	1.805307	58.2978	29.7072	0.8596	0.0584
40       0.49       2       47       1737.951       2.191464       58.2904       30.1162       0.8955       0.045         40       0.49       3       48       1776.669       2.348507       52.6866       27.7137       0.8911       0.04         40       0.66       1       49       1828.819       2.736057       58.9415       25.6724       0.9429       0.024         40       0.66       2       50       1880.97       2.530343       63.2393       29.452       0.9229       0.033         40       0.66       3       51       1933.12       2.504579       63.169       29.4751       0.9198       0.034         40       0.83       1       52       1998.703       2.964393       61.4156       27.2456       0.9353       0.028         40       0.83       2       53       2064.286       2.998536       60.5353       26.5314       0.9323       0.029         40       0.83       3       54       2129.869       2.974129       57.8912       26.9543       0.9355       0.028         40       1       1       55       2208.885       3.334679       59.3173       26.1898       0.9434       0.				1	46	1699.234	2.197093	59.7527	29.3753	0.8972	0.0443
40       0.49       3       48       1776.669       2.348507       52.6866       27.7137       0.8911       0.04         40       0.66       1       49       1828.819       2.736057       58.9415       25.6724       0.9429       0.024         40       0.66       2       50       1880.97       2.530343       63.2393       29.452       0.9229       0.033         40       0.66       3       51       1933.12       2.504579       63.169       29.4751       0.9198       0.034         40       0.83       1       52       1998.703       2.964393       61.4156       27.2456       0.9353       0.028         40       0.83       2       53       2064.286       2.998536       60.5353       26.5314       0.9323       0.029         40       0.83       3       54       2129.869       2.974129       57.8912       26.9543       0.9355       0.028         40       1       1       55       2208.885       3.334679       59.3173       26.1898       0.9434       0.024         40       1       2       56       2287.901       3.379264       66.2786       27.7106       0.9447       0.024			0.49		47		2.191464	58.2904	30.1162	0.8955	0.0455
40       0.66       1       49       1828.819       2.736057       58.9415       25.6724       0.9429       0.024         40       0.66       2       50       1880.97       2.530343       63.2393       29.452       0.9229       0.033         40       0.66       3       51       1933.12       2.504579       63.169       29.4751       0.9198       0.034         40       0.83       1       52       1998.703       2.964393       61.4156       27.2456       0.9353       0.028         40       0.83       2       53       2064.286       2.998536       60.5353       26.5314       0.9323       0.029         40       0.83       3       54       2129.869       2.974129       57.8912       26.9543       0.9355       0.028         40       1       1       55       2208.885       3.334679       59.3173       26.1898       0.9434       0.024         40       1       2       56       2287.901       3.379264       66.2786       27.7106       0.9447       0.024		40	0.49	3	48	1776.669	2.348507	52.6866	27.7137		0.047
40       0.66       2       50       1880.97       2.530343       63.2393       29.452       0.9229       0.033         40       0.66       3       51       1933.12       2.504579       63.169       29.4751       0.9198       0.034         40       0.83       1       52       1998.703       2.964393       61.4156       27.2456       0.9353       0.028         40       0.83       2       53       2064.286       2.998536       60.5353       26.5314       0.9323       0.029         40       0.83       3       54       2129.869       2.974129       57.8912       26.9543       0.9355       0.028         40       1       1       55       2208.885       3.334679       59.3173       26.1898       0.9434       0.024         40       1       2       56       2287.901       3.379264       66.2786       27.7106       0.9447       0.024		40	0.66	1	49	1828.819	2.736057	58.9415			0.0245
40       0.66       3       51       1933.12       2.504579       63.169       29.4751       0.9198       0.034         40       0.83       1       52       1998.703       2.964393       61.4156       27.2456       0.9353       0.028         40       0.83       2       53       2064.286       2.998536       60.5353       26.5314       0.9323       0.029         40       0.83       3       54       2129.869       2.974129       57.8912       26.9543       0.9355       0.028         40       1       1       55       2208.885       3.334679       59.3173       26.1898       0.9434       0.024         40       1       2       56       2287.901       3.379264       66.2786       27.7106       0.9447       0.024		40	0.66	2	50	1880.97	2.530343	63.2393	29.452		0.0335
40       0.83       1       52       1998.703       2.964393       61.4156       27.2456       0.9353       0.028         40       0.83       2       53       2064.286       2.998536       60.5353       26.5314       0.9323       0.029         40       0.83       3       54       2129.869       2.974129       57.8912       26.9543       0.9355       0.028         40       1       1       55       2208.885       3.334679       59.3173       26.1898       0.9434       0.024         40       1       2       56       2287.901       3.379264       66.2786       27.7106       0.9447       0.024			0.66	3	51	1933.12	2.504579	63.169			0.0347
40       0.83       2       53       2064.286       2.998536       60.5353       26.5314       0.9323       0.029         40       0.83       3       54       2129.869       2.974129       57.8912       26.9543       0.9355       0.028         40       1       1       55       2208.885       3.334679       59.3173       26.1898       0.9434       0.024         40       1       2       56       2287.901       3.379264       66.2786       27.7106       0.9447       0.024					52	1998.703	2.964393				0.0281
40       0.83       3       54       2129.869       2.974129       57.8912       26.9543       0.9355       0.028         40       1       1       55       2208.885       3.334679       59.3173       26.1898       0.9434       0.024         40       1       2       56       2287.901       3.379264       66.2786       27.7106       0.9447       0.024					53	2064.286					0.0299
40 1 1 55 2208.885 3.334679 59.3173 26.1898 0.9434 0.024 40 1 2 56 2287.901 3.379264 66.2786 27.7106 0.9447 0.024			0.83	3	54	2129.869	2.974129				0.0283
40 1 2 56 2287.901 3.379264 66.2786 27.7106 0.9447 0.024			1		55	2208.885	3.334679				0.0243
40 4 0 5 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6			1		56						0.0247
		40	1	3	57	2366.917	3.382593	60.0479	26.8645	0.9429	0.0254

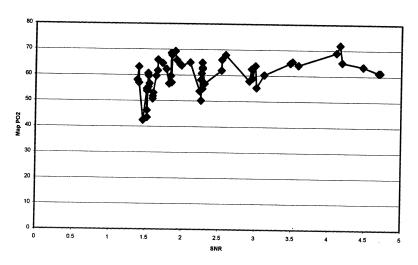






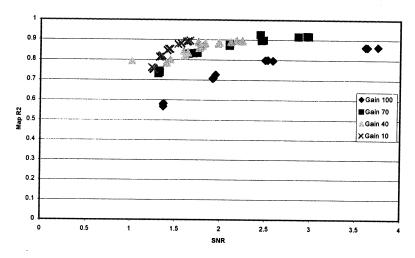
Gain		Exposure 16	Relative Im Cum	nulative	: Accumulat	SNR	PO2 Mean	PO2 St De	R2 Mean	R2 St Dev
	70	0.15	1	1			53.1055	31.2113	0.7796	0.0958
	70	0.15	2	2		1.595314		31.4954	0.7855	0.0855
	70	0.15	3	3		1.596586	51.7846	31.5816	0.7755	0.0033
	70	0.31	1	4		2.254757	58.2223	30.8665	0.8733	0.0523
	70	0.31	2	5		2.304921	56.7583	31.9849	0.8764	0.0506
	70	0.31	3	6	109.0417	2.263214	60.7205	32.3248	0.8716	
	70	0.47	1	7	146.1791	2.948257	62.5186	28.8582		0.0539
	70	0.47	2	8	183.3165	2.997514	63.8171		0.9135	0.0357
	70	0.47	3	9		2.959307	58.8974	28.6885	0.9109	0.0378
	70	0.63	1	10		3.504579	65.4751	27.8418	0.9704	0.0394
	70	0.63	2	11	320.0138			27.5211	0.9207	0.0336
	70	0.63	3	12	369.7937	3.58575	64.0734	29.6804	0.9274	0.031
	70	0.79	1	13		3.476564 4.185393	64.9139	28.3856	0.9236	0.035
	70	0.79	2	14			65.2427	26.7321	0.9431	0.0242
	70	0.79	3	15		4.155964	71.8692	29.7798	0.9411	0.0255
	10	0.79	1		557.061	4.1066	68.9786	28.9941	0.9386	0.0264
	10	0.4	2	16	588.6673	1.405007	56.9862	30.383	0.8439	0.0667
	10	0.4	3	17	620.2736	1.404493	63.1363	33.5966	0.8376	0.0703
	10			18	651.8799	1.384143	58.1358	32.4402	0.8272	0.0752
		0.55	1	19	695.3386	1.550057	56.6854	28.6073	0.8759	0.0512
	10	0.55	2	20	738.7972	1.531629	60.6583	30.9949	0.8671	0.0597
	10	0.55	3	21	782.2559	1.538971	59.6844	30.2792	0.8735	0.0544
	10	0.7	1	22	837.5669	1.643686	59.6811	29.8847	0.89	0.0483
	10	0.7	2	23	892.878	1.665157	65.9298	30.6777	0.8948	0.0455
	10	. 0.7	3	24	948.189	1.662371	61.7208	28.3624	0.8953	0.0462
	10	0.85	1	25	1015.352	1.848643	68.5813	31.0531	0.9189	0.0346
	10	0.85	2	26	1082.516	1.782129	62.3568	28.7479	0.9066	0.0421
	10	0.85	3	27	1149.679	1.729321	64.6265	30.2779	0.9024	0.0443
	10	1	1	28	1228.695	1.859807	67.7337	30.3843	0.9136	0.0379
	10	1	2	29	1307.711	1.92155	65.8236	29.9062	0.9166	0.0363
	10	1	3	30	1386.726	1.9013	69.2661	30.9281	0.9178	0.0364
	100	0.06	1	31	1391.467	1.5174	43.5161	33.4359	0.6218	0.142
	100	0.06	2	32	1396.208	1.462521	42.4348	32.1801	0.6088	0.152
	100	0.06	3	33	1400.949	1.516171	46.245	30.5128	0.6297	0.1435
	100	0.145	1	34	1412.406	2.273757	54.7378	32.7368	0.7662	0.1007
	100	0.145	2	35	1423.864	2.257286	50.1788	30.7761	0.762	0.0972
	100	0.145	3	36	1435.321	2.236279	53.8048	33.1385	0.7456	0.1092
	100	0.23	1	37	1453.495	3.01475	55.2714	31.0975	0.8242	0.0734
	100	0.23	2	38	1471.668	2.9164	57.8654	32.2111	0.8114	0.0806
	100	0.23	3	39	1489.842	3.1197	60.2691	33.0445	0.8338	0.0721
	100	0.4	1	40	1521.448	4.712071	61.2496	29.8165	0.8912	0.0443
	100	0.4	2	41	1553.055	4.688257	61.2809	28.1974	0.8961	0.0454
1	100	0.4	3	42	1584.661	4.473707	63.6176	31.8991	0.8852	0.0487
	40	0.32	1	43	1609.946	1.5368	55.4042	29.0272	0.8246	0.0734
	40	0.32	2	44	1635.231	1.517071	53.8511	31.9076	0.8132	0.0785
	40	0.32	3	45	1660.516	1.516057	54.6924	32.7898	0.8088	0.0804
	40	0.49	1	46	1699.234	1.842079	59.6334	31.9336	0.8737	0.0535
	40	0.49	2	47	1737.951	1.819757	56.709	30.7449	0.8594	0.0594
	40	0.49	3	48	1776.669	1.851507	57.1019	30.4113	0.8525	0.0635
	40	0.66	1	49		2.104943	64.9133	30.0657	0.9138	0.037
	40	0.66	2	50	1880.97	1.967729	64.18	31.5324	0.8841	0.0487
	40	0.66	3	51		1.986479	63.6933	29.7067	0.8922	0.046
	40	0.83	1	52	1998.703		64.8441	31.9518	0.9041	0.0425
	40	0.83	2	53		2.276714	62.4749	29.1944	0.9025	0.0423
	40	0.83	3	54	2129.869	2.2759	62.9329	29.8147	0.9051	0.0439
	40	1	1	55		2.541343	66.0281	30.1749	0.9051	0.0418
	40	1	2			2.591857	67.9619	30.1246	0.9169	0.0359
	40	1	3	57		2.536957	61.9198	29.6126	0.9075	0.0309
			-				3 100	_0.0120	0.0010	0.0094

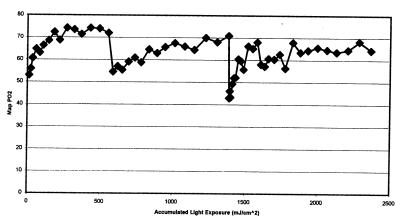


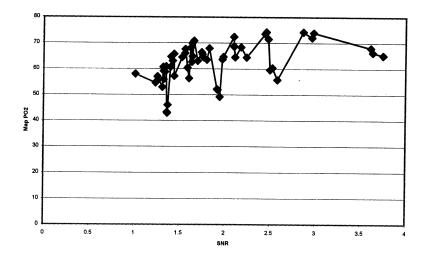


Cain		Evaceure 1	Dolotivo Im	Cuma ulatic	. ^	CND	DO0.14	D00.0/ D		
Gain	70	0.15	Relative in	Cumulative 1	Accumulat 11.85236			PO2 St. D€		R2 St. Dev
	70	0.15	2	2			52.903 55.8798	32.7733	0.7325	0.1041
	70	0.15	3	3			60.6626	33.4164 35.1454	0.7383 0.7451	0.1113
	70	0.31	1	4			64.7687	31.651	0.7451	0.1041 0.0709
	70	0.31	2	5			63.0644	32.4378	0.8325	0.0709
	70	0.31	3	6			66.3737	32.445	0.8339	0.0093
	70	0.47	1	7		2.102364	68.5863	31.1614	0.8761	0.0053
	70	0.47	2	8			72.3793	33.37	0.8765	0.053
	70	0.47	3	9			68.7853	32.0801	0.8714	0.0561
	70	0.63	1	10			74.2449	33.1039	0.8971	0.0459
	70	0.63	2	11			73.4923	31.9805	0.926	0.0455
	70	0.63	3	12		2.480829	71.4642	31.3944	0.8985	0.0429
	70	0.79	1	13	432.2161	2.866643	74.2537	30.2499	0.9163	0.0358
	70	0.79	2	14			73.9385	30.8788	0.9173	0.0347
	70	0.79	3	15	557.061	2.962064	72.0386	31.386	0.9186	0.0364
	10	0.4	1	16	588.6673	1.2354	54.6041	33.4098	0.761	0.0981
	10	0.4	2	17	620.2736	1.255164	57.0198	32.832	0.7526	0.101
	10	0.4	3	18	651.8799	1.253093	55.4233	31.7813	0.7566	0.1024
	10	0.55	1	19	695.3386	1.325571	59.1534	31.5551	0.8139	0.0768
	10	0.55	2	20	738.7972	1.351636	60.8962	31.6401	0.8194	0.0778
	10	0.55	3	21	782.2559	1.341893	58.8365	31.8688	0.8158	0.0784
	10	0.7	1	22	837.5669	1.407286	64.6885	32.5044	0.8465	0.0683
	10	0.7	2	23	892.878	1.425021	63.0371	31.3605	0.8538	0.0644
	10	0.7	3	24	948.189	1.43875	65.7123	32.9903	0.8542	0.0602
	10	0.85	1	25	1015.352	1.562129	67.5597	31.6752	0.8808	0.0505
	10	0.85	2	26	1082.516	1.560307	66.0256	32.2798	0.8818	0.0505
	10	0.85	3	27	1149.679	1.526779	64.5031	32.0364	0.8777	0.0518
	10	1	1	28	1228.695	1.638779	69.8933	31.6102	0.8929	0.0466
	10	1	2	29	1307.711	1.620521	68.056	32.4237	0.8904	0.0461
	10	1	3	30	1386.726	1.658779	70.8272	31.4441	0.8964	0.0466
	100	0.06	1	31	1391.467	1.365521	42.9322	32.6854	0.5683	0.153
	100	0.06	2	32	1396.208	1.370479	46.0459	33.9414	0.5821	0.1439
	100	0.06	3	33	1400.949	1.362493	43.235	31.5879	0.5802	0.1514
	100	0.145	1	34	1412.406	1.947371	49.2172	31.9046	0.7268	0.1141
	100	0.145	2	35	1423.864	1.9242	51.8969	32.2806	0.7089	0.1152
	100	0.145	3	36	1435.321	1.915043	52.0852	35.4292	0.707	0.119
	100 100	0.23	1	37	1453.495	2.527536	60.3997	34.5744	0.7999	0.0849
	100	0.23 0.23	2	38	1471.668	2.501343	59.5653	32.4009	0.7986	0.0858
	100	0.23	3 1	39 40	1489.842	2.583586	55.7673	31.8721	0.7961	0.0854
	100	0.4	2		1521.448	3.634471	66.2506	33.1174	0.8635	0.0569
	100	0.4	3	41 42		3.749493	65.1519	32.4157	0.8652	0.0586
	40	0.32	1	43	1584.661 1609.946	3.613557	68.0268	32.1029	0.8637	0.0585
	40	0.32	2	44	1635.231	1.011307	58.0296	32.3314	0.7945	0.0873
	40	0.32	3	44	1660.516	1.441707	57.2084 60.5047	31.2016	0.8001	0.0813
	40	0.49	1	46	1699.234	1.3989 1.5879	60.5947	34.1484	0.7843	0.0896
	40	0.49	2	47	1737.951	1.6362	60.3772 62.6073	30.8028	0.8415	0.068
	40	0.49	3	48	1776.669	1.605014	56.3085	32.5153	0.8356	0.0701
	40	0.66	1	49	1828.819	1.829336	67.8949	32.3405	0.8229	0.0779
	40	0.66	2	50	1880.97	1.801843	63.456	31.4686 33.6456	0.8824	0.0516
	40	0.66	3	51	1933.12	1.762843	64.4078	31.5356	0.8671 0.8596	0.0551 0.0608
	40	0.83	1	52	1998.703	1.753671	65.5881	30.644	0.8888	0.0608
	40	0.83	2	53	2064.286	1.9844	64.5773	30.044	0.8877	0.0471
	40	0.83	3	54	2129.869	1.97485	63.604	30.9199	0.8802	0.0464
	40	1	1	55	2208.885	2.114571	64.4976	30.0008	0.8899	0.0508
	40	1	2	56	2287.901	2.177929	68.3007	32.2907	0.8966	0.0439
	40	1	3	57	2366.917	2.23995	64.4078	30.7988	0.8945	0.0443

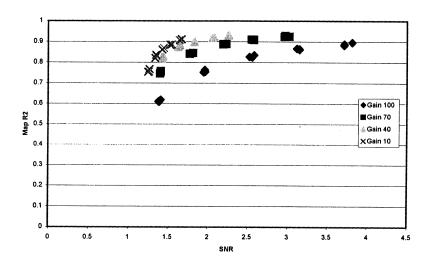
# Mouse 3a Tissue

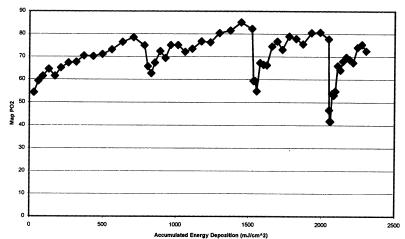


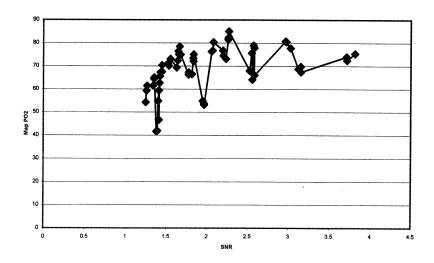




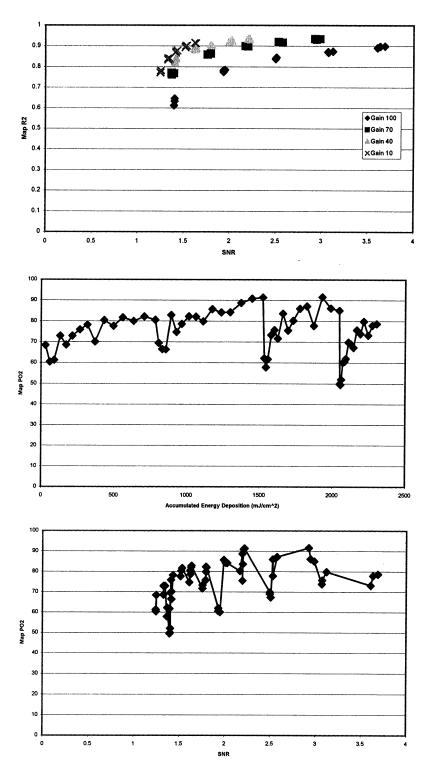
Gain		Exposure 1Rel						PO2 St. D€	R2 Mean	R2 St. Dev
	10	0.4	1	1	29.83465		54.2929	31.954	0.7545	0.1028
	10	0.4	2	2			59.3012	32.9182	0.755	0.1012
	10	0.4	3	3	89.50394		61.4194	33.1379	0.768	0.0946
	10	0.55	1	4	130.5266		64.5087	32.7688	0.8357	0.0656
	10	0.55	2	5	171.5492		61.4447	31.6342	0.8213	0.0756
	10	0.55	3	6	212.5719		65.0657	31.7011	0.8316	0.0697
	10	0.7	1	7	264.7825		67.2662	33.2668	0.8621	0.059
	10	0.7	2	8	316.9931	1.4462	67.5801	27.97	0.8697	0.058
	10	0.7	3	9	369.2037		70.3787	32.3974	0.8699	0.0542
	10	0.85	1	10	432.6024		70.1708	33.1687	0.8846	0.0498
	10	0.85	2	11	496.001	1.522459	71.0868	32.7576	0.8849	0.0503
	10	0.85	3	12	559.3996		73.073	31.784	0.8865	0.051
	10	1	1	13	633.9862	1.645319	76.4273	31.1483	0.9068	0.0409
	10	1	2	14	708.5728	1.664059	78.4581	31.0013	0.9106	0.038
	10	1	3	15	783.1594	1.674585	74.9484	31.3675	0.9122	0.0368
	40	0.32	1	16	807.0272	1.422963	65.6925	32.1986	0.8232	0.0734
	40	0.32	2	17	830.8949	1.416637	62.6822	32.652	0.8156	0.0768
	40	0.32	3	18	854.7626	1.439726	67.3019	34.8399	0.8275	0.0726
	40	0.49	1	19	891.31	1.639674	72.368	32.241	0.8789	0.0518
	40	0.49	2	20	927.8575	1.626193	69.3753	31.945	0.8736	0.0531
	40	0.49	3	21	964.4049	1.653133	75.0447	32.765	0.8821	0.0497
	40	0.66	1	22	1013.632	1.837407	75.0644	30.7912	0.8997	0.044
	40	0.66	2	23	1062.859	1.833711	72.127	31.1546	0.8985	0.0436
	40	0.66	3	24	1112.086	1.831637	73.4233	31.4555	0.8977	0.0437
	40	0.83	1	25	1173.993	2.069674	76.7009	30.8673	0.9166	0.0358
	40	0.83	2	26	1235.9	2.056133	76.2951	31.5576	0.9187	0.0363
	40	0.83	3	27	1297.807		80.3291	30.7684	0.9197	0.0358
	40	1	1	28	1372.394	2.259015	81.4934	30.4663	0.9327	0.0299
	40	1	2	29	1446.98	2.267148	85.0689	29.602	0.9303	0.0309
	40	1	3	30	1521.567	2.2616	82.2324	31.2938	0.9283	0.0314
	70	0.15	1	31	1532.755	1.406711	59.3934	34.1476	0.7505	0.1029
	70	0.15	2	32	1543.943	1.409481	59.3854	33.4786	0.7586	0.0997
	70	0.15	3	33	1555.131	1.399504	54.8251	33.0757	0.7461	0.1022
	70	0.31	1	34	1578.253	1.776459	67.2759	31.9246	0.842	0.0668
	70	0.31	2	35	1601.375	1.815815	66.481	33.2796	0.8452	0.0651
	70	0.31	3	36	1624.496	1.774333	66.2977	33.0188	0.8412	0.0665
	70	0.47	1	37	1659.552	2.200267	74.4833	32.3745	0.8887	0.0473
	70	0.47	2	38	1694.608	2.193904	76.6953	31.0294	0.8874	0.0499
	70	0.47	3	39	1729.664	2.231926	73.1161	31.1217	0.889	0.0493
	70	0.63	1	40	1776.653	2.571089	78.9465	31.3773	0.9108	0.0402
	70	0.63	2	41		2.580985	77.8667	31.2049	0.9085	0.0406
	70 70	0.63	3	42	1870.632		75.5965	32.2913	0.9104	0.0403
	70	0.79	1	43		2.973481	80.4637	29.3631	0.9284	0.0316
	70 70	0.79	2	44		2.963556	80.6906	31.025	0.9243	0.033
	70	0.79	3	45	2047.403	3.025459	77.736	31.1334	0.9247	0.0325
	100	0.06	1	46	2051.878	1.408807	46.6626	34.0599	0.6187	0.1413
	100	0.06	2		2056.353	1.390311	41.8608	32.3684	0.6085	0.1512
	100	0.06	3		2060.828	1.379985	41.6882	30.5675	0.61	0.1423
	100	0.145	1		2071.643	1.964756	53.7948	32.2564	0.7638	0.0919
	100	0.145	2		2082.458	1.967252	53.1316	33.4414	0.7543	0.107
	100	0.145	3		2093.273	1.948896	54.8458	32.6001	0.7522	0.1026
	00	0.23	1		2110.428	2.58243	65.9946	32.8156	0.8348	0.0714
	00	0.23	2		2127.583	2.557644	64.0963	31.8675	0.8242	0.0717
	00	0.23	3		2144.738	2.52437	67.9531	34.086	0.8266	0.0746
	00	0.315	1		2168.233	3.149911	69.8047	32.5501	0.8642	0.0576
	00	0.315	2			3.119511	68.7328	32.0417	0.8667	0.0579
	00	0.315	3			3.152356	67.4219	31.3275	0.861	0.0624
	00	0.4	1			3.712978	74.0834	32.5521	0.8822	0.0505
	00	0.4	2			3.815556	75.3829	30.4895	0.8957	0.0465
7	00	0.4	3	60	2304.726	3.716726	72.5043	31.6959	0.8879	0.0492





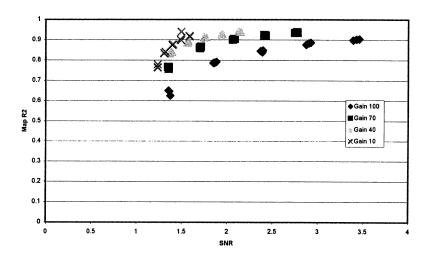


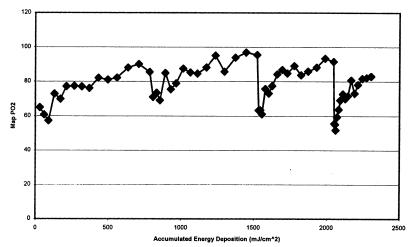
Gain		Exposure 1					PO2 Mean	PO2 St. D€	R2 Mean	R2 St. Dev
	10	0.4	1	1			68.3765	34.4412	0.7832	0.0918
	10	0.4	2				60.3828	32.6263	0.7729	0.0938
	10	0.4	3				61.2621	33.7001	0.7728	0.0947
	10	0.55	1	4			72.8594	34.2186	0.8349	0.0681
	10	0.55	2	5			68.5709	32.8407	0.8408	0.0673
	10	0.55	3	6			72.869	32.4855	0.8396	0.0687
	10	0.7	1	7	264.7825	1.412007	75.8372	32.2745	0.8683	0.0554
	10	0.7	2	8	316.9931	1.433696	78.1534	33.3046	0.8785	0.0523
	10	0.7	3	9	369.2037	1.416948	70.0845	33.5629	0.8751	0.0534
	10	0.85	1	10			80.3243	34.2184	0.9	0.0458
	10	0.85	2	11	496.001	1.517052	77.6035	32.1845	0.8952	0.0449
	10	0.85	3	12			81.6392	33.856	0.9016	0.0448
	10	1	1	13	633.9862		79.9942	31.6674	0.9141	0.0366
	10	1	2	14			82.098	31.8275	0.9141	0.0373
	10	1	3	15	783.1594	1.623126	80.5158	32.7948	0.9152	0.0371
	40	0.32	1	16	807.0272	1.405096	69.4751	31.8162	0.8238	0.0694
	40	0.32	2	17	830.8949	1.414037	66.4904	35.4277	0.8396	0.0698
	40	0.32	3	18	854.7626	1.417296	66.39	34.6509	0.8427	0.0663
	40	0.49	1	19	891.31	1.637533	82.8177	30.4323	0.8915	0.0486
	40	0.49	2	20	927.8575	1.614259	74.7071	32.9349	0.8881	0.0488
	40	0.49	3	21	964.4049	1.6254	78.5523	32.4108	0.884	0.0521
	40	0.66	1	22	1013.632	1.797348	82.2476	30.7741	0.9064	0.0405
	40	0.66	2	23	1062.859	1.804652	82.0325	31.7717	0.905	0.0411
	40	0.66	3	24	1112.086	1.798496	79.8511	31.6799	0.9042	0.0422
	40	0.83	1	25	1173.993	1.992704	85.6966	28.6201	0.9214	0.0372
	40	0.83	2	26	1235.9	2.029622	84.1408	33.4947	0.9255	0.0335
	40	0.83	3	27	1297.807	2.012222	84.2075	31.5339	0.9276	0.0324
	40	1	1	28	1372.394	2.197237	88.688	29.8057	0.9365	0.026
	40	1	2	29	1446.98	2.212548	90.8213	30.4399	0.9367	0.020
	40	1	3	30	1521.567	2.22037	91.3635	31.5302	0.934	0.0298
	70	0.15	1	31	1532.755	1.370807	62.2085	33.6107	0.7621	0.0290
	70	0.15	2	32	1543.943	1.367296	57.8711	32.4899	0.7715	0.0967
	70	0.15	3	33	1555.131	1.395667	61.6869	32.7905	0.7686	0.0946
	70	0.31	1	34	1578.253	1.760333	73.2865	31.2572	0.8592	0.0621
	70	0.31	2	35	1601.375	1.792837	75.73	32.8233	0.8635	0.0577
	70	0.31	3	36	1624.496	1.758459	71.6082	31.7988	0.8596	0.0601
	70	0.47	1	37	1659.552	2.202963	83.6044	32.2228	0.8987	0.0445
	70	0.47	2	38	1694.608	2.200126	75.4555	31.5909	0.8997	0.0445
	70	0.47	3	39	1729.664	2.171941	80.185	31.2833	0.9002	0.045
	70	0.63	1	40	1776.653	2.530963	85.9763	32.0092	0.9206	0.0337
	70	0.63	2	41	1823.643	2.57697	87.1368	29.5879	0.9200	0.0357
	70	0.63	3	42		2.531178	77.7445	30.5814	0.9192	0.0358
	70	0.79	1	43	1929.556	2.926904	91.541	29.4474	0.935	0.0338
	70	0.79	2	44	1988.479	2.946548	86.1446	30.7619	0.9314	0.0271
	70	0.79	3	45	2047.403	2.98623	85.0351	30.2432	0.9345	0.0294
	100	0.06	1	46		1.402022	49.8785	34.4963	0.6461	0.0301
	100	0.06	2	47	2056.353	1.39563	49.51	31.9089	0.6124	
	100	0.06	3	48	2060.828	1.402822	51.9903	32.1192	0.6332	0.1358
	100	0.145	1		2071.643	1.949859	60.0672	33.4627		0.1354
	100	0.145	2		2082.458	1.932756			0.7852	0.0927
	100	0.145	3	51	2093.273	1.932736	60.5336	33.4991	0.7826	0.0902
	100	0.23	1		2110.428	2.4996	61.9497	36.0968	0.7751	0.0965
	100	0.23	2		2127.583	2.4996	69.8069 68.9733	32.4041	0.8384	0.0723
	100	0.23	3			2.508378	67.2756	33.1368	0.8379	0.0677
	100	0.315	1		2168.233			31.9931	0.845	0.0692
	100	0.315	2	56	2191.728	3.075081	75.7456	33.4292	0.8688	0.0553
	100	0.315	3			3.071356	73.8262	33.4248	0.8722	0.0557
	100	0.313	1			3.123289	79.8329	34.1004	0.875	0.0545
	100	0.4	2		2245.057	3.610207	73.1357	30.0954	0.8916	0.0478
	00	0.4	3			3.636733	77.8711	32.1963	0.898	0.0446
- 1	00	0.4	3	ю	2304.726	3.688763	78.6768	31.9384	0.8994	0.043

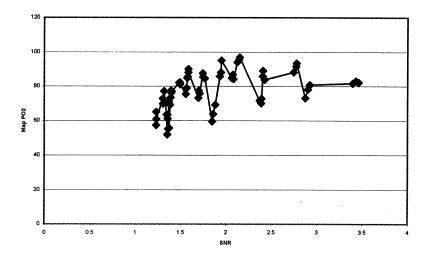


Gain		Exposure 3	Relative Im	Cumulative	: Accumulat	CND	DO2 Maan	DO0 04 D	D0.14	D0.01 D
ou	10	0.4	1	1			64.9766	PO2 St. D€		R2 St. Dev
	10	0.4	2	2			60.8096	32.5012	0.7795	0.0953
	10	0.4	3	3			57.3027	33.4929 32.8772	0.7645	0.095
	10	0.55	1	4				33.3182	0.7655	0.102
	10	0.55	2	5			69.7979		0.837	0.0674
	10	0.55	3	6			77.0928	34.3218	0.8333	0.0705
	10	0.7	1	7			77.3774	33.4159 32.1369	0.841	0.0674
	10	0.7	2	8	316.9931	1.403778	77.0324	33.0576	0.8741	0.0522
	10	0.7	3	9	369.2037	1.398948	76.1231	32.8144	0.8769	0.0524
	10	0.85	1	10	432.6024	1.484267	82.0979	31.2087	0.8767	0.0513
	10	0.85	2	11	496.001	1.49623	81.0378	32.8806	0.9014 0.898	0.043
	10	0.85	3	12	559.3996	1.493163	82.1098	32.9046	0.9403	0.0455
	10	1	1	13	633.9862	1.585807	88.0422	30.0346	0.9403	0.0422 0.036
	10	1	2	14	708.5728	1.585652	90.0391	30.5681	0.9202	0.0345
	10	1	3	15	783.1594	1.580681	85.4821	31.6587	0.9202	0.0343
	40	0.32	1	16	807.0272	1.371222	70.9834	30.8444	0.8332	0.0331
	40	0.32	2	17	830.8949	1.390733	73.388	33.1665	0.8395	0.0739
	40	0.32	3	18	854.7626	1.3834	69.123	31.7289	0.83	
	40	0.49	1	19	891.31	1.572852	84.8061	34.425	0.8929	0.0674 0.0472
	40	0.49	2	20	927.8575	1.5584	75.3968	31.6618	0.8873	0.0472
	40	0.49	3	21	964.4049	1.567067	78.9192	30.2684	0.886	0.0303
	40	0.66	1	22	1013.632	1.745378	87.4987	32.4787	0.000	0.0477
	40	0.66	2	23	1062.859	1.748489	85.2175	31.2961	0.9131	0.037
	40	0.66	3	24	1112.086	1.767378	84.6003	31.7427	0.9116	0.0397
	40	0.83	1	25	1173.993	1.945311	88.0657	28.8299	0.9286	0.0372
	40	0.83	2	26	1235.9	1.949741	95.1213	30.8064	0.92831	0.0333
	40	0.83	3	27	1297.807	1.933481	85.696	31.6265	0.9256	0.032
	40	1	1	28	1372.394	2.125163	93.9374	29.5682	0.942	0.0320
	40	1	2	29	1446.98	2.151667	96.8605	29.6409	0.9398	0.0274
	40	1	3	30	1521.567	2.144533	95.49	30.6758	0.9394	0.0274
	70	0.15	1	31	1532.755	1.355563	63.3009	34.7719	0.7575	0.1008
	70	0.15	2	32	1543.943	1.347422	63.4385	33.5787	0.768	0.0929
	70	0.15	3	33	1555.131	1.358393	61.052	32.647	0.7653	0.0925
	70	0.31	1	34	1578.253	1.711	75.6701	32.4843	0.8668	0.0571
	70	0.31	2	35	1601.375	1.696948	73.1317	34.4582	0.8632	0.0593
	70	0.31	3	36	1624.496	1.701533	77.3596	32.0273	0.8586	0.0627
	70	0.47	1	37	1659.552	2.083719	84.1888	31.3915	0.9047	0.0405
	70	0.47	2	38	1694.608	2.076444	86.7617	32.1311	0.904	0.0414
	70	0.47	3	39	1729.664	2.063815	84.763	30.1723	0.901	0.0454
	70	0.63	1	40	1776.653	2.408141	89.0282	30.974	0.9245	0.0327
	70	0.63	2	41	1823.643	2.426363	83.7486	31.6726	0.9217	0.0342
	70	0.63	3	42	1870.632		85.8464	30.0553	0.9208	0.0347
	70	0.79	1	43	1929.556	2.747652	88.1612	30.9903	0.9348	0.0293
	70	0.79	2	44	1988.479	2.778296	93.4185	28.9005	0.9348	0.029
	70	0.79	3	45	2047.403	2.773304	91.5489	32.1736	0.939	0.0264
	00	0.06	1	46	2051.878	1.373556	55.6798	35.5861	0.6254	0.146
	00	0.06	2	47	2056.353	1.362904	55.1774	33.872	0.6471	0.1349
	00	0.06	3	48	2060.828	1.354015	51.8807	33.1823	0.6507	0.1331
	00	0.145	1	49	2071.643	1.850089	59.4823	30.7688	0.7867	0.092
	00	0.145	2	50	2082.458	1.86057	63.7523	32.846	0.7874	0.0884
	00	0.145	3		2093.273	1.882319	69.1437	36.7375	0.7919	0.0869
	00	0.23	1		2110.428	2.39323	72.6975	34.2522	0.8486	0.0646
	00	0.23	2			2.389111	70.0519	33.1367	0.8401	0.0697
	00	0.23	3	54	2144.738	2.371	71.6138	33.7361	0.8453	0.0669
	00	0.315	1	55		2.923511	80.7446	32.181	0.8864	0.0497
	00	0.315	2			2.874452	73.0974	32.1228	0.876	0.0529
	00	0.315	3		2215.222	2.903193	78.1554	33.3231	0.8832	0.0528
	00	0.4	1		2245.057	3.39423	81.6787	33.9078	0.8984	0.0461
	00	0.4	2		2274.892	3.460215	82.1298	32.8302	0.9043	0.0414
10	00	0.4	3	60	2304.726	3.429778	82.9793	31.0943	0.9023	0.0438

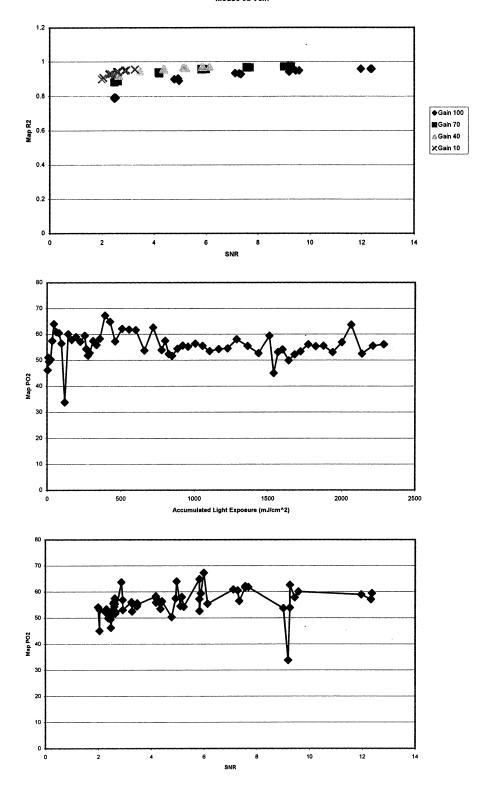
## Mouse 4a Tissue





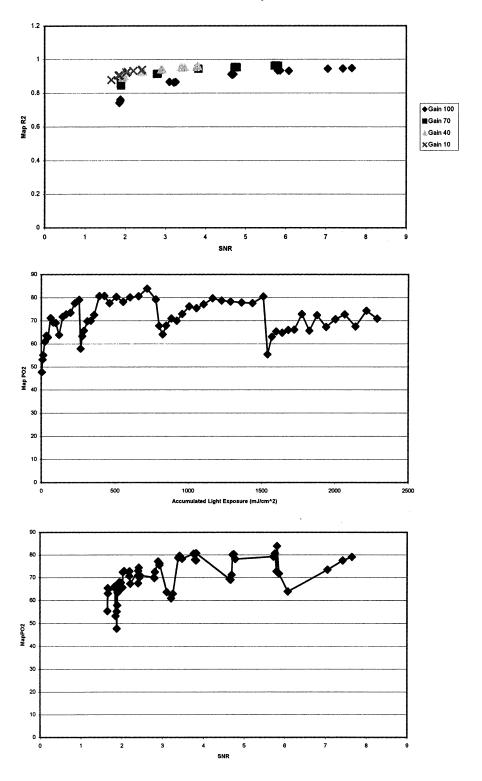


Gain		Exposure 1	Relative Im Cur	mulativ	e Accumula	t, SNP	PO2 Moon	DO2 C4 D-	D0 M	D0 01 D
	100	0.06	1	1			46.2413	PO2 St. D€		R2 St. Dev
	100	0.06	2	2			51.0555	31.2319 29.7192	0.7863	0.0904
	100	0.06	3	3			49.412	30.5579	0.7922	0.0838
	100	0.145	1	4			50.2866	26.4852	0.7936	0.0861
	100	0.145	2	5			57.4998	29.7529	0.8989	0.0451
	100	0.145	3	6			63.9757	30.3678	0.9034	0.0418
	100	0.23	1	7			60.8788	28.8409	0.8897	0.0482
	100	0.23	2	8			60.5036	27.4923	0.9333	0.0293
	100	0.23	3	9			56.491	26.623	0.9317	0.0301
	100	0.315	1	10			33.7939	11.3997	0.9285 0.9417	0.0326
	100	0.315	2	11			60.0648	26.1406	0.9417	0.0258
	100	0.315	3	12			57.8755	25.5156	0.9478	0.0227
	100	0.4	1	13		11.95566	58.9466	24.3787	0.9578	0.022
	100	0.4	2	14		12.33004	57.0861	23.1901	0.9584	0.0187
	100	0.4	3	15			59.4674	22.9969	0.958	0.0179 0.018
	70	0.15	1	16	266.5984		54.3219	30.4287	0.8877	
	70	0.15	2	17	277.7067		51.7616	27.7822	0.8816	0.0477 0.0521
	70	0.15	3	18	288.815		52.8028	28.5423	0.8912	0.0321
	70	0.31	1	19	311.772		57.4241	26.6316	0.0912	
	70	0.31	2	20	334.7291	4.180252	55.8462	25.6705	0.9394	0.0289
	70	0.31	3	21	357.6862		58.301	25.6918	0.9367	0.0265 0.0267
	70	0.47	1	22	392.4921	5.99023	67.2376	27.6273	0.9571	0.0267
	70	0.47	2	23	427.298		64.8627	26.4966	0.9579	0.0195
	70	0.47	3	24	462.1039		57.2309	22.6513	0.955	0.0187
	70	0.63	1	25	508.7587	7.567733	62.1207	22.5469	0.9686	0.0136
	70	0.63	2	26	555.4134	7.680089	61.808	23.5587	0.9666	0.0130
	70	0.63	3	27	602.0681	7.562593	61.6279	23.9916	0.9654	0.0147
	70	0.79	1	28	660.5717		53.7316	18.512	0.9034	0.0136
	70	0.79	2	29	719.0752	9.256215	62.6192	21.4068	0.9725	0.0124
	70	0.79	3	30	777.5787	9.252622	53.8831	19.1024	0.9712	0.0128
	40	0.32	1	31	801.2764	2.624637	57.4538	27.3035	0.9219	0.0126
	40	0.32	2	32	824.974	2.656207	52.3714	25.6035	0.9194	0.0343
	40	0.32	3	33	848.6717		51.6799	24.5364	0.9217	0.0338
	40	0.49	1	34	884.9587	3.465193	54.3578	23.7446	0.9464	0.0333
	40	0.49	2	35	921.2457	3.466926	55.6265	25.266	0.9458	0.0233
	40	0.49	3	36	957.5327	3.474719	55.2153	24.3636	0.9465	0.023
	40	0.66	1	37	1006.409		56.3453	22.5382	0.9565	0.023
	40	0.66	2	38	1055.285		55.5135	23.4137	0.9588	0.0183
	40	0.66	3	39	1104.162	4.350637	53.4804	21.4382	0.9582	0.0187
	40	0.83	1	40	1165.628	5.2354	54.276	21.1731	0.9632	0.0162
	40	0.83	2	41	1227.093		54.5259	21.9059	0.9644	0.0162
	40	0.83	3	42	1288.559		58.0108	23.145	0.9646	0.0154
	40	1	1	43	1362.614		55.4217	19.6536	0.9712	0.0121
	40	1	2	44	1436.669		52.6632	19.5386	0.9692	0.0133
	40	1	3	45	1510.724	5.881252	59.3984	21.9245	0.97	0.0129
	10	0.4	1	46	1540.346	2.047067	44.9983	23.2808	0.9064	0.0398
	10	0.4	2	47	1569.969	2.051593	53.0802	26.854	0.9066	0.0398
	10	0.4	3	48	1599.591	1.9928	54.0821	28.6099	0.8991	0.0422
	10	0.55	1	49	1640.321	2.381311	49.8412	24.262	0.9292	0.0312
	10	0.55	2	50	1681.051	2.278837	52.1385	25.517	0.9276	0.0319
	10	0.55	3	51	1721.781	2.310526	53.3384	25.2274	0.9299	0.0301
	10	0.7	1	52	1773.62	2.601807	56.0286	24.3599	0.9427	0.0253
	10	0.7	2	53		2.622178	55.3013	24.5241	0.9412	0.0252
	10	0.7	3			2.569689	55.4751	26.2194	0.9425	0.0247
	10	0.85	1	55	1940.244	2.926919	53.0072	22.1237	0.9514	0.0212
	10	0.85	2			2.919859	56.872	23.3162	0.9527	0.0202
	10	0.85	3		2066.138	2.875778	63.6572	26.796	0.9483	0.0231
	10	1	1		2140.193	3.280837	52.4587	21.0436	0.9562	0.019
	10	1	2		2214.248	3.280237	55.5089	22.9946	0.9549	0.0193
	10	1	3	60	2288.303	3.256844	56.0607	22.9189	0.9544	0.0204

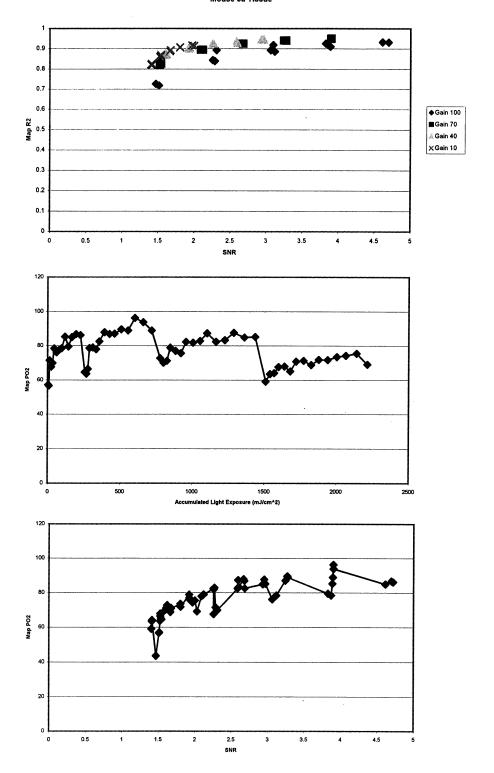


Gain		Exposure 1	Relative Im Cu	mulativ	Accumulat	SNR	PO2 Mean	PO2 St. D€	P2 Mean	R2 St. Dev
	100	0.06	1	1			47.7652	34.0497	0.7541	0.1085
	100	0.06	2	2			53.1851	32.2245	0.7341	
	100	0.06	3	3			55.1511	32.3214	0.7410	0.107
	100	0.145	1	4			60.9515	31.4961		0.0989
	100	0.145	2	5			63.6236		0.8634	0.0593
	100	0.145	3	6			62.8875	31.56	0.8669	0.0575
	100	0.23	1	7				31.0666	0.866	0.0606
	100	0.23	2	8			71.1771	32.7502	0.9113	0.037
	100	0.23	3	9			69.3285	29.9091	0.9121	0.0366
	100	0.315	1	_			69.0837	32.0626	0.9074	0.00418
	100	0.315		10			63.9224	27.2446	0.9317	0.0271
	100		2	11	143.2967		71.7915	29.1064	0.9334	0.0294
	100	0.315	3	12	166.624		72.796	31.3634	0.9334	0.0283
	100	0.4	1	13	196.2461	7.050156	73.4951	29.44	0.9442	0.0249
		0.4	2	14	225.8681	7.421222	77.5166	30.6204	0.9455	0.0244
	100	0.4	3	15	255.4902		79.055	29.7445	0.9475	0.0226
	70	0.15	1	16	266.5984	1.891281	57.8994	30.4998	0.853	0.0612
	70	0.15	2	17	277.7067	1.897696	63.3721	32.2227	0.8448	0.0651
	70	0.15	3	18	288.815	1.894978	65.7333	33.7442	0.8609	0.0608
	70	0.31	1	19	311.772	2.801504	69.8133	30.1597	0.9141	0.0379
	70	0.31	2	20	334.7291	2.790333	70.0534	31.195	0.914	0.0389
	70	0.31	3	21	357.6862	2.814096	72.5058	30.5953	0.9157	0.0374
	70	0.47	1	22	392.4921	3.823978	80.7039	31.1622	0.9438	0.0245
	70	0.47	2	23	427.298	3.826896	80.7321	28.9344	0.9441	0.0251
	70	0.47	3	24	462.1039	3.82303	77.5781	28.6279	0.9452	0.0253
	70	0.63	1	25	508.7587	4.750311	80.2946	29.5501	0.9552	0.0194
	70	0.63	2	26	555.4134	4.784341	78.1494	28.1699	0.9531	0.0206
	70	0.63	3	27	602.0681	4.7232	80.0924	28.942	0.9516	0.0212
	70	0.79	1	28	660.5717	5.760593	80.6246	28.2649	0.9638	0.0167
	70	0.79	2	29	719.0752	5.812978	83.8884	28.4426	0.9624	0.0175
	70	0.79	3	30	777.5787	5.722548	79.2245	27.7121	0.9625	0.0164
	40	0.32	1	31	801.2764	1.981281	67.8055	31.0842	0.8991	0.0415
	40	0.32	2	32	824.974	1.925681	64.0778	31.2149	0.8906	0.0494
	40	0.32	3	33	848.6717	1.940415	67.9342	31.0329	0.8964	0.0462
	40	0.49	1	34	884.9587	2.448111	70.9768	29.592	0.9271	0.0402
	40	0.49	2	35	921.2457	2.433785	70.0152	31.0149	0.926	0.0317
	40	0.49	3	36	957.5327	2.401237	72.9757	30.6364	0.9245	0.0317
	40	0.66	1	37	1006.409	2.926274	76.2121	30.0589	0.9422	0.0324
	40	0.66	2	38	1055.285	2.922622	75.4443	29.5041	0.9414	0.0244
	40	0.66	3	39	1104.162	2.892837	77.1184	30.596	0.9414	0.0202
	40	0.83	1	40	1165.628	3.421378	79.6789	28.6756	0.9505	
	40	0.83	2	41	1227.093	3.38583	78.7134	28.226	0.9523	0.0219 0.0213
	40	0.83	3	42	1288.559		78.2875	28.8438		
	40	1	1	43	1362.614		77.8734	28.3193	0.9536 0.9592	0.0204
	40	1	2	44	1436.669	3.81663	77.6165	29.0069		0.0189
	40	1	3	45	1510.724	3.76597	80.4811	28.1495	0.958	0.018
	10	0.4	1	46	1540.346	1.647711	55.3826		0.9549	0.0202
	10	0.4	2	47	1569.969	1.65937		29.2869	0.8794	0.0488
	10	0.4	3	48			63.0616	31.3006	0.8792	0.0494
	10	0.55	1	49	1599.591 1640.321	1.6552	65.3658	33.1906	0.8774	0.049
	10	0.55	2			1.866304	64.7691	30.5943	0.9061	0.0399
	10			50	1681.051	1.831541	65.9882	30.0864	0.9081	0.0397
		0.55	3	51 52	1721.781	1.831259	66.1458	32.8499	0.9025	0.0421
	10 10	0.7	1	52 53		2.059059	72.8709	31.3669	0.9265	0.0331
		0.7	2	53 54	1825.459	2.0186	65.6895	29.4057	0.9238	0.0323
	10	0.7	3	54	1877.297	2.029089	72.3919	32.5485	0.9189	0.0364
	10	0.85	1	55	1940.244		67.3396	29.4738	0.9337	0.0287
	10	0.85	2			2.188607	70.6172	30.8073	0.932	0.0314
	10	0.85	3		2066.138		72.7602	30.3415	0.9317	0.0307
	10	1	1		2140.193		67.5463	28.7448	0.9382	0.0272
	10	1	2		2214.248		74.3731	31.5861	0.9398	0.0253
	10	1	3	60	2288.303	2.404259	70.9447	28.3395	0.9354	0.0285





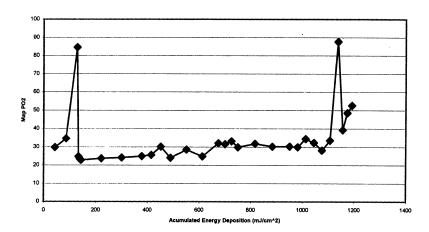
Gain		Exposure 1	Relative Irr Cun	nulativ	e Accumula	t <sub>i</sub> SNR	PO2 Mean	DO2 St Da	D2 Maan	R2 St. Dev
	100	0.06	1		4.443307		43.5548	32.2989	0.706	
	100	0.06	2	2			57.1264	34.388	0.7258	0.1219 0.1093
	100	0.06	3	3			56.6324	32.0772	0.7238	0.1093
	100	0.145	1	4			71.4797	33.2975	0.8417	0.1110
	100	0.145	2	5			67.5991	31.2017	0.8396	0.0666
	100	0.145	3	6			69.9141	32.6131	0.8438	0.0705
	100	0.23	1	7			78.4037	33.2322	0.8934	0.0455
	100	0.23	2	8	79.60925		76.1637	32.3134	0.8858	0.0494
	100	0.23	3	9	96.64193		77.637	32.486	0.8931	0.0467
	100	0.315	1	10	119.9693		78.5093	30.7984	0.9185	0.0351
	100	0.315	2	11	143.2967		85.2743	30.9947	0.9149	0.0372
	100	0.315	3	12	166.624	3.827437	79.511	31.5683	0.9107	0.041
	100	0.4	1	13		4.61463	84.9656	30.6047	0.9259	0.0321
	100	0.4	2	14			86.718	30.4836	0.9329	0.0301
,	100	0.4	3	15			86.1941	31.5897	0.9322	0.0307
	70	0.15	1	16			64.5076	33.1464	0.8262	0.0752
	70	0.15	2	17			63.6234	33.1206	0.8193	0.0745
	70	0.15	3	18	288.815		66.3763	33.3459	0.8268	0.0723
	70	0.31	1	19	311.772		78.5733	31.4295	0.8964	0.0462
	70	0.31	2	20	334.7291		79.0106	31.1489	0.8943	0.047
	70	0.31	3	21	357.6862		77.9216	32.1514	0.8943	0.0475
	70	0.47	1	22	392.4921		82.5698	30.1576	0.9255	0.0326
	70	0.47	2	23	427.298		87.848	31.2968	0.9264	0.0332
	70	0.47	3	24	462.1039		86.8616	31.0748	0.9248	0.034
	70	0.63	1	25	508.7587		87.0019	30.2508	0.9417	0.0264
	70	0.63	2	26	555.4134		89.5631	28.5702	0.9422	0.0265
	70 70	0.63 0.79	3	27	602.0681	3.27723	88.8839	30.6957	0.9398	0.0264
	70	0.79	1	28	660.5717		96.2313	28.5921	0.9515	0.0224
	70	0.79	2	29	719.0752	3.90563	93.8041	29.9284	0.9498	0.0212
	40	0.79	3 1	30	777.5787		88.9249	29.4781	0.9483	0.0237
	40	0.32	2	31 32	801.2764	1.621156	72.8141	33.5044	0.8717	0.531
	40	0.32	3	33	824.974	1.598259	70.0742	32.4769	0.8762	0.0547
	40	0.49	1	34	848.6717	1.611	71.2131	32.2693	0.8693	0.056
	40	0.49	2	35	884.9587 921.2457		78.9008	32.564	0.905	0.0412
	40	0.49	3	36	957.5327	1.924267 1.936267	76.9724	32.0939	0.9013	0.044
	40	0.66	1	37	1006.409	2.256696	75.7244 82.2923	31.9027	0.9059	0.0398
	40	0.66	2	38	1055.285	2.261296	81.8245	30.8797	0.9252	0.033
	40	0.66	3	39	1104.162		82.8509	31.4522	0.9254	0.0333
	40	0.83	1	40	1165.628	2.595356	87.29	30.673 30.5153	0.9247	0.0348
	40	0.83	2	41		2.587807	82.3839		0.9298	0.0268
	40	0.83	3		1288.559		83.2837	30.6405 31.313	0.9373	0.0272
	40	1	1	43	1362.614		87.6259	30.0576	0.9288 0.9457	0.0273
	40	1	2	44	1436.669	2.93283	84.8932	29.4324	0.9437	0.0239
	40	1	3	45	1510.724		85.1262	30.8059	0.9456	0.0237
	10	0.4	1	46	1540.346		59.0896	32.02	0.8224	0.0243 0.0741
	10	0.4	2	47	1569.969	1.409141	63.479	32.5313	0.0224	0.0741
	10	0.4	3	48	1599.591	1.411148	64.1089	33.2134	0.826	0.0752
	10	0.55	1	49	1640.321	1.538385	67.6241	32.4744	0.8703	0.0752
	10	0.55	2	50	1681.051	1.52637	67.8957	32.9326	0.8602	0.0601
	10	0.55	3	51	1721.781	1.535022	65.0922	32.0557	0.8654	0.0564
	10	0.7	1	52	1773.62	1.673489	70.8176	31.9787	0.894	0.0354
	10	0.7	2	53	1825.459	1.668659	71.3344	32.8242	0.8906	0.047
	10	0.7	3	54	1877.297	1.664511	68.8153	30.9859	0.8878	0.0496
	10	0.85	1		1940.244	1.802548	71.8552	31.2236	0.9084	0.0384
	10	0.85	2		2003.191	1.803207	71.7543	30.8969	0.9075	0.0403
	10	0.85	3	57	2066.138	1.802467	73.5595	31.2532	0.904	0.042
	10	1	1			1.969763	74.2993	31.1816	0.9169	0.0363
	0	1	2			2.001341	75.5048	30.5542	0.9141	0.0381
1	0	1	3	60	2288.303	2.031059	69.1801	30.7321	0.9023	0.0419

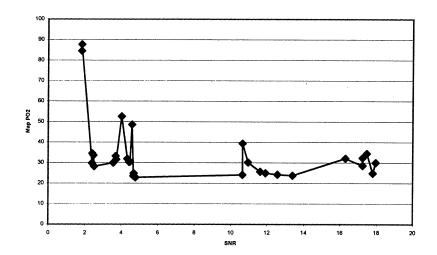


# Mouse6a

Gain	Exposure <sup>-</sup>	Relative Im	Cumulative	Accumulate	SNR	PO2 Mean	PO2 St. D€	R2 Mean	R2 St. Dev
1	0 0.55		1			29.747	23.7742	0.6966	0.129
1	0 0.55	2	2	86.20276	2.401879		26.6582	0.7137	0.129
1	0 0.55	3	3	129.3041	1.81845		32.0814	0.7157	0.1173
10	0.06	1	4	134.0061	4.682986	24.7623	26.018	0.4258	0.0027
10	0.06	2	5	138.7081	4.658593	23.5131	26.6065	0.405	0.1792
10	0.06	3	6	143.41	4.765929	22.7952	24.3599	0.384	0.1863
4	0 1	1	7	221.7762	13.38494	23.7151	11.8737	0.8749	0.0591
4	0 1	2	8	300.1423	12.56751	24.1796	11.357	0.8785	0.0559
4	0 1	3	9	378.5085	11.90782	24.8932	13.2223	0.08741	0.0559
7	0.47	1	10	415.3406	11.61982	25.6125	17.6148	0.7872	0.0904
7	0.47	2	11	452.1726	10.94506	30.1621	22.6711	0.7988	0.0981
7	0.47	3	12	489.0047	10.63664	24.0272	16.7616	0.8049	0.0812
7	0.79	1	13	550.914	17.24391	28.5788	15.6978	0.8739	0.0585
7		2	14	612.8232	17.80051	24.8413	13.3198	0.8583	0.0614
7		3	15	674.7325	16.29986	32.1015	17.9156	0.8745	0.0546
4		1	16	699.8096	3.725086	31.5125	26.0308	0.6873	0.126
40		2	17	724.8868	3.689443	33.1512	24.9948	0.6922	0.1341
40		3	18	749.964	3.558114	29.8872	24.3217	0.7124	0.1188
10		1	19	816.5752	4.324079	31.8299	21.2095	0.8296	0.0793
10		2	20	883.1864	4.427536	30.2618	20.7714	0.8131	0.0804
10		3	21	949.7976	4.480621	30.3282	20.2491	0.8137	0.0786
100		1	22	981.1441	17.95599	29.9827	24.4624	0.7667	0.0972
100		2	23	1012.491	17.47234	34.4066	24.0839	0.7812	0.1028
100		3	24	1043.837	17.24619	32.2917	22.7189	0.8017	0.0838
10		1	25	1075.183	2.508929	28.1878	24.2145	0.6637	0.1323
10		2	26	1106.53	2.468714	33.5509	26.3254	0.6988	0.1246
10		3	27	1137.876	1.825029	87.677	32.6266	0.8563	0.0633
100		1	28	1155.901	10.65046	39.3371	24.4196	0.8033	0.1778
100		2	29	1173.925	4.579829	48.5458	32.0213	0.6916	0.1208
100	0.23	3	30	1191.949	4.020764	52.5716	30.8783	0.75	0.1065

## Mouse 6a Vein

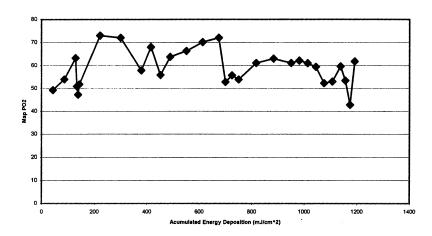


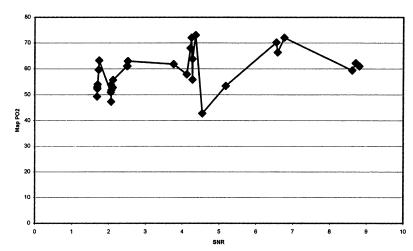


## Mouse6a

Gain	Exposure 1	Relative In C	Cumulative	Accumulate	SNR	PO2 Mean	PO2 St. De	R2 Mean	R2 St. Dev
10		1	1	43.10138	1.6822	49.3075	30.992	0.7858	0.0913
10	0.55	2	2	86.20276	1.6965	53.9733	31.3614	0.7942	0.0832
10	0.55	3	3	129.3041	1.735943	63.2369	31.2701	0.5675	0.1594
100	0.06	1	4	134.0061	2.055271	50.8819	34.8957	0.6708	0.1244
100	0.06	2	5	138.7081	2.063707	47.2779	31.4022	0.6704	0.1258
100	0.06	3	6	143.41	2.067171	51.7946	35.5517	0.6739	0.1228
40	1	1	7	221.7762	4.362057	73.0184	28.3021	0.9464	0.0234
40	1	2	8	300.1423	4.249179	72.0658	27.9342	0.9518	0.022
40	1	3	9	378.5085	4.120564	57.8418	27.2207	0.9444	0.0238
70	0.47	1	10	415.3406	4.222421	68.0117	31.8056	0.8899	0.0475
70	0.47	2	11	452.1726	4.276243	55.8318	28.2183	0.9099	0.0373
70	0.47	3	12	489.0047	4.278157	63.7527	29.2946	0.9031	0.0393
70	0.79	1	13	550.914	6.58805	66.3317	28.4793	0.9351	0.0298
70	0.79	2	14	612.8232	6.551957	70.1753	29.356	0.933	0.0287
70	0.79	3	15	674.7325	6.764686	72.0691	29.7986	0.932	0.031
40	0.32	1	16	699.8096	2.113286	52.798	30.8152	0.8222	0.07808
40	0.32	2	17	724.8868	2.11605	55.6847	31.2029	0.8344	0.0701
40	0.32	3	18	749.964	2.062079	53.8808	30.6514	0.8285	0.0712
10	0.85	1	19	816.5752	2.495886	61.0584	32.456	0.8952	0.042
10	0.85	2	20	883.1864	2.520514	62.985	29.186	0.8977	0.0434
10	0.85	3	21	949.7976	2.505529	61.0581	29.8639	0.8956	0.0456
100	0.4	1	22	981.1441	8.709564	62.1457	29.551	0.8809	0.051
100	0.4	2	23	1012.491	8.804207	60.9789	31.6326	0.8811	0.0544
100	0.4	3	24	1043.837	8.610229	59.3866	31.1957	0.8812	0.0521
10	0.4	1	25	1075.183	1.690429	52.2744	31.7192	0.7962	0.084
10	0.4	2	26	1106.53	1.685571	52.9881	30.6631	0.7919	0.0855
10	0.4	3	27	1137.876	1.723443	59.5982	32.6467	0.5731	0.1565
100	0.23	1	28	1155.901	5.182893	53.3846	32.1763	0.8251	0.0706
100	0.23	2	29	1173.925	4.542164	42.7674	31.0102	0.6033	0.1334
100	0.23	3	30	1191.949	3.760886	61.7685	31.7414	0.8302	0.073

### Mouse 6a Artery

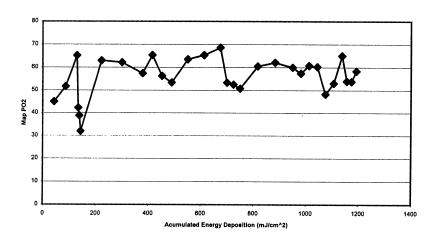


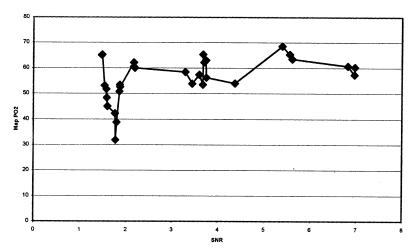


## Mouse6a

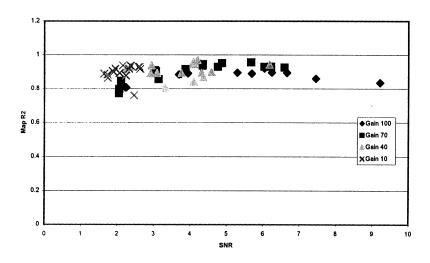
Gain		Exposure 1	Relative Irr Cum	ulative	Accumulate	SNR	PO2 Mean	PO2 St. D∈F	R2 Mean	R2 St. Dev
	10	0.55	1	1	43.10138	1.59845	45.0042	29.1851	0.7246	0.1119
	10	0.55	2	2	86.20276	1.575086	51.6795	30.9596	0.7418	0.1035
	10	0.55	3	3	129.3041	1.480793	65.2168	33.7728	0.7545	0.1029
	100	0.06	1	4	134.0061	1.761621	42.2214	33.8521	0.5307	0.0168
	100	0.06	2	5	138.7081	1.798329	38.8014	31.7598	0.4969	0.1708
	100	0.06	3	6	143.41	1.77115	31.8993	27.8824	0.5065	0.1622
	40	1	1	7	221.7762	3.737871	62.973	30.1596	0.8852	0.0512
	40	1	2	8	300.1423	3.698029	62.1602	30.1193	0.9089	0.0396
	40	1	3	9	378.5085	3.594121	57.3765	27.5421	0.9029	0.0443
	70	0.47	1	10	415.3406	3.6734	65.3405	33.441	0.8398	0.0688
	70	0.47	2	11	452.1726	3.74505	56.2466	31.1747	0.8457	0.0689
	70	0.47	3	12	489.0047	3.669836	53.4364	30.1142	0.8416	0.0686
	70	0.79	1	13	550.914	5.616071	63.4912	30.5935	0.8961	0.0454
	70	0.79	2	14	612.8232	5.558986	65.3312	30.5295	0.8959	0.0436
	70	0.79	3	15	674.7325	5.400007	68.5534	31.195	0.8979	0.0434
	40	0.32	1	16	699.8096	1.866543	53.3638	33.2487	0.7561	0.0984
	40	0.32	2	17	724.8868	1.875314	52.4893	32.6618	0.75	0.1013
	40	0.32	3	18	749.964	1.861321	50.7679	32.6359	0.7472	0.1015
	10	0.85	1	19	816.5752	2.172771	60.5152	32.4011	0.85	0.0736
	10	0.85	2	20	883.1864	2.170229	62.1143	32.2467	0.8554	0.0596
	10	0.85	3	21	949.7976	2.193186	59.9848	32.0708	0.8482	0.0662
	100	0.4	1	22	981.1441	6.969193	57.3756	30.6339	0.837	0.0681
	100	0.4	2	23	1012.491	6.822393	60.7537	31.5668	0.8489	0.0622
	100	0.4	3	24	1043.837	· 6.97665	60.2811	31.8092	0.8377	0.0685
	10	0.4	1	25	1075.183	1.584471	48.2846	30.6572	0.7309	0.1075
	10	0.4	2	26	1106.53	1.533786	53.0867	32.2792	0.741	0.1042
	10	0.4	3	27	1137.876	1.472107	65.0854	33.8918	0.7595	0.1016
	100	0.23	1	28	1155.901	4.37225	53.9694	31.3088	0.7872	0.0858
	100	0.23	2	29	1173.925	3.440464	53.8152	32.6526	0.726	0.1056
	100	0.23	3	30	1191.949	3.291336	58.3846	32.8472	0.7777	0.0897

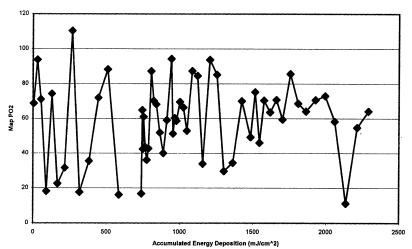


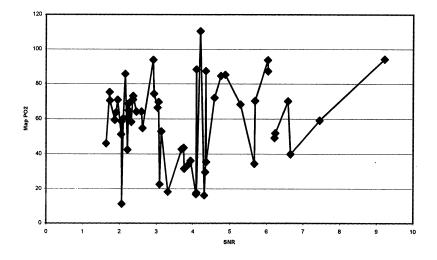




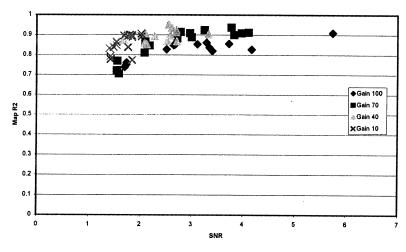
Gain		Exposure 1	Relative Irr Cu	mulativ	e Accumula	tı SNR	PO2 Mean	PO2 St. D€	D2 Maan	D0 04 D
	40	0.32	1		4.606299		68.8044	31.2106		R2 St. Dev
	40	0.32	2	2				22.9927	0.916	0.0405
	40	0.32	3	3			71.1036	31.2493	0.8931	0.0465
	40	0.49	1	4			18.1823	8.0122	0.9292	0.0314
	40	0.49	2	5			74.3462	29.6955	0.8052	0.0672
	40	0.49	3	6			22.5538		0.9386	0.0271
	40	0.66	1	7			31.5466	7.59 12.2421	0.8945	0.0417
	40	0.66	2				110.3499	24.81	0.8942	0.0387
	40	0.66	3	9			17.6724		0.9695	0.0146
	40	0.83	1	10			35.4445	9.503	0.8417	0.0682
	40	0.83	2	11			71.9903	18.2562	0.8673	0.0472
	40	0.83	3	12			88.2576	26.6711 29.4925	0.8998	0.0329
	40	1	1	13			16.1251	3.4174	0.9599	0.0185
	40	1	2	14			10.1251	3.4174	0.8952	0.0357
	40	1	3	15			16.8419	3.2154	0.9434	0.0197
	100	0.06	1	16	744.685		64.9049	32.8002	0.9454	0.0225
	100	0.06	2	17	749.2913		42.3699	26.7311	0.8072	0.0835
	100	0.06	3	18	753.8976		61.0427		0.8079	0.0758
	100	0.145	1	19	765.0295		43.5304	32.2805	0.8101	0.0765
	100	0.145	2	20	776.1614		36.1372	24.0178	0.8875	0.0467
	100	0.145	3	21	787.2933		42.6731	20.3349	0.8912	0.0447
	100	0.23	1	22	804.9508		87.2633	23.6777	0.885	0.0474
	100	0.23	2	23	822.6083		70.2286	29.6702	0.9194	0.0361
	100	0.23	3	24	840.2657	5.29257	68.2215	31.1108	0.8894	0.0461
	100	0.315	1	25	864.4488		51.9048	31.8766	0.8955	0.0461
	100	0.315	2	26	888.6319	6.65763	39.9473	27.1945	0.8963	0.0429
	100	0.315	3	27	912.815	7.455037	59.0961	21.8943	0.894	0.0455
	100	0.4	1	28	943.5236		94.2311	30.0235	0.8604	0.0563
	70	0.15	1	29	955.0394		51.2416	28.8572 31.2838	0.835	0.0287
	70	0.15	2	30	966.5551	2.103807	60.2566	30.4709	0.7728	0.0908
	70	0.15	3	31	978.0709	2.057526	58.6069	31.2342	0.8473	0.0682
	70	0.31	1	32	1001.87		69.5822	31.6809	0.7996	0.0821
	70	0.31	2	33	1025.669		66.3983	29.546	0.9031 0.9103	0.0419
	70	0.31	3	34	1049.469	3.132519	52.9377	28.4965	0.8567	0.0378
	70	0.47	1	35	1085.551	4.344667	87.2942	29.948	0.8367	0.0581
	70	0.47	2	36		4.756748	84.5099	30.4683		0.0238
	70	0.47	3	37	1157.717	3.872119	33.8376	14.7263	0.93 0.9166	0.0312
	70	0.63	1	38	1206.083	6.0336	93.6515	29.4582	0.9305	0.0342
	70	0.63	2	39	1254.449	4.875333	85.1731	30.1613	0.9523	0.0293
	70	0.63	3	40	1302.815	4.334222	29.5939	9.4831	0.9366	0.0215
	70	0.79	1	41	1363.465		34.4212	10.1276	0.9564	0.0253
	70	0.79	2	42	1424.114		70.0455	26.2873	0.9267	0.019
•	70	0.79	3	43	1484.764		49.1708	21.5662	0.9207	0.0273 0.0271
	10	0.4	1	44	1515.472	1.733859	75.2444	32.2363	0.8833	0.0271
	10	0.4	2	45	1546.181	1.6388	46.0037	25.2196	0.8889	0.0302
	10	0.4	3	46	1576.89	1.7436	70.4221	34.0038	0.8644	0.0549
•	10	0.55	1	47	1619.114	1.907163	63.6227	29.8465	0.9001	0.0349
•	10	0.55	2	48	1661.339	1.9518	70.7966	31.3566	0.9186	0.0431
•	10	0.55	3	49	1703.563	1.873022	59.425	28.1104	0.9051	
•	10	0.7	1	50		2.156059	85.6312	29.4138	0.9051	0.0413 0.0273
•	10	0.7	2	51		2.239696	68.6899	31.5558	0.9374	0.0273
•	10	0.7	3			2.457726	64.1286	31.8605	0.7605	0.0509
1	10	0.85	1			2.359963	70.6842	29.5201	0.7605	0.0918
1	10	0.85	2			2.371037	73.0027	30.0614	0.9374	0.0276
1	10	0.85	3			2.319556	58.2536	27.1059	0.9367	0.0276
1	0	1	1			2.067259	11.1294	2.1751	0.894	0.0347
	0	1	2		2214.094		54.75	25.4091	0.9178	0.0328
1	0	1	3		2290.866		64.1275	27.2512	0.9288	0.0336
								_ · · · -	3.0200	3.0213

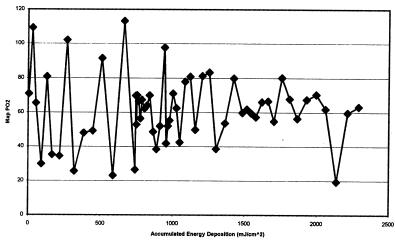


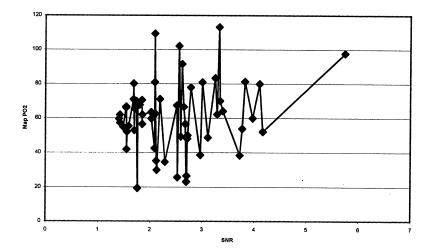




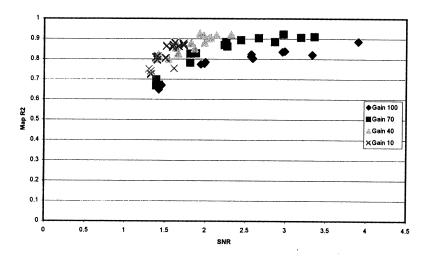
<u>.</u>										
Gain	40	Exposure 1						PO2 St. D€	R2 Mean	R2 St. Dev
	40	0.32	1	1			70.8455	30.6055	0.8755	0.0567
	40	0.32	2	2			109.2541	38.9873	0.8609	0.0577
	40	0.32	3	3			65.4583	30.5117	0.9023	0.0436
	40	0.49	1	4			29.8225	15.9387	0.8525	0.0565
	40	0.49	2	5			80.8359	32.6677	0.9106	0.038
	40	0.49	3	6			35.2091	18.5705	0.8542	0.0495
	40	0.66	1	7			34.5426	17.6597	0.8929	0.045
	40	0.66	2	8	267.9331		102.0563	28.6738	0.9522	0.0222
	40	0.66	3	9			25.5898	12.69	0.8706	0.0523
	40	0.83	1	10			47.9954	24.9178	0.8683	0.051
	40	0.83	2	11	446.0433		49.2206	22.6919	0.8982	0.0378
	40	0.83	3	12	509.7638		91.487	31.7326	0.9345	0.0305
	40	1	1	13	586.5354		23.0843	6.8782	0.9129	0.0317
	40	1	2	14			113.1708	21.8803	0.9041	0.0339
	40	1	3	15	740.0787		26.42	7.7907	0.9232	0.0325
	100	0.06	1	16	744.685		69.7565	32.0596	0.751	0.1026
	100	0.06	2	17	749.2913		52.8509	31.8979	0.7383	0.1031
	100	0.06	3	18	753.8976		69.9195	32.8344	0.7611	0.1022
	100	0.145	1	19	765.0295		66.4552	30.6936	0.8489	0.0647
	100	0.145	2	20	776.1614		56.4394	29.1715	0.8523	0.0619
	100	0.145	3	21	787.2933		67.323	32.3404	0.8276	0.0752
	100	0.23	1	22	804.9508	3.2918	62.1198	30.8858	0.8616	0.0615
	100	0.23	2	23	822.6083		64.044	34.0146	0.82	0.0772
	100 100	0.23	3	24	840.2657	3.348533	69.9095	33.634	0.8372	0.0727
	100	0.315	1	25	864.4488	3.112889	48.6219	27.658	0.8539	0.0569
	100	0.315	2	26	888.6319	3.726667	38.4066	22.0276	0.8561	0.0596
	100	0.315 0.4	3	27	912.815	4.166615	52.0204	29.6071	0.8271	0.0683
	70	0.4	1	28	943.5236	5.740933	97.6957	25.6182	0.9102	0.0387
	70	0.15	1 2	29	955.0394	1.550393	41.8279	27.4844	0.7219	0.1023
	70	0.15	3	30 31	966.5551	1.559015	52.0781	31.1217	0.77	0.094
	70	0.13	1	32	978.0709	1.589844	55.3086	31.3081	0.7057	0.1217
	70	0.31	2	33	1001.87 1025.669	2.189637	70.9532	34.4801	0.8472	0.0636
	70	0.31	3	34	1025.669	2.104674	62.4106	30.1482	0.8676	0.0567
	70	0.47	1	35	1049.469	2.087281 2.784081	42.4885	25.2776	0.8108	0.0743
	70	0.47	2	36	1121.634		77.8774	31.3127	0.9147	0.038
	70	0.47	3	37	1157.717	3.00583 2.722074	80.8444	32.0801	0.889	0.0474
	70	0.63	1	38	1206.083	3.826711	49.8552	24.7003	0.8827	0.0473
	70	0.63	2	39	1254.449	3.255156	81.2233	29.8977	0.9007	0.0457
	70	0.63	3	40	1302.815	2.968852	83.2558	29.6647	0.9241	0.0335
	70	0.79	1	41	1363.465	3.773815	38.5874 53.7616	17.805	0.9089	0.0359
	70	0.79	2	42	1424.114		79.8841	21.4293 31.1844	0.9377	0.0261
	70	0.79	3	43	1484.764	3.972096	59.8501	27.487	0.9123	0.0363
	10	0.4	1	44	1515.472	1.424985	61.8534	31.6675	0.9091	0.0357
	10	0.4	2	45	1546.181	1.405481	59.5395	31.7441	0.7936	0.0833
	10	0.4	3	46	1576.89	1.428341	57.2696	30.5162	0.8325 0.778	0.0685
	10	0.55	1	47	1619.114	1.543726	66.0749	34.059	0.778	0.0948
	10	0.55	2	48	1661.339	1.545652	66.5736	34.1983	0.8652	0.0651 0.0552
	10	0.55	3		1703.563	1.486637	54.8662	29.4067	0.8387	0.0552
	10	0.7	1		1757.303	1.687356	80.1336	34.1151	0.8963	0.0719
	10	0.7	2	51	1811.043	1.765274	67.9196	34.4058	0.8382	
	10	0.7	3		1864.783	1.847481	56.4528	31.6574	0.0362	0.0659 0.0955
	10	0.85	1		1930.039	1.802681	67.5455	31.3095	0.7742	0.0933
	10	0.85	2		1995.295	1.845844	70.3832	31.0639	0.8983	0.0432
	10	0.85	3		2060.551		61.9221	31.323	0.8894	0.0443
	10	1	1		2137.323	1.762511	19.3637	5.7828	0.8948	0.0494
	10	1	2			2.028289	59.6783	28.4991	0.892	0.0379
	10	1	3			2.023119	63.3193	29.3132	0.9056	0.0399
										0.000

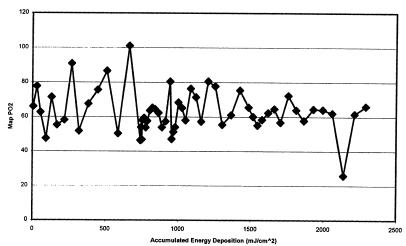


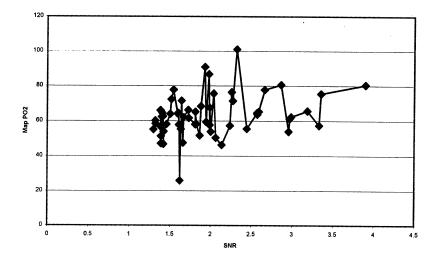




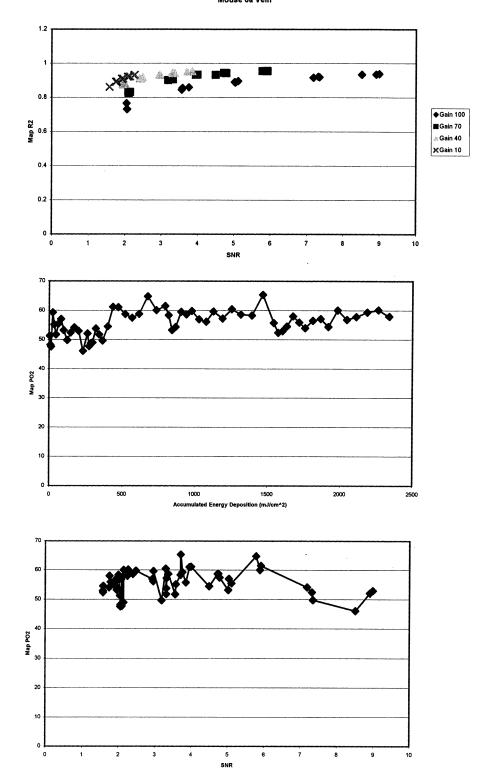
Gain	40	Exposure 1					PO2 Mean	PO2 St. De	R2 Mean	R2 St. Dev
	40	0.32	1	1			66.0312	34.0154	0.8019	0.0801
	40	0.32	2	2			77.784	33.3576	0.7984	0.0865
	40	0.32	3	3			62.688	31.9904	0.823	0.0719
	40	0.49	1	4			47.4943	28.0336	0.8263	0.0673
	40	0.49	2	5			71.4634	31.565	0.8724	0.0566
	40	0.49	3	6		1.634148	55.2751	30.2666	0.8556	0.0587
	40	0.66	1	7	217.2638	1.82417	58.1615	29.6712	0.8791	0.0518
	40	0.66	2	8	267.9331	1.928259	90.7991	28.4605	0.9262	0.0312
	40	0.66	3	9	318.6024	1.865067	51.7046	29.5919	0.8526	0.0621
	40	0.83	1	10	382.3228	1.988756	67.5634	31.8492	0.8815	0.0488
	40	0.83	2	11	446.0433	2.036185	75.6843	32.2844	0.9023	0.0413
	40	0.83	3	12	509.7638	1.978185	86.6363	33.1054	0.9153	0.037
	40	1	1	13	586.5354	2.062859	50.3835	27.2298	0.9076	0.0398
	40	1	2	14	663.3071	2.318941	101.0003	27.5538	0.9217	0.0333
	40	1	3	15	740.0787	2.136119	46.2956	23.7173	0.919	0.0358
	100	0.06	1	16	744.685	1.423081	53.9747	34.1192	0.6485	0.1384
	100	0.06	2	17	749.2913	1.419022	46.7842	32.3321	0.6581	0.1322
	100	0.06	3	18	753.8976		58.1187	35.4562	0.6711	0.1368
	100	0.145	1	19	765.0295	1.943185	59.3999	32.5927	0.7741	0.0911
	100	0.145	2	20	776.1614	1.999956	53.8148	31.4264	0.7854	0.0876
	100	0.145	3	21	787.2933	1.986556	57.6375	31.4136	0.7769	0.091
	100	0.23	1	22	804.9508	2.573422	63.691	33.1865	0.8236	0.0789
	100	0.23	2	23	822.6083	2.591556	65.2326	33.3333	0.8036	0.0808
	100	0.23	3	24	840.2657	2.569689	64.4844	32.7098	0.8132	0.0796
	100	0.315	1	25	864.4488	2.987637	62.2819	33.5227	0.8393	0.0671
	100	0.315	2	26	888.6319	2.958793	53.9284	32.0208	0.8356	0.0693
	100	0.315	3	27	912.815	3.329785	57.3698	30.9929	0.8218	0.0713
•	100	0.4	1	28	943.5236	3.900837	80.4918	32.299	0.8865	0.0491
	70	0.15	1	29	955.0394	1.389541	47.1028	31.6236	0.6685	0.1315
	70	0.15	2	30	966.5551	1.391104	51.3252	33.1651	0.6993	0.121
	70	0.15	3	31	978.0709	1.422733	53.9557	34.0287	0.673	0.1277
	70	0.31	1	32	1001.87	1.880622	68.3289	33.6593	0.8284	0.0736
	70	0.31	2	33	1025.669	1.812652	65.1475	33.7344	0.8275	0.0745
	70	0.31	3	34	1049.469	1.809904	58.0019	33.8576	0.7819	0.0912
	70	0.47	1	35	1085.551	2.259415	76.3864	32.7919	0.885	0.0515
	70	0.47	2	36	1121.634	2.272785	71.3931	31.5558	0.8626	0.0582
	70	0.47	3	37	1157.717	2.238052	57.2309	31.1347	0.8702	0.056
	70	0.63	1	38	1206.083	2.8646	80.5134	32.2844	0.8855	0.0483
	70	0.63	2	39	1254.449	2.664081	77.7624	31.2216	0.9051	0.0429
	70	0.63	3	40	1302.815	2.443696	55.4961	29.5883	0.8942	0.0468
	70	0.79	1	41	1363.465	2.969593	61.0717	27.5278	0.9228	0.0326
	70	0.79	2		1424.114	3.354763	75.4166	31.4166	0.9113	0.0375
	70	0.79	3	43	1484.764	3.187311	65.5874	29.784	0.907	0.0395
	10	0.4	1	44	1515.472	1.322274	60.1128	34.4292	0.7419	0.104
	10	0.4	2	45	1546.181	1.297756	55.1515	33.5696	0.7518	0.108
	10	0.4	3	46	1576.89	1.322837	58.3417	33.2074	0.7267	0.1143
	10	0.55	1		1619.114	1.401081	62.4011	33.4096	0.7972	0.0854
	10	0.55	2		1661.339	1.405526	64.5927	31.8958	0.8138	0.0798
	10	0.55	3		1703.563	1.382644	56.8192	33.579	0.8094	0.0792
	10	0.7	1		1757.303	1.517896	72.3317	32.0207	0.8654	0.0602
	10	0.7	2			1.504911	63.9293	32.8963	0.8061	0.0822
	10	0.7	3		1864.783	1.6104	57.8424	32.2302	0.7542	0.0989
	10	0.85	1		1930.039	1.60317	64.5091	30.9498	0.8706	0.0561
	10	0.85	2			1.595178	64.1368	31.8819	0.8606	0.0588
	10	0.85	3			1.668993	62.107	32.464	0.8644	0.057
	10 10	1	1			1.622763	25.8606	13.2643	0.8809	0.0464
	10	1	2					30.8714	0.8689	0.0567
	10	1	3	58 2	2290.866	1.725452	66.1538	32.1491	0.8773	0.0522



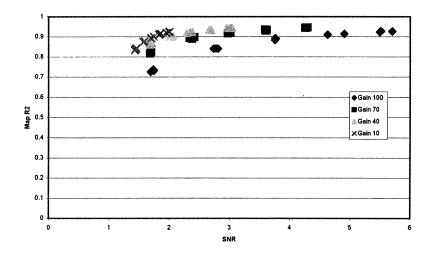


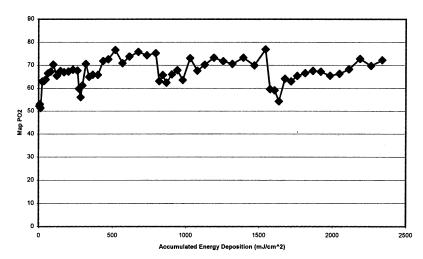


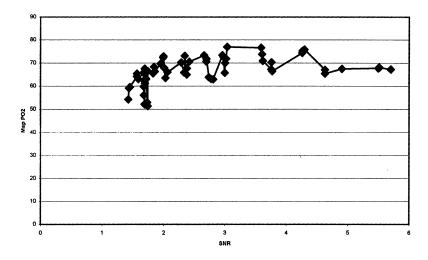
Gain		Exposure 1	Relative Im Cur	mulativ	e Accumula	t, SNR	PO2 Moan	PO2 St. D€	D2 Maar	D0 04 D
	100	0.06	1	1			51.2522			R2 St. Dev
	100	0.06	2	2					0.7657	0.0993
	100	0.06	3	3			47.5757		0.7313	0.1103
	100	0.145	1	4			59.2386		0.7309	0.1092
	100	0.145	2	5					0.8593	0.0599
	100	0.145	3	6			55.1357	30.7004	0.8557	0.0602
	100	0.23	1	7			51.7116	29.1017	0.8449	0.0649
	100	0.23	2	8			55.4518	29.0772	0.8961	0.046
	100	0.23	3	9			56.982	30.9034	0.8872	0.0476
	100	0.315	1	10			53.1879	27.7022	0.8901	0.0458
	100	0.315	2	11			49.7864	24.8386	0.9189	0.0347
	100	0.315	3	12			52.3969	24.8752	0.9223	0.034
	100	0.313	1	13			54.1517	26.7849	0.9161	0.0361
	100	0.4	2				52.9003	24.4024	0.9378	0.0273
	100	0.4	3	14			46.0958	22.0689	0.9347	0.0293
	70	0.4		15			52.0602	23.8576	0.9349	0.0279
	70		1	16	272.5512		47.7034	28.271	0.8326	0.0706
		0.15	2	17	283.9075		48.7137	28.187	0.8245	0.0719
	70	0.15	3	18	295.2638		48.9345	29.2114	0.832	0.0704
	70 70	0.31	1	19	318.7335		53.7492	27.7283	0.9057	0.0407
	70	0.31	2	20	342.2031		51.7378	26.8534	0.9081	0.0415
	70	0.31	3	21	365.6728	3.18703	49.638	26.3136	0.9016	0.043
	70	0.47	1	22	401.2559		54.4591	25.8896	0.9321	0.0304
	70	0.47	2	23	436.839		61.1229	27.2159	0.9332	0.0279
	70	0.47	3	24	472.422	3.949319	61.0035	28.2116	0.9323	0.0292
	70	0.63	1	25	520.1185	4.727763	58.693	25.4072	0.9449	0.0237
	70	0.63	2	26	567.815	4.782474	57.4444	25.6168	0.9432	0.0243
	70	0.63	3	27	615.5114	4.746578	58.75	26.2106	0.9448	0.0243
	70	0.79	1	28	675.3213	5.785104	64.7497	26.3841	0.9547	0.0194
	70	0.79	2	29	735.1311	5.890881	60.0488	24.4148	0.9542	0.0205
	70	0.79	3	30	794.9409	5.915519	61.4809	24.3235	0.9558	0.0189
	40	0.32	1	31	819.1677	1.99837	58.3149	31.9065	0.8808	0.0514
	40	0.32	2	32	843.3945	1.9532	53.2416	28.45	0.8767	0.0518
	40	0.32	3	33	867.6213	1.935326	54.2847	28.6299	0.8758	0.0551
	40	0.49	1	34	904.7185	2.452867	59.4933	30.2921	0.9107	0.0339
	40	0.49	2	35	941.8157	2.395215	58.5932	28.9138	0.9103	0.0405
	40	0.49	3	36	978.913	2.482926	59.7318	29.6266	0.9183	0.0359
	40	0.66	1	37	1028.881	2.93803	56.9624	26.015	0.9336	0.0285
	40	0.66	2	38	1078.848	2.959311	56.1154	26.2368	0.9336	0.0203
	40	0.66	3	39	1128.816	2.962926	59.6643	27.3152	0.9312	0.0292
	40	0.83	1	40	1191.654	3.324244	57.2343	24.2672	0.944	0.0299
	40	0.83	2	41	1254.493		60.4372	26.3299	0.9432	
	40	0.83	3	42	1317.331	3.368489	58.6195	25.1595	0.9424	0.0248
	40	1	1	43	1393.039		58.2919	25.13 <i>9</i> 5 25.1145		0.0249
	40	1	2	44	1468.748	3.708593	65.2939	26.4707	0.9515	0.0208
	40	1	3	45	1544.457	3.851319	55.7396		0.9517	0.0218
	10	0.4	1	46		1.578615	52.3828	23.2156	0.9533	0.0203
	10	0.4	2	47	1605.024	1.576244		28.6463	0.8615	0.0566
	10	0.4	3	48	1635.307		52.8995	29.344	0.8632	0.0592
	10	0.55	1	49	1676.947	1.583119 1.758985	54.5037	29.6446	0.8599	0.059
	10	0.55	2	50			58.0021	29.2707	0.8896	0.0479
	10	0.55	3	50 51	1718.587 1760.226	1.787104	55.8741	28.8495	0.8944	0.0451
	10	0.53				1.745015	53.9976	28.5266	0.8927	0.0471
	10	0.7	1 2	52	1813.222	1.913481	56.4832	28.5009	0.9069	0.0408
	10	0.7	3		1866.219	1.946533	57.1108	28.0541	0.9103	0.0397
	10	0. <i>1</i> 0.85				1.915956	54.4318	26.9905	0.909	0.0378
	10	0.85	1			2.141689	60.0487	28.0802	0.9245	0.0326
	10		2			2.075622	56.8497	26.839	0.9215	0.0328
		0.85	3		2112.272	2.11877	57.8371	27.5946	0.9215	0.0359
	10 10	1	1	58	2187.98		59.345	27.4214	0.9323	0.0294
	10 10	1	2		2263.689		60.1358	26.505	0.9312	0.0286
	10	1	3	60	2339.398	2.245711	57.9603	26.4987	0.9306	0.0302



Gain		Exposure 1	Relative Im	Cumulativ	Accumula	t SNR	PO2 Mean	PO2 St. De	D2 Maan	D0 04 D
	100	0.06	1	1				32.5389		R2 St. Dev
	100	0.06	2	2					0.7251	0.1117
	100	0.06	3	3				33.1555	0.7375	0.1026
	100	0.145	1	4				30.5347	0.7306	0.1135
	100	0.145	2	5				32.2955	0.8405	0.066
	100	0.145	3	6				32.674	0.841	0.0638
	100	0.23	1					32.9013	0.8402	0.0685
	100	0.23		7			66.4799	31.2111	0.8904	0.0483
	100	0.23	2	8	81.38681		67.219	31.5977	0.8829	0.0504
	100		3	9	98.7998		70.2678	31.6941	0.8925	0.0483
		0.315	1	10	122.648		65.441	29.8351	0.9097	0.0389
	100	0.315	2	11	146.4963		67.4619	29.9911	0.9142	0.0364
	100	0.315	3	12	170.3445		67.0081	30.9477	0.9099	0.0392
	100	0.4	1	13	200.628		67.2509	29.7154	0.9265	0.033
	100	0.4	2	14	230.9114		68.0288	31.7979	0.9273	0.0307
	100	0.4	3	15	261.1949	5.501074	67.7005	30.0347	0.9229	0.0348
	70	0.15	1	16	272.5512	1.675822	59.8028	31.0707	0.8176	0.0745
	70	0.15	2	17	283.9075	1.678763	56.065	30.516	0.8169	0.0743
	70	0.15	3	18	295.2638	1.696193	61.169	32.6118	0.8234	0.0787
	70	0.31	1	19	318.7335	2.41583	70.5662	32.7382	0.8985	0.0437
	70	0.31	2	20	342.2031	2.378474	64.969	29.9347	0.8896	0.0476
	70	0.31	3	21	365.6728	2.333822	65.8583	32.8095	0.8938	0.0454
	70	0.47	1	22	401.2559	2.997615	65.7786	28.0036	0.9252	0.0434
	70	0.47	2	23	436.839	3.017874	71.8051	29.6283	0.9232	0.0354
	70	0.47	3	24	472.422	2.973022	72.5883	30.323	0.9163	
	70	0.63	1	25	520.1185	3.592215	76.6084	31.32	0.9361	0.0367
	70	0.63	2	26	567.815	3.619156	70.9096	29.8143		0.0284
	70	0.63	3	27	615.5114	3.606407	73.7711		0.9345	0.0279
	70	0.79	1	28	675.3213	4.295281	75.7892	30.7518	0.9304	0.03
	70	0.79	2	29	735.1311	4.256904	74.358	29.7497	0.9463	0.024
	70	0.79	3	30	794.9409	4.263778		29.3394	0.9457	0.0241
	40	0.32	1	31	819.1677	1.719015	75.2624	29.8057	0.944	0.0238
	40	0.32	2	32	843.3945		63.0575	31.2391	0.8677	0.055
	40	0.32	3	33	867.6213	1.671622	65.743	32.5224	0.8653	0.0537
	40	0.49	1	34	904.7185	1.677726	62.4427	30.9485	0.861	0.0594
	40	0.49	2	35	941.8157	2.060993	66.0117	28.7913	0.9024	0.0381
	40	0.49	3	36		2.008822	67.8351	30.0332	0.9008	0.0435
	40	0.45	1		978.913	2.030911	63.5411	30.131	0.8984	0.0421
	40	0.66	2	37	1028.881	2.343044	73.0713	31.9102	0.9226	0.0347
	40	0.66		38	1078.848	2.380163	67.6297	30.8956	0.9241	0.0327
	40	0.83	3	39	1128.816	2.285726	70.2035	30.2747	0.9171	0.0345
	40	0.83	1	40	1191.654	2.659096	73.2779	30.2291	0.9341	0.0287
			2	41	1254.493		71.7243	30.4414	0.9334	0.0297
	40 40	0.83	3	42	1317.331	2.696096	70.5876	28.8809	0.9358	0.0293
	40 40	1	1	43	1393.039		73.3168	29.1648	0.9443	0.0233
	40	1	2	44	1468.748	3.001519	69.9585	27.4935	0.9425	0.0248
	40	1	3	45	1544.457	3.037867	76.9408	29.8755	0.9458	0.0226
	10	0.4	1	46	1574.74	1.451067	59.5751	32.0203	0.8433	0.0659
	10	0.4	2	47	1605.024	1.435281	59.121	31.8087	0.839	0.0663
	10	0.4	3	48	1635.307	1.42597	54.2659	31.4928	0.8328	0.0718
	10	0.55	1		1676.947	1.563756	64.1448	32.4539	0.8725	0.0522
	10	0.55	2		1718.587	1.586489	62.9891	30.8988	0.8781	0.0515
	10	0.55	3	51	1760.226	1.565719	65.3893	33.0551	0.8741	0.0544
	10	0.7	1			1.743089	66.5638	29.6604	0.8995	0.0417
	10	0.7	2	53		1.691289	67.5443	32.3446	0.8924	0.0457
	10	0.7	3	54		1.706126	67.2317	31.4161	0.8935	0.0476
	10	0.85	1	55		1.829096	65.4657	29.9242	0.9093	0.0395
	10	0.85	2			1.858007	66.3008	30.2654	0.9149	0.0358
	10	0.85	3			1.845096	68.2785	30.7638	0.9137	0.0356
	10	1	1	58		1.998415	72.8268	30.5513	0.9244	0.0351
	10	1	2	59		1.951222	69.7145	29.6427	0.9196	0.0357
	10	1	3			1.992756	72.2702	30.568	0.9246	0.0337
					•			33.300	3.5270	0.0040

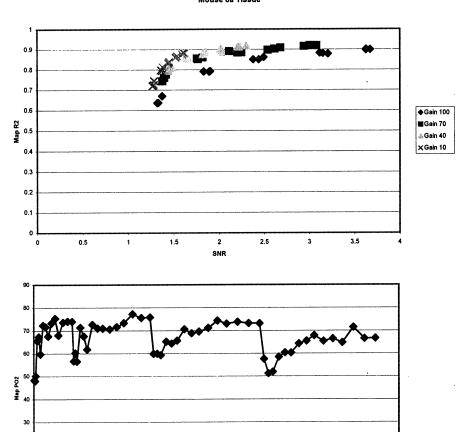


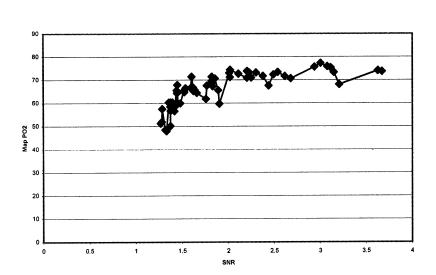




# Mouse8a

Cain		F			_					
Gain	100	Exposure 1R 0.06					PO2 Mean	PO2 St. D€	R2 Mean	R2 St. Dev
	100	0.06	1 2		1 4.5425; 2 9.08503;				0.6361	0.1464
	100	0.06	3						0.6369	0.1419
	100	0.145	1	4			50.1646		0.6702	0.1259
	100	0.145	2	5			65.5605	35.3906	0.7903	0.0934
	100	0.145	3	6			67.3054	34.6884	0.7907	0.0894
	100	0.23	1	7			59.696	34.329	0.7925	0.0925
	100	0.23	2				72.3287	32.8979	0.8615	0.0624
	100	0.23	3	8			71.6752	32.7111	0.8499	0.0653
	100	0.25	1	10			67.5771	34.8443	0.8498	0.0652
	100	0.315	2	11			73.2653	34.3795	0.8811	0.0535
	100	0.315	3	12			75.2875	33.4604	0.8824	0.0524
	100	0.4	1	13			68.0415	31.3756	0.8774	0.0562
	100	0.4	2	14			73.6296	30.4495	0.8994	0.0441
	100	0.4	3	15			74.0757	32.6875	0.9006	0.0443
	70	0.15	1	16			73.9852	33.433	0.8978	0.0455
	70	0.15	2	17			56.6847	34.2903	0.7433	0.1029
	70	0.15	3	18			60.2896	33.4264	0.7605	0.0956
	70	0.31	1	19			56.5688	31.8388	0.7762	0.0908
	70	0.31	2	20			71.3911	32.744	0.8608	0.0568
	70	0.31	3	21		1.767993	67.5699	32.1551	0.8525	0.0624
	70	0.47	1	22	365.6728		61.8384	30.1394	0.8568	0.0635
	70	0.47	2	23	401.2559 436.839		72.6717	32.5205	0.8909	0.0473
	70	0.47	3	23 24		2.249015	71.0113	31.5012	0.8849	0.0497
	70	0.63	1	2 <del>4</del> 25	472.422	2.203193	70.927	30.7979	0.8844	0.05
	70	0.63	2	25 26	520.1185	2.67983	70.6311	30.7937	0.9089	0.0397
	70	0.63	3	27	567.815 615.5114	2.614385	71.5783	30.3907	0.903	0.0414
	70	0.79	1	28	675.3213	2.53843	73.3809	33.3957	0.8977	0.0435
	70	0.79	2	29		3.003511	77.1974	30.7505	0.9196	0.0345
	70	0.79	3	30	735.1311	2.938096	75.5845	31.3405	0.9154	0.0379
	40	0.32	1	31	794.9409	3.078059	75.796	32.0106	0.9194	0.0356
	40	0.32	2	32	819.1677	1.454585	59.8533	30.0829	0.8189	0.0746
	40	0.32	3	33	843.3945	1.48097	59.9443	32.3529	0.8102	0.0747
	40	0.49	1	34	867.6213	1.442993	59.317	32.6905	0.7948	0.0868
	40	0.49	2	35	904.7185 941.8157	1.621904	65.2272	32.1569	0.8537	0.0614
	40	0.49	3	36	978.913	1.660319	64.3871	32.3502	0.8572	0.06
	40	0.66	1	37	1028.881	1.638289 1.855067	65.6546	31.9243	0.8551	0.0643
	40	0.66	2	38	1028.848		70.6107	32.4583	0.8883	0.0504
	40	0.66	3	39	1128.816	1.826452	68.8369	31.9053	0.8807	0.0516
	40	0.83	1	40	1191.654	1.821756	69.5494	32.0716	0.877	0.0545
	40	0.83	2	41	1254.493	2.019185	71.1695	31.7329	0.9027	0.0438
	40	0.83	3	42	1317.331		74.3629	31.7346	0.8869	0.0462
	40	1	1	43	1393.039	2.012104 2.2052	73.0265	31.0523	0.898	0.0467
	40	1	2	44	1468.748	2.2052	73.7654	30.2036	0.9142	0.038
	40	1	3	45	1544.457	2.300807	73.2246	31.0708	0.9136	0.0374
	10	0.4	1	46	1574.74	1.285081	73.1487	31.4915	0.9188	0.0356
	10	0.4	2	47	1605.024	1.269763	57.5078	34.6709	0.7454	0.1034
	10	0.4	3	48	1635.307	1.282578	51.2285	30.7564	0.7204	0.1184
	10	0.55	1	49	1676.947	1.373156	51.8962	31.6959	0.7254	0.1108
	10	0.55	2	50		1.378104	58.4486 60.3394	31.6444	0.796	0.0839
	10	0.55	3	51		1.357978		33.0291	0.8139	0.0789
	10	0.7	1	52	1813.222	1.445452	60.2865	32.9742	0.7979	0.0839
	10	0.7	2		1866.219	1.440244	64.2744	34.4958	0.8352	0.0688
	10	0.7	3			1.440244	65.4519	32.626	0.8303	0.072
	10	0.85	1				67.8503	32.7177	0.8396	0.0644
	10	0.85	2					31.7728	0.8606	0.0591
	10	0.85	3					31.9935	0.8671	0.056
	10	1	1	58				32.2312	0.8599	0.061
	10	1	2					32.8702	0.8837	0.05
	10	1	3					32.3265	0.8765	0.0529
		-	-		_555.556	1.020013	66.7075	31.7473	0.8825	0.0523





Accumulated Energy Deposition (mJ/cm^2)

# **Appendix F: ARVO Abstract**

The following abstract was submitted to the Association for Research in Vision and Ophthalmology, and accepted for poster presentation at the 2002 Annual Meeting, May 5-10. A travel grant was also awarded.

## IMAGING OF OXYGEN TENSION IN THE MOUSE RETINA

## **PURPOSE**

Retinal hypoxia and inadequate oxygen delivery have been implicated as causal for the development of several eye diseases, including diabetic retinopathy, glaucoma, and retinopathy of prematurity. The imaging of oxygen tension (PO<sub>2</sub>) in the retina, generated from a measure of the phosphorescence lifetimes of bolus-injected palladium-porphyrin probes has been used successfully for nearly a decade to study retinal oxygen dynamics in the cat, miniature pig, and monkey; however, the specific parameters for applying this technique in the mouse have not been thoroughly investigated. As the number of transgenic and knockout mouse models displaying characteristics of human retinal diseases rapidly increases, an ability to image PO<sub>2</sub> in these very small eyes will likely be of great benefit. In this study, we investigate the refinement of a technique for generating PO<sub>2</sub> maps in the mouse retina using our recently constructed phosphorescence lifetime imaging system.

#### **METHOD**

To accurately measure retinal  $PO_2$  in this animal, it was necessary to optimize a number of important acquisition parameters, including excitation power, intravascular probe concentration, camera exposure time, and camera intensifier gain settings. Measurements were made using both an in vitro calibration system and in vivo experiments in mice. Appropriate ranges for the stated parameters were determined using relationships between camera signal-to-noise values and the coefficient of determination ( $R^2$ ) generated from the least-squares analysis used to produce the  $PO_2$  maps.

#### RESULTS

 $R^2$  decreased with increasing intensifier gain (at the same signal-to-noise ratio), with the highest gain setting for the camera (255) producing unacceptable fits. Intensifier gain settings of 10 and 100 yielded  $R^2$  values above 0.90 with exposure times of 440 ms and 43 ms, respectively. Thus, moderate intensifier gain (near 100) reduced exposure time dramatically without significantly affecting the fits. The determined ranges for these parameters are currently being applied to the in vivo experiments, where excitation power and intravascular probe concentration will also be varied to study the effects of probe excitation on mouse retinal physiology.

## CONCLUSION

Determination of these parameters will allow a more efficient and effective method for creating oxygen maps in the mouse retina. Investigation of how changes in retinal oxygen tension correlate with ocular disease progression in cases where abnormalities in the delivery and consumption of oxygen are thought to be contributing factors, such as diabetic retinopathy, will then be possible.

# Appendix G: Sigma Xi MS Research Award Executive Summary

The following executive summary was submitted to the Worcester Polytechnic Institute Chapter of Sigma Xi, the Scientific Research Society, in nomination for their annual MS Research Award. The project was granted the award for 2002.

## Introduction and Specific Aims

Retinal hypoxia has been recognized as a causal factor in the development of numerous eye diseases, including diabetic retinopathy, retinopathy of prematurity, and glaucoma. An ability to measure oxygen tension non-invasively in the eye would significantly advance our understanding of oxygen's role in these diseases. Recently, a phosphorescence lifetime imaging technique has been developed in the laboratory of Ross Shonat for measuring oxygen tension in the eye, and has important implications for the study of retinal oxygenation in mouse models of all of these serious diseases. It will be used specifically at WPI to study diabetic retinopathy.

While the phosphorescence lifetime imaging technique has become recognized in the literature, the specific parameters for data collection and analysis in the mouse eye have not been thoroughly investigated. This goal of this project was to examine these parameters in an effort to optimize the phosphorescence lifetime imaging technique for measuring oxygen tension in the mouse retina. The specific aims for achieving the goal of optimization were:

- 5. To calibrate the phosphorescence lifetime imaging system *in vitro* using known oxygen concentrations
- 6. To determine appropriate parameters for optimal excitation of the probe, including energy and power of the excitation light
- 7. To determine optimal procedures for image collection and analysis, including camera exposure time and intensifier gain

# Background

Phosphorescence lifetime imaging is the marriage of techniques in physiology, pathology, imaging, and microscopy. Understanding its application to the diabetic mouse eye requires study of the pathogenesis of diabetic retinopathy and the basics of imaging and microscopy. The following sections provide background in these areas.

#### Diabetes and Diabetic Retinopathy

Diabetes is a disease characterized by the body's inability to produce insulin or utilize it efficiently. There exist two forms of diabetes: type-1, also known as juvenile-onset or insulin-dependent diabetes mellitus, and type-2, also known as adult-onset or non-insulin dependent diabetes mellitus. The greatest risk for complications, including diabetic retinopathy, exists in type-1 patients. Major risk factors in complications include abnormalities in blood glucose and/or levels of insulin, usually resulting from poor glycemic control.

Diabetic retinopathy is the most common microvascular complication of diabetes. Within 20 years of developing diabetes, more than 80% of type-1 patients have some degree of retinopathy. The disease is the leading cause of blindness among Americans of working age.

Diabetic retinopathy enters its earliest clinical stage when microaneurysms begin to form. These abnormalities manifest themselves as minute bulges or outpouchings on the retinal capillaries. Increased vascular permeability follows, reflecting an alteration in the blood-retinal barrier. Fluid begins to accumulate in the retina at this stage, accompanied by hard exudates (yellow-white discrete patches of lipid that occur in rings around leaking capillaries) and cotton wool spots (areas of dense, scar-like tissue), resulting in obscured vision. Ultimately, capillary nonperfusion, ischemia, and hypoxia result.

In the proliferative stages of the disease, new blood vessels begin to grow, possibly induced by the ischemic/hypoxic state of the retina. These new vessels are fenestrated capillaries and are thus extremely fragile and prone to hemorrhage. The new vessels grow out of the retina and into the vitreous, causing vitreal scarring and shrinkage. This traction pulls on the fragile new vessels, causing retinal traction, retinal tears, vitreous hemorrhage, and retinal detachment (which results in blindness).

The pathogenesis of diabetic retinopathy is thought to be related to hypoxia. It is not completely understood whether a change in oxygen consumption causes the alterations in vascular responses to

compensate for changes in blood flow, or if the changes in blood flow cause alterations in oxygen consumption. However, it is understood that, by the time capillary closure and nonperfusion are clinically apparent, the retinal tissue is hypoxic, and the primary stimulus for neovascularization is hypoxia.

The two most common treatments for diabetic retinopathy are vitrectomy and panretinal photocoagulation. These are aimed at relieving hypoxia and slowing the neovascularization process, hopefully reducing the risk of visual loss. The treatments tend to improve oxygenation in the ischemic and hypoxic retina. Progression of diabetic retinopathy can often be prevented with good glycemic control of diabetic patients; the progress of the disease may be stopped in its very early stages if blood glucose is strictly regulated. For all forms of treatment, early detection of the disease is essential; once the cascade of prolifereative retinopathy has begun, little can be done to save the sight of the patient.

Numerous animal models, including dogs, cats, rats, and mice, have been developed for diabetic retinopathy. Mouse models for the disease have gained prominence due to the similarity between the human and mouse retinas, the relatively quick breeding time for mice, and the ease of working with these animals in a laboratory setting. The ability to study the changes in oxygen tension in these diabetic mouse eyes will likely be of great benefit to diabetic retinopathy research.

### Phosphorescent Probe for Intravascular PO<sub>2</sub> Measurements

Light-emitting probes have received considerable attention in the literature as imaging aids. Chemicals that may be injected into the bloodstream, and that emit light when excited, have numerous implications for the study of blood vessels. Additionally, the phosphorescent probe used in this study, palladium meso-tetra porphrine, has the favorable quality of being sensitive to oxygen molecules in the bloodstream.

Phosphorescence is defined as the emission of light during a transition from an excited triplet state to the ground state. When a large number of phosphorescent molecules are excited simultaneously, the resultant total light emission can be represented by the function:

$$I(t) = I_0 \exp(-t/\tau)$$

where I(t) is the phosphorescence intensity as a function of time,  $I_0$  is the initial, maximum intensity at t = 0, t is the time post-excitation, and  $\tau$  is the lifetime of the decay.

When the phosphorescent probe is excited by light that has been sinusoidally modulated, the phosphorescence emitted will have the same frequency, but will have lower amplitude and be delayed in phase by an angle  $\theta$ .  $\theta$  is related to the probe lifetime by the following equation:

$$\tan \theta = \omega \tau$$

where  $\omega$  is the excitation frequency.

A phosphorescent molecule that has been excited to the triplet state may transfer its energy to another molecule without light emission, a phenomenon termed *quenching*. Such interactions between phosphors and their environment are common; the spin-forbidden transition from the triplet state to the ground has a relatively long lifetime (on the order of ms), and increases the probability of contact between molecules. In blood, the only significant quenching agent is oxygen. The efficiency of phosphorescence quenching depends on the frequency of collision between the excited triplet state molecule and the quencher before the phosphor returns to the ground state, and is therefore dependent on the concentration of oxygen in the vicinity of the probe. This relationship is represented by the Stern-Volmer equation for an oxygen-quenched probe:

$$\tau_0 / \tau = 1 + k_0 \tau_0 [PO_2]$$

where  $k_Q$  is the bimolecular rate constant (or quenching constant), and  $[PO_2]$  is the oxygen concentration. In a zero oxygen environment,  $\tau = \tau_0$  and the lifetime is at a maximum.

# Phosphorescence Lifetime Imaging of Oxygen Tension

Phosphorescence lifetime imaging requires a unique microscopic instrument (Figure 1). An illuminating beam is emitted by a xenon arc lamp, sinusoidally modulated using an optical chopper, and filtered to 524±20 nm (the excitation wavelength of the phosphorescent probe used in this study) by a monochromator. The light is then reflected down into the objective by a dichromatic mirror. This light excites the phosphorescent molecules in the specimen to the triplet state, and phosphorescence is emitted

during the decay of the molecules back to their ground states. This emitted light then passes straight through the dichromatic mirror to the CCD camera, which transmits the image to the PC-based image analysis system.

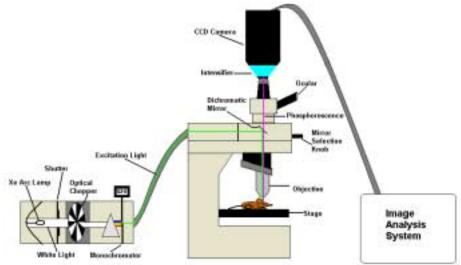


Figure 1—The phosphorescence lifetime imaging system

A phase-sensitive measure of the phosphorescence lifetime in the presence of oxygen is possible when the delivered excitation light and the sensitivity of the collection system (intensifier) are independently modulated and the phase relationship between these two elements is accurately varied. Intensity images (Figure 2) may then be taken with varying intensifier phase delays, and a graph of intensity versus phase delay may be constructed. This graph may be used in conjunction with the following equation to determine the phosphorescence phase delay,  $\theta$ :

$$I(\theta_D) = k[Pd]\{1 + m_D m cos(\theta - \theta_D)\}$$

where  $I(\theta_D)$  is the intensity, k is a constant, [Pd] is the probe concentration,  $\theta_D$  is the phase delay of the intensifier sensitivity, and m and  $m_D$  are parameters defined as:

$$(1+\omega^2\tau^2)^{-1/2}$$

for the excitation/emission and intensifier sinusoids, respectively. A best-fit estimate for  $\tau$  may then calculated using linear regression. This value of  $\tau$  may be used in the Stern-Volmer equation to calculate PO<sub>2</sub> maps (Figure 2).

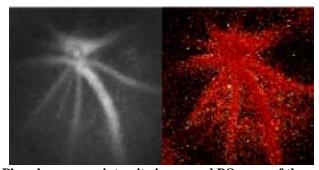


Figure 2—Phosphorescence intensity image and  $PO_2$  map of the mouse retina

# Methods and Results

In Vitro System

An *in vitro* system was designed and constructed to calibrate the probe prior to data collection and to determine approximate gain settings and exposure times required to produce acceptable oxygen maps (Figure 3). The system includes a length of Tygon® tubing, into which a solution consisting of albumin stock solution, NaCl, glucose, and probe is injected. A peristaltic pump is used to circulate the fluid through the system. The phosphorescent solution flows through an oxygenator used to apply gas mixtures with known oxygen concentrations. Upon leaving the oxygenator, the solution then flows through a glass capillary tube situated under a microscope equipped with the phosphorescence lifetime imaging system. The phosphorescence lifetime is then measured as previously described, and a PO<sub>2</sub> map is generated.

Signal-to-noise ratios (SNR) were used to determine appropriate gain settings and exposure times for subsequent *in vivo* experiments. A physiological oxygen concentration of 40 mm Hg (5% oxygen applied using the oxygenator) was applied to the probe solution. Exposure times were tested at random in an attempt to achieve a maximal range of SNR for camera intensifier gain settings 10, 100, and 255. Exposure times yielding SNR of approximately 2 and approximately 225 were noted for each gain.

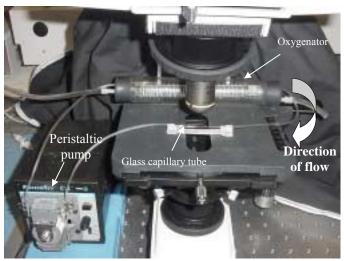


Figure 3—In vitro phosphorescence lifetime imaging system

Phosphoresce lifetime images were then taken at a range of ten exposure times equally spaced between the time yielding SNR  $\approx$  2 and the time yielding SNR  $\approx$  225. R<sup>2</sup> maps, which demonstrate the integrity of the fit between the phosphorescence intensity data and the equation  $I(\theta_D) = k[Pd]\{1 + m_D m cos(\theta - \theta_D)\}$ , were then created. From these maps, the average R<sup>2</sup> value for the entire capillary tube was determined. These values were plotted versus SNR for each gain setting (Figure 4).

These data indicate that a gain setting of 255 does not produce images with acceptable  $R^2$  values, regardless of the SNR. Conversely,  $R^2$  values of greater than 0.9 were obtained with gain settings 10 and 100 for all SNR > 50. These results were verified in later experiments for a full range of physiological oxygen concentrations. As a result, all subsequent experiments were conducted at gain settings between 10 and 100. Since the data indicate that all SNR > 50 yield similarly high  $R^2$  values, exposure times resulting in signal-to-noise ratios of 50 or less were used, thereby minimizing excitation light exposure.

The correspondence between the  $PO_2$  values indicated by the map and those applied using the gas mixer and oxygenator was used to calibrate the system to provide accurate measures of  $PO_2$  within the vasculature. It was discovered using the *in vitro system* that the data analysis program as it existed assigned different  $PO_2$  values to image sets taken with different gain settings and exposure times. The identification of this problem allowed the adjustment of the program parameters and the production of accurate oxygen maps.

#### In Vivo System

Mice used in the study were handled according to the Institutional Animal Care and Use Committee protocols. Mice were anesthetized with an avertin/saline solution and situated in a stereotaxic

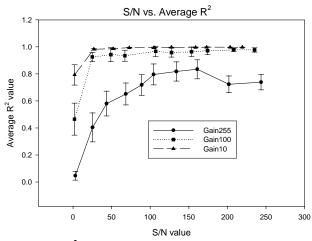


Figure 4—Average R<sup>2</sup> value versus SNR for gain settings 10, 100, and 255

head holder to prevent movement during experimentation. Mouse eyes were dilated, hydrated with an ophthalmic ointment, and shielded with a cover glass to allow observation of retinal vessels at the back of the eye. A solution of Pd meso-Tetra (4-carboxyphenyl) Porphrine probe was injected into the femoral vein in the amount of 10 mg/kg.

Gain and exposure time settings were determined *in vivo* using the *in vitro* experiments as a guide. SNR values were calculated using gain settings 10, 40, 70, and 100. Quality of oxygen maps (determined by average R<sup>2</sup> value) improved with SNR of up to about 15, after which quality remained constant. When ranges of exposure times yielding SNR between three and 15 were used for each gain, it was determined that exposure times of greater than one second caused damage to the retinal vessels (indicated by lack of blood flow). As such, a new range of exposure times resulting in SNR between three and 15 without exceeding one second was determined (Table 1).

Gain setting	Exposure time range (seconds)
100	0.058 - 0.402
70	0.15 - 0.79
40	0.32 - 1.0
10	0.4 - 1.0

Table 1—Exposure times yielding a range of SNR between approximately 3 and 15, without exceeding 1.0 seconds

Experiments were also conducted with repeated exposures of 0.23 seconds at gain 100 and 1.0 seconds at gain 40. Average  $PO_2$  was plotted versus accumulated light exposure, and it was determined that extended light exposure (greater than 1000 mJ/cm<sup>2</sup>) actually cause a decrease in vessel  $PO_2$ . Such decreases were not observed with shorter terms of light exposure.

### **Conclusions**

The phosphorescence lifetime imaging system may be used on the mouse eye with accurate and reliable results. Gain settings between 10 and 100 will yield acceptable intensity images and oxygen maps. Exposure times have been determined for each gain setting. Longer exposure times yield intensity images and maps of better quality—however, care must be taken not to exceed cumulative light exposure of  $1000 \, \text{mJ/cm}^2$  over the course of the experiment due to the risk of retinal damage and decrease in retinal  $PO_2$ . If longer exposure times are necessary, power of excitation light must be decreased.

The phosphorescence lifetime imaging system will be used to study retinal oxygenation changes in mouse models of diabetic retinopathy. Understanding the changes in oxygenation at different stages of this serious disease may assist in developing and administering treatments and cures. The noninvasive nature of the technique makes its application to human patients a potential option. Detection of hypoxia using phosphorescence lifetime imaging may allow for early detection and treatment of diabetic retinopathy, potentially preventing blindness.