Design of a Hybrid Ski Touring Binding System

Jacqueline Aaron, Conor Daly, and Eric Heiman

Meet the Team

Jackie Aaron



Conor Daly



Eric Heiman



Introduction

- Our experience with equipment has led us to find deficiencies
- Many bindings good at one thing: long backcountry missions, short tours, resort laps
- No binding serves all purposes without compromises

Objective

- Create a system than interchanges between an alpine resort style and uphill touring style ski binding that satisfies two use cases:
 - Ascend and descend on a touring binding
 - Ascend on a touring binding and descend on an alpine binding

Disciplines of Skiing

Alpine Skiing

- Lift serviced terrain
- Defined safety standards
- Performance oriented
- Used for descent only



Backcountry Skiing

- Human-powered access
 Developing safety standards
 Lightweight oriented
- Used for ascent and descent



Mechanics of Ski Bindings: Alpine vs Touring

Alpine Bindings

- Always fixed at the heel and toe
- Held by forward and downward pressure from the heel piece
- Releasable at the heel and toe
- Provide suspension and power transfer



Tech Bindings

- Fixed at the toe while ascending
- Fixed at the toe and heel while descending
- Held by clamping force of the toe piece and 'floating' pins at the heel
- Limited suspension and power transfer





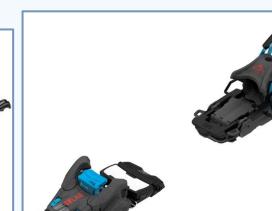
Toe Piece

Heel Piece

Current Market options

Salomon Shift

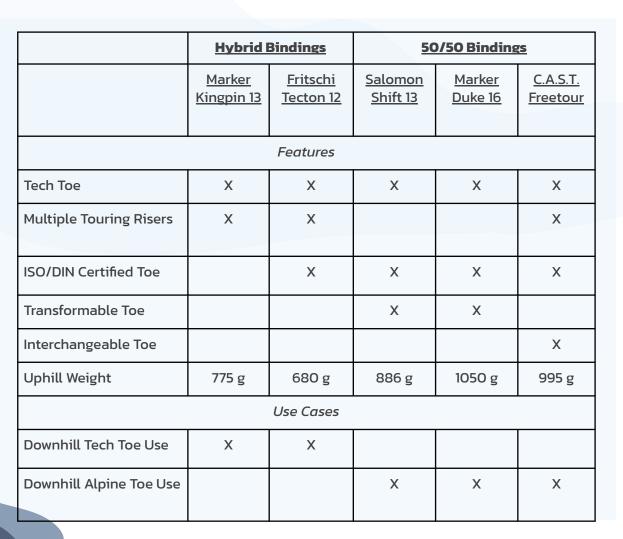
Fritschi Tecton



C.A.S.T. Freetour System



The State of the Art



Reasoning for product's development

Rational:

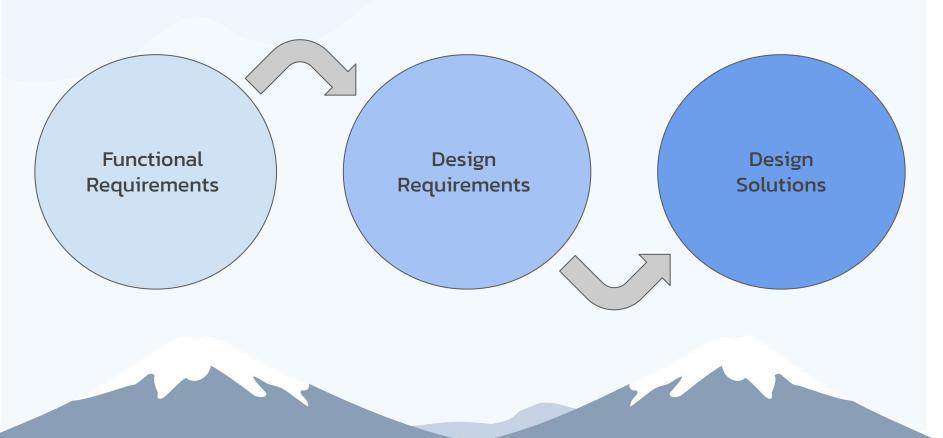
To support the need for a high performing setup that can be used in the resort and the backcountry

Ethos of Each Discipline

Alpine Skiing

Backcountry Skiing

- Unconcerned with weight savings as uphill use is not a part of alpine skiing
- Prioritize safety and performance features
- Expect gear to perform at a high level
- Desire for safety and performance features
- Prioritize lightweight gear over safety features and performance
- More cautious mentality of how a slope will be skied



Functional Requirements (FR)

FR1: Transmit skiing loads
FR1.1: Transmit uphill
skiing loads
FR1.2: Transmit
descending skiing loads



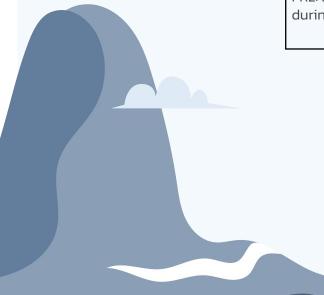
Functional Requirements (FR)	Design Requirements (DR)
FR1: Transmit skiing loads FR1.1: Transmit uphill skiing loads FR1.2: Transmit descending skiing loads	DR1: System for transmitting skiing loads DR1.1: System that allows for free movement of heel about secure pivot point at toe DR1.2: System that firmly holds heel in place

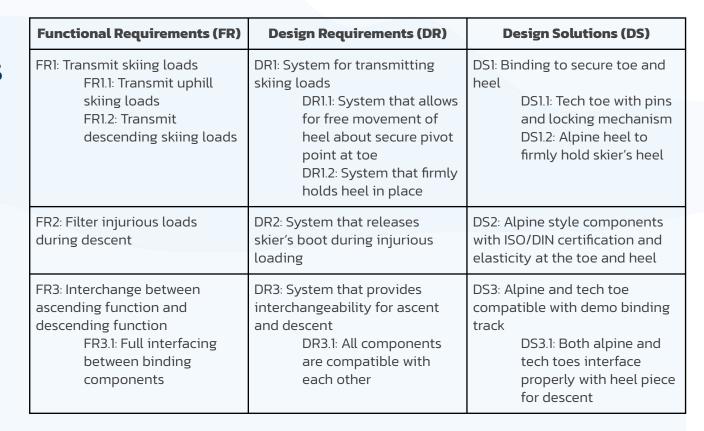


Functional Requirements (FR)	Design Requirements (DR)	Design Solutions (DS)
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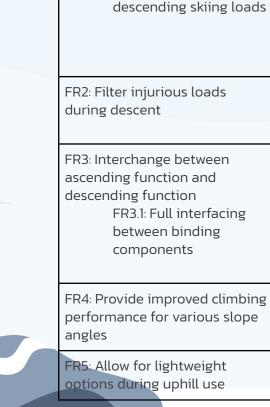


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FR2: Filter injurious loads during descent	DR2: System that releases skier's boot during injurious loading	DS2: Alpine style components with ISO/DIN certification and elasticity at the toe and heel





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FR2: Filter injurious loads during descent	DR2: System that releases skier's boot during injurious loading	DS2: Alpine style components with ISO/DIN certification and elasticity at the toe and heel	
FR3: Interchange between ascending function and descending function FR3.1: Full interfacing between binding components	DR3: System that provides interchangeability for ascent and descent DR3.1: All components are compatible with each other	DS3: Alpine and tech toe compatible with demo binding track DS3.1: Both alpine and tech toes interface properly with heel piece for descent	
FR4: Provide improved climbing performance for various slope angles	DR4: System to improve climbing position on steep slope angles	DS4: Touring risers to elevate heel during ascent of steeper slopes	



FR1: Transmit skiing loads		
FR1.1: Transmit uphill		
skiing loads		
FR1.2: Transmit		

Functional Requirements (FR)

descending skiing loads

DR1: System for transmitting skiing loads

Design Requirements (DR)

DR1.1: System that allows for free movement of heel about secure pivot point at toe DR1.2: System that firmly holds heel in place

DR2: System that releases

DR3: System that provides

DR4: System to improve

slope angles

climbing position on steep

loading

skier's boot during injurious

heel DS1.1: Tech toe with pins and locking mechanism DS1.2: Alpine heel to firmly hold skier's heel

DS2: Alpine style components with ISO/DIN certification and

elasticity at the toe and heel

compatible with demo binding

DS3: Alpine and tech toe

track

Design Solutions (DS)

DS1: Binding to secure toe and

FR3: Interchange between ascending function and descending function FR3.1: Full interfacing between binding components

interchangeability for ascent and descent DR3.1: All components are compatible with each other

tech toes interface properly with heel piece for descent DS4: Touring risers to elevate heel during ascent of steeper

DS3.1: Both alpine and

FR5: Allow for lightweight options during uphill use

DR5: Removable components during uphill use

slopes DS5: Removable heel piece on demo track

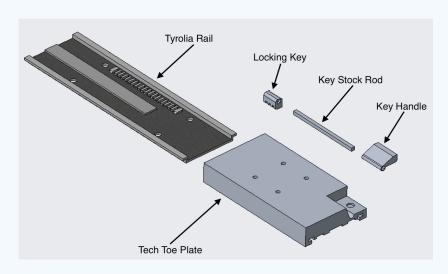
Tyrolia Attack2 13 Demo Binding and Voile Risers





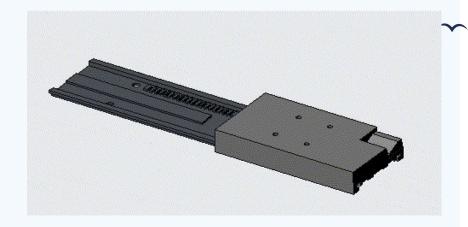
Voile Climbing Risers

Our Design





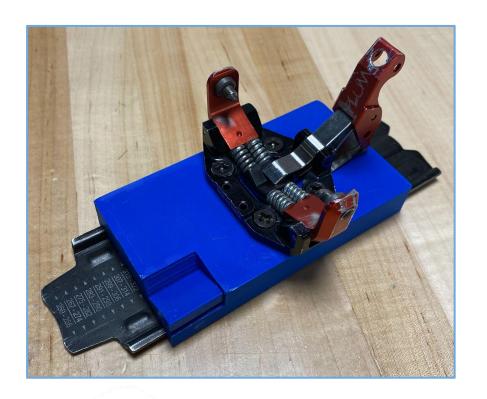
- Strength characteristics
- Weight
- Availability at WPI



Design Changes

- Magnets instead of springs
- Use of more metal components

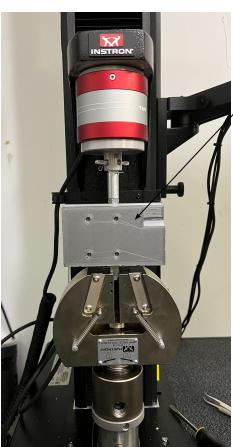
3D Printed Prototype



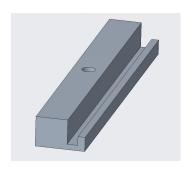


Instron Tensile Testing and Material Selection





3D Printed Plate



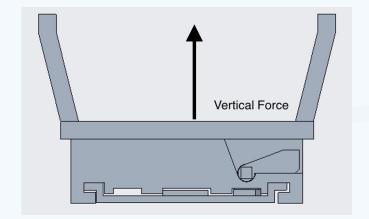
Testing Fixture

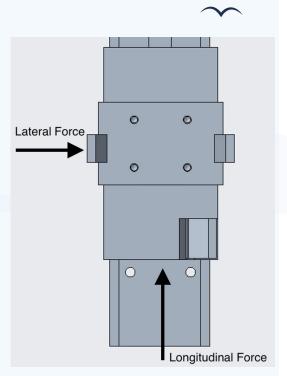




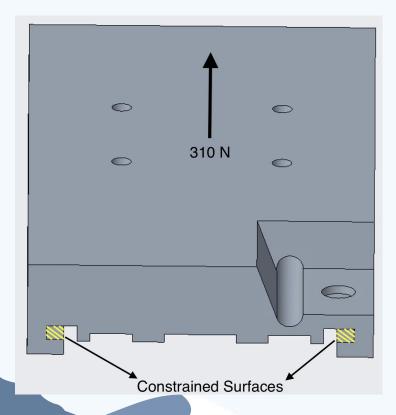
3 Analysis Cases

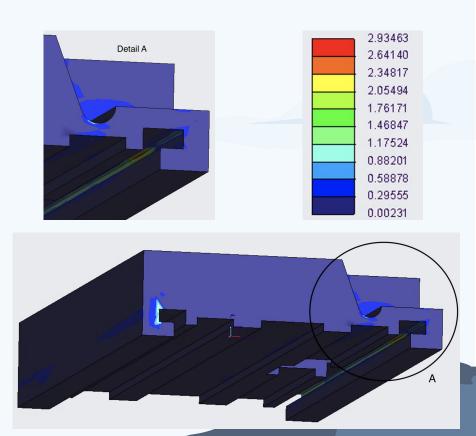
- 1. Vertical Load
- 2. Lateral Load
- 3. Longitudinal Load



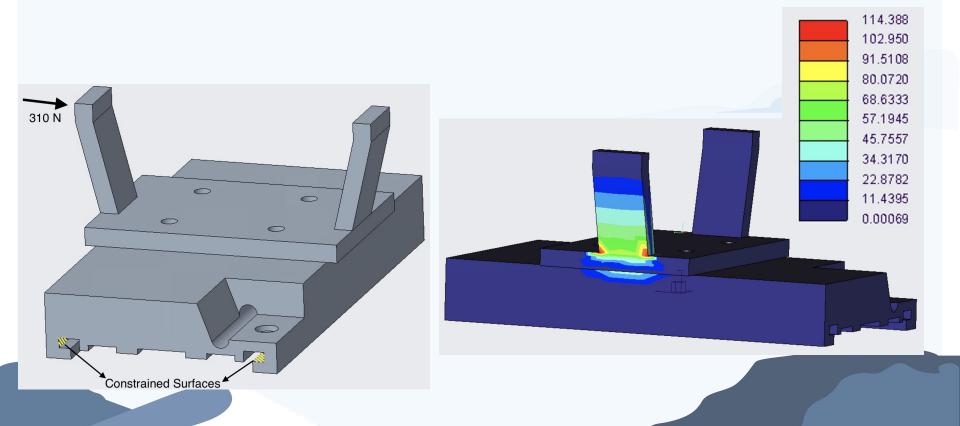


Case 1: Tech Toe Plate Under Vertical Load

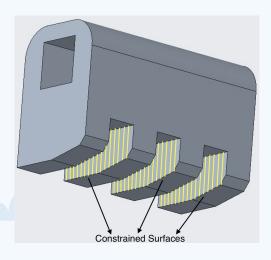


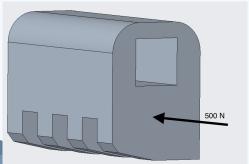


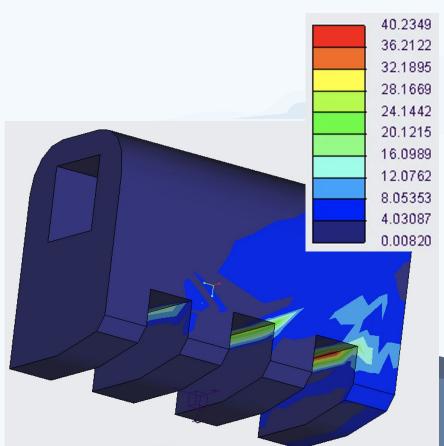
Case 2: Tech Toe Plate Under Lateral Load



Case 3: Locking Key Under Longitudinal Load

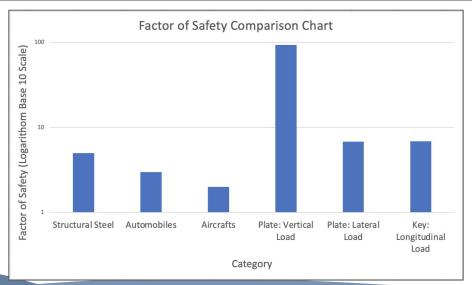






Simulations Summary

Analysis Case	Minimum Factor of Safety
Plate under Vertical Load	94.04
Plate under Lateral Load	6.85
Key under Longitudinal Load	6.86



Manufacturing Process

Haas Mini Mill

Haas Super Mini Mill

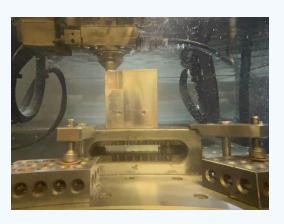
Accutex Wire EDM



 Used for plate, initial cuts on stock for the handle and key



 Used for teeth on key, magnet pocket on handle

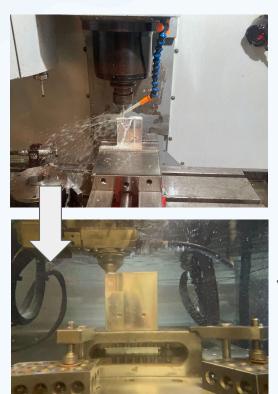


 Used for square hole on key and handle, outer profile of key and handle, rail cutouts on plate

Manufacturing Process: Tech Toe Plate



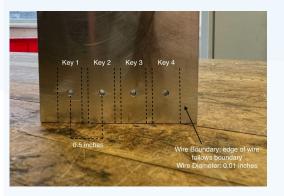






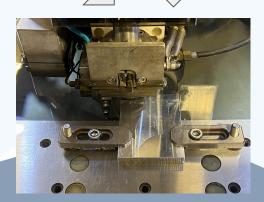


Manufacturing Process: Locking Key



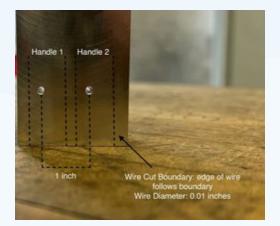








Manufacturing Process: Handle



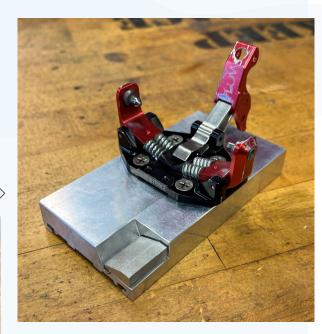


Final Prototype







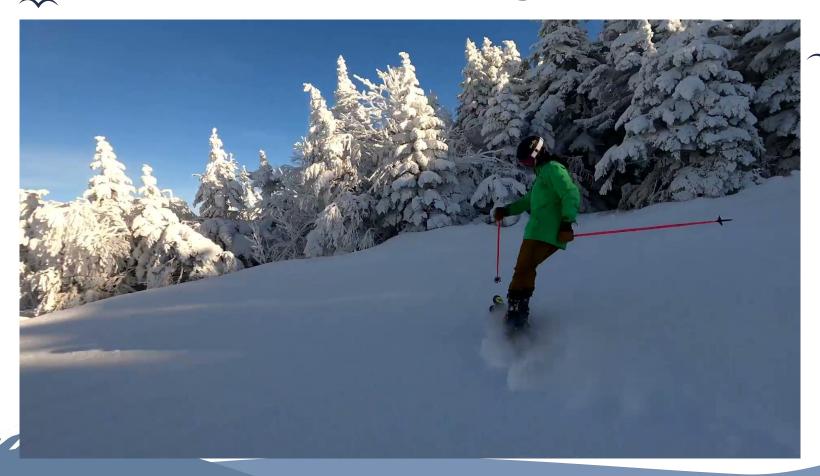


On Snow Testing





On Snow Testing



On Snow Testing: Results

Uphill Performance

- Light, natural, and comparable to touring specific bindings
- Climbing risers were a cause of concern

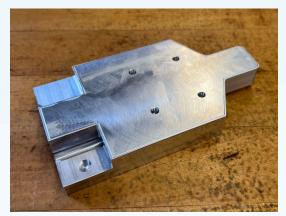
Durability



Downhill Performance

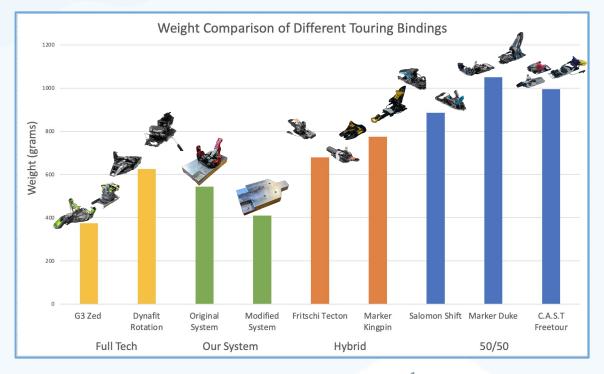








Modifications



Recommendations

- Consolidate components
- Integrate riser system into Kingpin/Tecton style heel piece
- Utilize rail attachment or Cast style toe piece interchanging system
- Injection molding

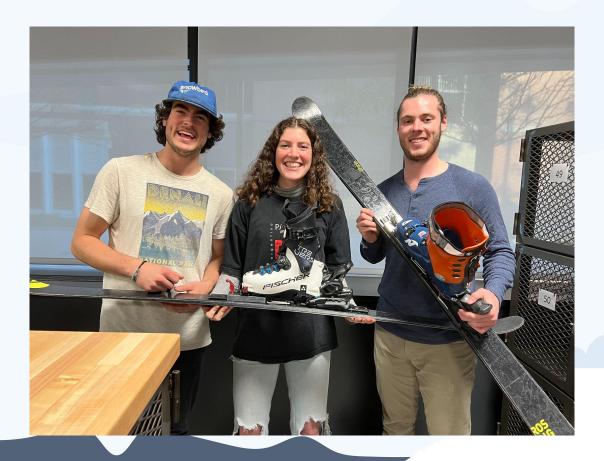


Fritschi Tecton Heel



Marker Kingpin Heel

Conclusion



Acknowledgements



Professor Ebadi
For guiding and advising our team throughout the semester



James Loiselle
For always being willing to lend us a hand in the machine shop



Ian Anderson

For aiding our team in the machine shop



Professor Oyewole (Kenny)
For aiding us in testing our
prototype



Barbara Fuhrman

For helping us make the necessary purchases for our project

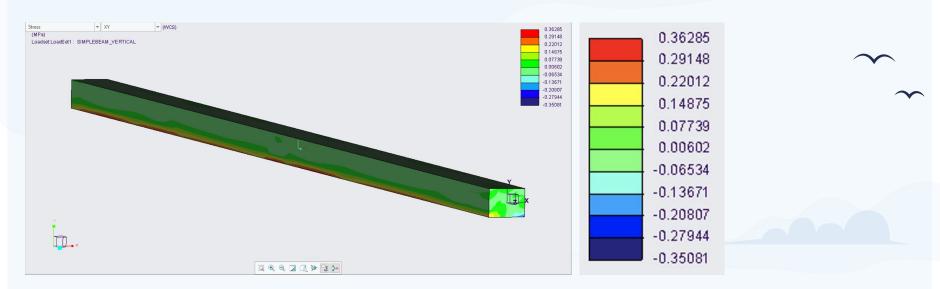


WPI
For providing the resources for us to complete this project

~ Questions?



Hand Calculations Case 1: Vertical

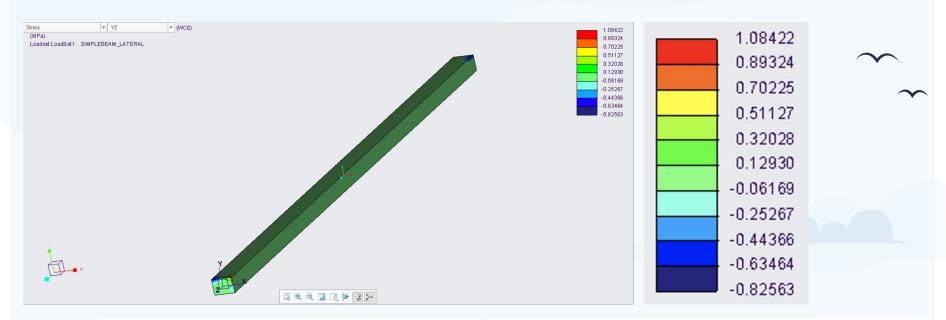


$$\sigma = \frac{P}{A_0}$$

$$\sigma = \frac{310 N}{2(.120 m \times .003575 m)}$$

$$\sigma = 361,305.4 Pa = 0.361 MPa$$

Hand Calculations Case 2: Lateral

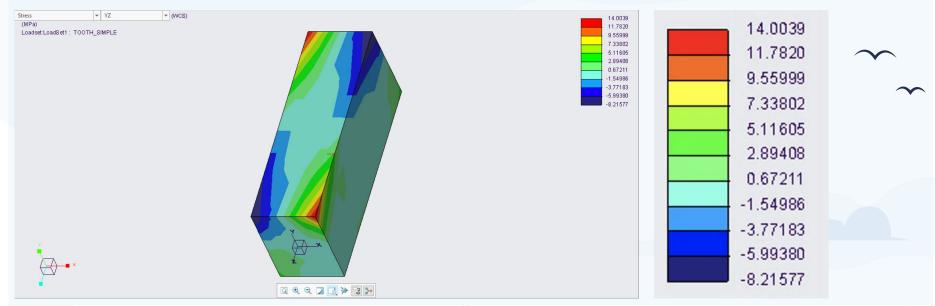


$$A = b \times l = 0.003575 m \times 0.120 m$$

 $A = 4.29 \times 10^{-4} m^2$

$$\begin{split} \tau_{YZ} &= \frac{3V}{2A} = \frac{3(310\,N)}{2(4.29\times10^{-4}\,m^2)} \\ \tau_{YZ} &= 1,083,916.084\,\frac{N}{m^2} \times \left(\frac{1\,MPa}{10^6\,\frac{N}{m^2}}\right) = 1.0839\,MPa \\ \tau_{YZ} &= 1.0839\,MPa \end{split}$$

Hand Calculations Case 3: Longitudinally



$$A = b \times l = 0.002 m \times 0.00675 m$$

 $A = .0000135 m^2$

$$\tau_{YZ} = \frac{3V}{2A} = \frac{3(125 N)}{2(.0000135 m^2)}$$

$$\tau_{YZ} = 138,888,888.89 \frac{N}{m^2} \times (\frac{1 MPa}{10^6 \frac{N}{m^2}}) = 13.89 MPa$$

$$\tau_{YZ} = 13.89 MPa$$