

WORCESTER POLYTECHNIC INSTITUTE



Roughness and Reflectivity of Mass Finished 6061 T6 Al Surfaces

Major Qualifying Project

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1. Abstract

The objective of this Major Qualifying Project is to study surfaces produced by mass finishing. To better understand the basic mechanisms we have determined the normal forces between a surface and a sample mass finishing media by measuring scratch depths from brief mass finishing times on polished surfaces, testing the micro-hardness of the surface, and measuring the shape of the abrasive particles in the media. We also studied how the surface produced by mass finishing effects the shininess of the surface. In particular scale-sensitive fractal analysis allowed us to identify the scales at which the surface roughness and surface reflectivity correlate the best. There appears to be limited literature on both the texture and reflectivity of mass finished surfaces. The results of this work should support product and process design for mass finishing.

Parts were machined using HAAS CNC machines. The finishing machine used is a BelAir centrifugal disk finishing machine. The surfaces were measured using an Olympus LEXT 4000 laser (409 nm) scanning confocal microscope. The surface reflectivity was measured using an Olympus USPM-RU III micro spectrophotometer.

Hardness and scratch depth tests show that for a pyramid type abrasive media the forces on machined and polished cylindrical aluminum alloy (6061 T6) parts ($r=0.375$ in., length=1.0 in.) are 16-19 mN. Regression analyses have shown a correlation coefficient R^2 of 0.95 between relative area and surface reflectivity in the scales of $2\text{-}5\ \mu\text{m}^2$, at a wavelength of 405 nm.

2. Introduction

This project came to fruition through the donation of a centrifugal disk finishing machine to WPI by Bel Air Finishing Supply. As previously mentioned, it was the goal of the MQP to study the surfaces produced by the mass finisher. We began with a literature review to identify exactly what was known about such devices already. We then proceeded to do experiments using both turned and polished aluminum with the goal of identifying the forces involved with this specific type of mass finishing operation. It was at this point that we were given a micro spectrophotometer from Olympus to utilize and learn about for a week. We took this opportunity to also include in the MQP research relating to surface roughness and reflectivity from mass finishing operations. The remainder of the project was focused on this goal and our methods and results are as follows.

2.1 Objective

The objective of this Major Qualifying Project is to study surfaces produced by mass finishing. To better understand the basic mechanisms we have determined the normal forces between a surface and a sample mass finishing media by measuring scratch depths, testing micro-hardness and measuring the shape of abrasive media. In addition we have studied how the surface produced by mass finishing effects the shininess of the surface.

2.2 Rationale

These two objectives are important for the major reason that there is very limited knowledge of the forces which are acting between the media and the part, as well as how the reflectivity of a non-smooth surface changes with roughness after a tumbling operation.

The principal work done on the generation of scratches on surfaces was Archard (Archard, 1953). However, most of this research was done in the 1950's and limited work has been done on the topic since. Furthermore, we were unable to find anything done on the topic of the generation of scratches during mass finishing operations.

Light scattering is also a well-documented phenomenon on surfaces. The basic principal of Snell's law is one that is well understood by the scientific community. However, the scattering of light on rough surfaces is one a subject with very limited research. The behavior of the different wavelengths of light and the roughness of a surface is not something which is well known. Jean Bennett is one of the few who has contributed to the knowledge of the topic; however there are still many questions which remain (Bennett, 1961).

2.3 State-of-the-Art

There appears to be limited literature on both the texture and reflectivity of mass finished surfaces. What sets our work apart from most other reflectivity research is that we are testing with rough surfaces, not flat or polished surfaces. In our literature review we failed to find any research correlating the roughness of a surface produced by mass finishing to the reflectivity of the surface taken from a micro spectrophotometer, which makes our results exciting. The results of this work should support product and process design for mass finishing.

2.3.1 Existing Research in Mass Finishing

To begin the team first looked at some of the fundamental work done in the area of abrasive wear on solids since the movement of media within the centrifugal disc finishing machine can be seem to act in this way. Early studies by Archard introduced that the wear rate is proportional to the load and independent of the area of contact. He also finds that given a constant flow and pressure, the wear rate is independent of speed of sliding (Archard, 1953).

Samuels and Mulhearn conducted a study using silicon carbide abrasive papers to model the abrasion of metals. They found that wear on a surface was related directly to the load, contact length and density of the work piece (Mulhearn and Samuels, 1962). Other important work, which may relate more closely to the process involved in centrifugal disk finishing, models the effects of low stress abrasive wear. During this study, Grigoroudis and Stephenson found again that the wear rate increased with load and that the quantity of material loss was proportional to amount of abrasive material used (Grigoroudis and Stephenson, 1997).

Specific to mass finishing, some research has been conducted using vibratory bowls. Using a vibratory bowl, contact forces were measured on aluminum work pieces. This work led to the discovery that surface hardness of a work piece was directly proportional to the lubrication of the compound run through the media (Wang et al., 2000). Using the same machine, Domblesky developed a set of relationships between the material removal rate of aluminum, brass and steel pieces and the vibratory bowl parameters (Domblesky et al., 2004). Up until this point in time, this research most closely resembles the team's current objectives.

Specific to centrifugal disc finishing, there has been very little research aimed at developing accurate models. Cariapa et al. performed research in 2007 in an effort to explain both the material removal characteristics and media flow in a centrifugal disc finishing machine. They successfully modeled the flow of the media in the machine, as well as, developed a method for calculating the material removal rate as a function of density and hardness. In addition they also identified several characteristics of the media weight loss during a finishing period. It is important to note, however, that the report identified the need for additional research into changes in surface finish of work pieces (Cariapa et al., 2007).

2.3.2 Existing Research in Roughness vs. Reflectivity of Mass Finished Surfaces

Once again, we were unable to find any research pertaining to the correlation between surface roughness and reflectivity of mass finished surfaces. Most of the literature that we discovered focused on specular reflection of smooth surfaces, and the remainder discussed using the bidirectional reflectance distribution function (BRDF). Li and Torrance conducted research attempting to correlate surface roughness and light scattering for rough metallic surfaces produced by bead-blasting, grinding and etching. Their results related surface roughness to incidence of light scattered from the rough surfaces (Li and Torrance, 2005).

Bennett and Porteus found a relationship between surface roughness and specular reflectance at normal incidences using steel plate disks coated in an aluminum film. Finishes were created using fine feed grinders. Roughness's of 2.5, 8, and 32 μin were measured using a profilometer (Bennett and Porteus, 1967).

Attempts to create a geometric model of reflectance for use in design of surfaces have been worked on to predict surface scattering based on scale-sensitive methods. We expect that the reflectance should decrease with decreasing scale (Shipulski and Brown, 1994). These experiments were done using steel however, and do not directly address the objective we are working towards.

3. Approach

3.1 Research Gap

It is clear from the existing research found in the area of centrifugal disc finishing and reflectivity that there is a wide gap in research which has yet to be explored. Although Cariapa successfully identified relationships for material removal rate and media flow, it was noted that further research regarding the relationships between finishing parameters and the resulting

surface finish was needed. The team did not identify any other material related specifically to identifying relationships in centrifugal disc finishing machines.

In order to lessen this gap, we designed several experiments to test for significant relationships between input parameters and the resulting surface finish. First, using design of experiments, we factored out any insignificant variables leaving a list of variables which were tested. The total number of initial variables is as follows: initial surface finish & duration inside the finisher.

4. Methods

4.1 Variable Significance Isolation

It is going to be very important that during the course of this project that we are able to quickly determine which variables are significant. In this case we will be looking at variables that affect surface finish when looking at mass finishing, and variables that affect determining the accuracy of obtaining an area scale value. Furthermore we will need to a basic discrimination test to affirm conclusions that were made during testing.

Discrimination testing is a useful tool because it allows for the identification of irrelevant data (Discrimination testing: a few ideas, old and new). There are many different ways to perform these tests. However, the underlying question in all of these tests is “how different is different”.

4.1.1 Application to Mass Finishing

In order to determine which variables greatly influence the final outcome of a surface during mass finishing we will need to test many variables, which of these are important, and

which do not require strict control. After we determine this we will be able to, in and quick and efficient matter developed a basic strategy to figure out which variables matter and which do not. To really answer the question “how different is different?”

4.2 Design of Experiment

4.2.1 Estimation of Contact force of Media & Part

To identify the forces involved in mass finishing we used first had to generate a surface which was polished. To do this, we used the Metallographic Polishing Laboratory located in Washburn Shops. The Surfaces we used were the ends of a 0.750 inch bar stock of T-6061 Aluminum. (Shown in Figure 1 after 30s. in Mass Finisher)

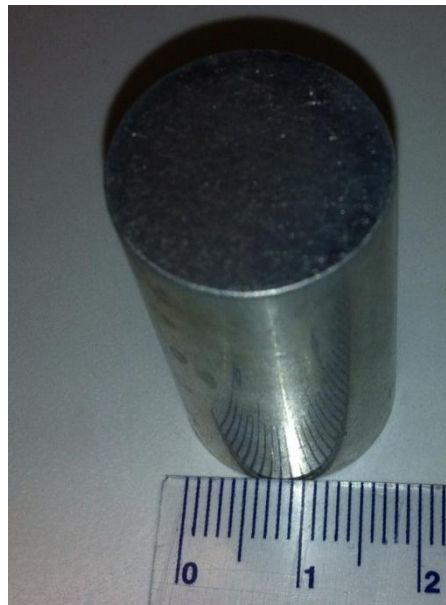


Figure 1 (Note: Scale is in cm)

To begin our experiment we identified which variables were to be tested. To quickly identify which variables are significant in the overall surface finish of a final part we took 4 data points and tested each several times. These 4 data points are as follows: there will be two groups of 2 and the groups will have quantifiable values within 10% of their values, and the groups will

be different by at least 100%. This will allow us to quickly determine if there is a correlation between these variables and surface finish quickly. If no correlation is found then this variable will be disregarded for future experimentation. For our purposes we will be testing the following variables:

Initial surface finish

4.2.2 Roughness and Reflectivity Correlations

To identify correlations in reflectivity we used initial surface finish and time in the mass finisher as our variables. There were three distinct branches in this experiment: processing, measurement and performance. A diagram outlining the overall process of the experiment can be seen in figure 5 below.

4.2.2.1 Processing

All the parts used for the experiment were 6061 T6 Aluminum. In order to prepare the surface finish for measurement, several steps were taken. First a rod of extruded aluminum was turned in a HAAS lathe at a feed of 0.5 mm/rev at a speed of 2000 rpm. A portion of the rod (1 inch) was cut off and used for the experiment. In order to be sure that the same area of the work piece was being measured after each interval of time, a small area was marked with an etching tool at one end of the part.

The next process required to achieve the desired finish was the mass finishing operation. As mentioned previously, time in the mass finisher was one of the variables and therefore this operation was repeated. The part was finished for a total of 7 times: 0, 0.5, 1, 4, 10, 30, and 60 minutes. The part was finished using a spin speed of 50%. A pyramid shaped abrasive media was chosen for the experiment so that the surfaces would become increasingly rough with increasing

time. After each interval of finishing, the part was removed, rinsed with water and then measured.

The tumbling in the mass finisher gave us our first scale of interaction for the experiment which was time. Later this would be compared with the other scales to identify where the best correlations were.

4.2.2.2 Measurement

After each mass finishing operation, the part then had to be measured using the Olympus LEXT confocal laser scanning microscope. The actual data used for the experiment came from measurements taken with the 100x objective on the microscope; however, measurements using the 20x and 50x objective were also taken for comparison purposes. Roughly four measurements were taken with the 100x objective for each interval, to ensure the target area was being measured. Measurements taken on the LEXT were analyzed using both the LEXT software, as well as, SFrax in order to get relative area calculations.

For analysis on the LEXT, all measurements were first filtered using the standard filtering in the software. All measurements were put through an inclination filter, curved surface correction filter and a flat surface spike removal filter before taking any data. For Sa calculations a cutoff value, λ_c , of 800 μm was selected. Roughly ten line profiles in the x direction were taken for each measurement and then averaged to acquire the average Ra's for each time interval. Sa data was also taken from each of the measurements and averaged to obtain the average Sa for each time interval of mass finishing operations.

In order to obtain a more accurate and relative set of data on the surface characterization, we utilized the area-scale analysis software SFrax. Using this software we were able to import the measurements from the LEXT and run several analyses such as relative area and complexity

calculations. Although we did correlate the average Ra's with reflectivity, we wanted to also correlate the relative areas because this had never been done before. During the area scale analysis, instead of averaging the data from each measurement, the measurements themselves were averaged within the software and then the data was taken from that. This allowed us to quickly gather area scale and complexity data that could be correlated to the reflectivity data.

The area scale analysis resulted in another scale of interaction. The different scales which were analyzed during the area scale analysis output different relative areas. In order to eventually find the best correlations we would have to determine which scales to look in.

4.2.2.3 Performance

The final area of the experiment was the performance of the work piece, or in our case, the reflectivity. Although it was separate, the reflectivity measurements ran concurrent to the surface roughness measurements. Therefore, after each mass finishing operation, the work piece was measured for both roughness and reflectivity before it was finished for the next interval of time.

The device used for the reflectivity measurements was an Olympus USPM RU-III micro spectrophotometer. The data output from the device is a percentage of light returned for each wavelength of the visible spectrum (380-780 nm).

Roughly 30 different points were measured for each interval, within the area designated earlier before mass finishing. Outliers were removed and the remaining data points were then averaged for each wavelength, resulting in the average reflectivity for each time interval over the range of wavelengths. This resulted in the last scale of interaction: wavelength. We now also had to determine which of the 400 wavelengths would show the best correlation with surface roughness.

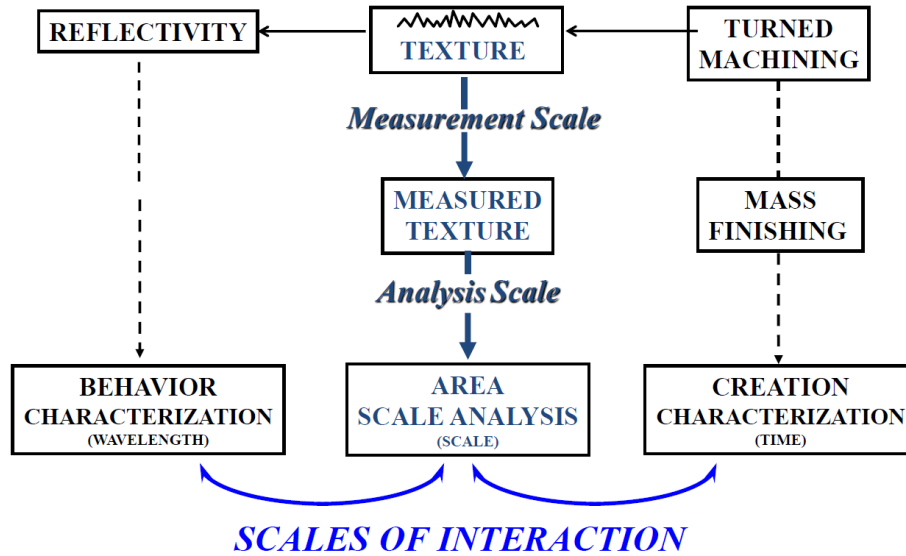


Figure 2: Roughness-Reflectivity Methods

4.3 Analysis

4.3.1 Roughness and Reflectivity Correlation

Three main tools were used in the analysis of the data measured during the roughness and reflectivity experiment: LEXT OLS 4000 software, SFrax, Excel, and MATLAB. As mentioned earlier, the standard Ra and Sa values were measured using the Olympus software, but were used only to show a simple outline of how roughness changes with time in the mass finisher. The majority of the analysis came from SFrax and Excel.

After both the reflectivity and relative area (and complexity) data was organized, we began to make correlations in SFrax between relative area and reflectivity. At first this required manually selecting different wavelengths to test and then inputting that data into the variable correlation analysis tool in SFrax. Based off of this method we were able to identify the best correlation was at 405 nm at a scale of $2 \mu\text{m}^2$. This method of manually analyzing each scale and wavelength would take far too much time, however, so we needed a faster way to test each possibly pairing and return its R^2 .

We did this by entering all of the data calculated in SFrax into Excel and using the RSQ function to correlate every single roughness for each scale with all reflectivity's at each wavelength. We then entered all of that data into MATLAB, which was able to produce a 3D plot of all correlations versus scale and wavelength. At this point, we had an overall picture of how well roughness and reflectivity were correlated.

5. Results

5.1 Estimation of Media Forces

Initial calculations for the media cutting forces were completed using a Vickers hardness test. A sample piece of Aluminum (6061 T6) was tested in the mass finisher for a time of 30 s. The Vickers hardness was then taken on the work hardened surface yielding a HV=124 (using a force of 10 g over 5 s.).

$$HV = \frac{F}{A} \approx \frac{0.1891F}{d^2}$$

Equation 1

Assuming that the abrasive in the media has diamond geometry, we used the following equation to calculate the normal forces, where F is in Newton's and d is in mm.

Data taken from scratch depth/width measurements were used for "d" (equation above). These measurements were obtained using line profile measurement tools within the LEXT software.

- A total of 11 scratches were measured
- An average of 7 width, depth and area measurements were taken for each scratch

- The scratches examined were the deepest scratches in isolated areas

Parameter	Mean Value	Standard Deviation
Scratch Depth	0.399 μm	0.180 μm
Scratch Width	5.396 μm	1.337 μm
Scratch Cross-Sectional Area	2.204 μm^2	0.790 μm^2
Vickers Hardness	124.0 HV _{10g}	6.555 HV _{10g}
Normal Force	19.09 mN	-

Table 1: Summary of Scratch Depths and Forces

5.2 Reflectivity Correlation

As mentioned in the Methods Section we mass finished the Pieces for a grand total of 7 different times, including the initial turned surface. The following Images are the images taken from the Olympus LEXT Confocal Microscope at a 20x objective.

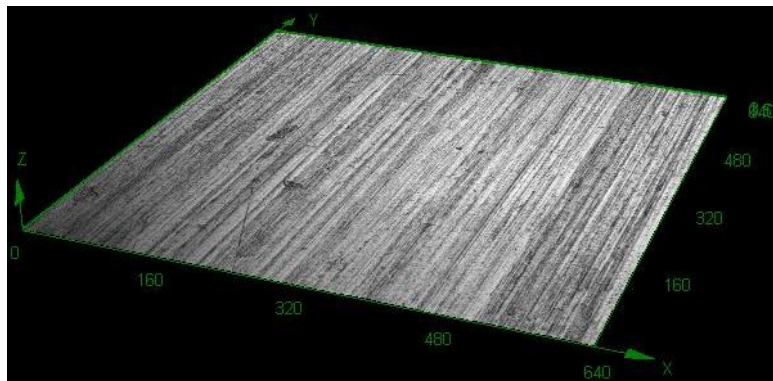


Figure 3 (Initial Machined Piece at .05mm/rev @ 2000 rpm)

It is clear from this image that the machining marks are still visible. However, due to the very small feed rate of the tooling the surface is still very smooth.

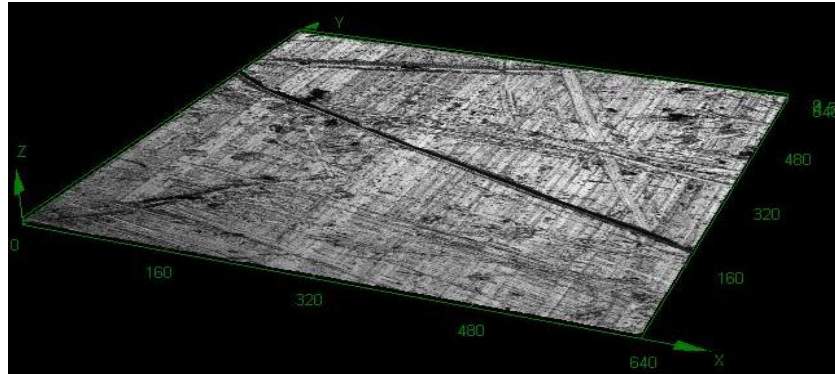


Figure 4 (Piece after 0.5min of Mass Finishing)

After only 30s (or .5 min) in the mass finisher deep scratches have begun to form on the surface as a result of the action of the media on the part.

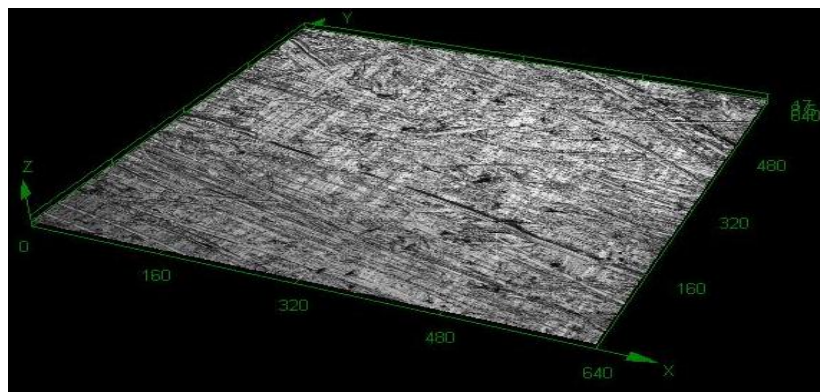


Figure 5 (Piece after 1 min of Mass Finishing)

After an additional 30s in the mass finisher many more scratches have formed and the machining marks have begun to disappear.

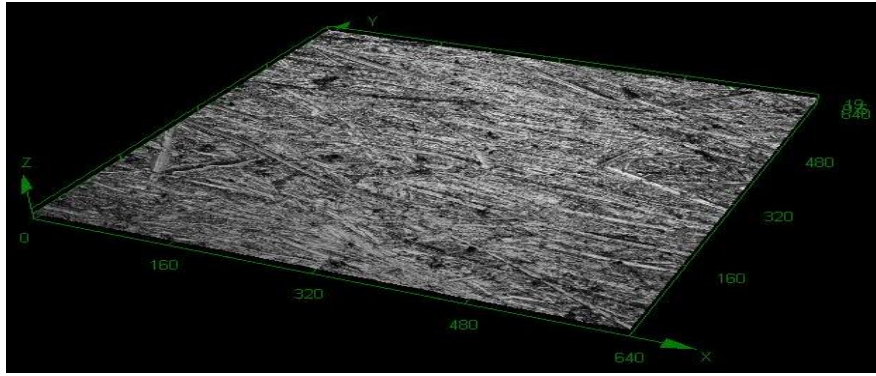


Figure 6 (Piece after 4 min of Mass Finishing)

After 4 minutes in the mass finisher the machining marks have been completely obscured by the action of the media.

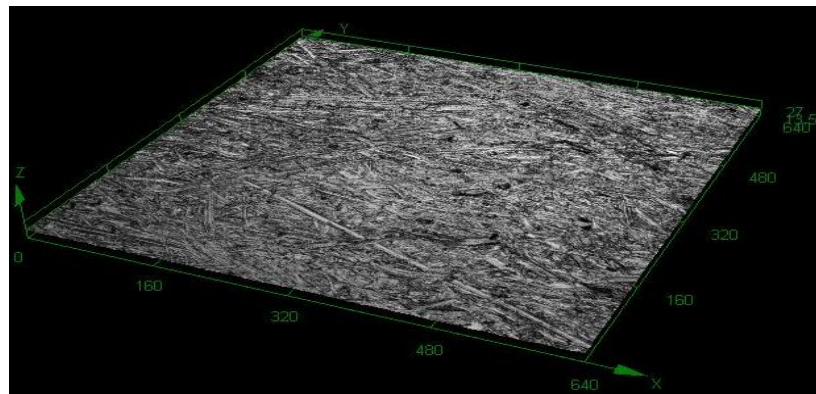


Figure 7 (Piece after 10 min of Mass Finishing)

After 10 minutes of mass finishing little can be distinguished from a visual inspection of the images which were generated from the Confocal Microscope. There is little that visually distinguishes the surfaces from here to the hour mark. However, the behavior of these surfaces is quite different.

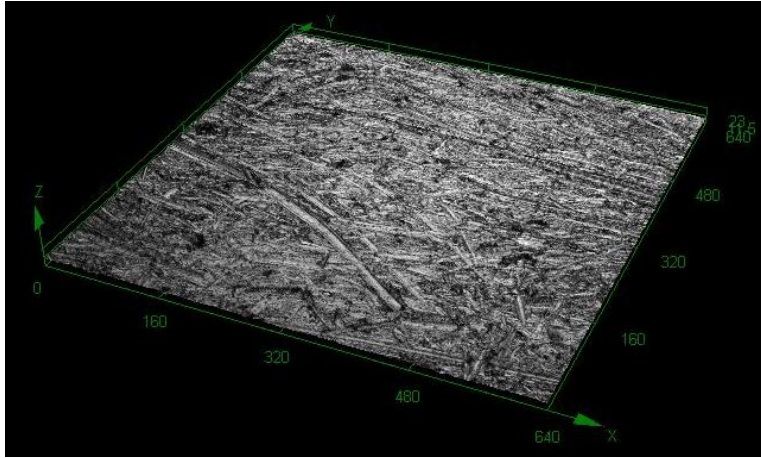


Figure 8 (Piece after 30 min of Mass Finishing)

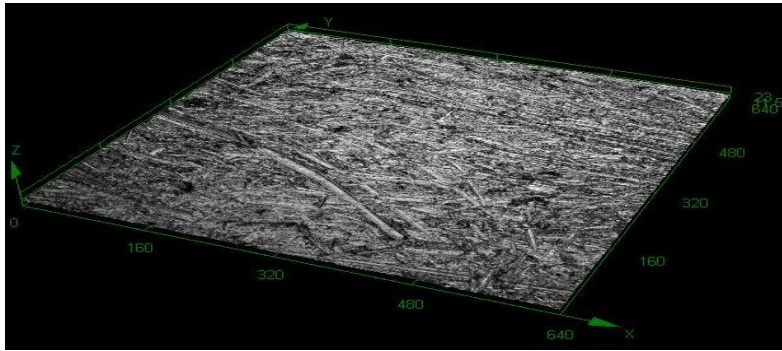


Figure 9 (Piece after 60 min of Mass Finishing)

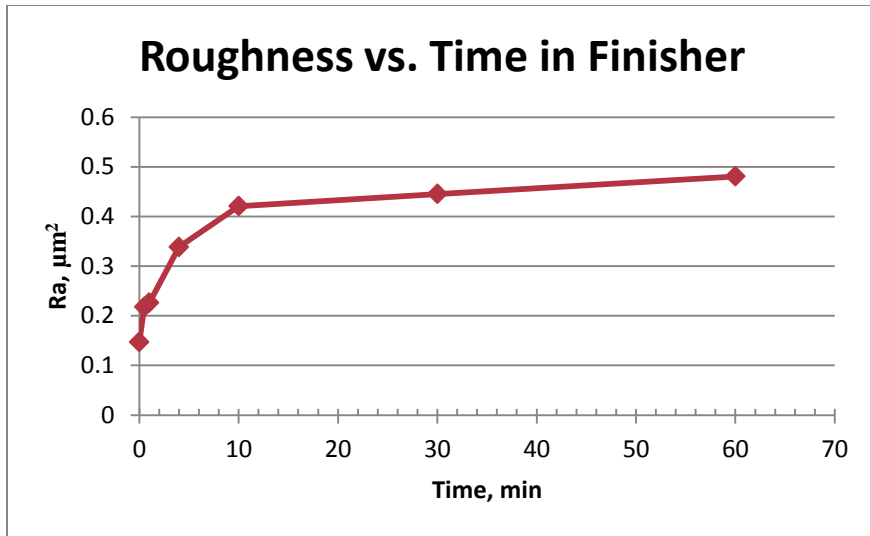


Figure 10 Ra vs. Time

As can be seen in Figure 10 Ra vs. Time, the Ra values for 10, 30, and 60 minutes of mass finishing is very similar. This is consistent with the previous statement of these images all looking very similar. However, Ra is not a perfect metric for measuring surface finish and other methods such as looking at Relative Area at different scales can tell you more about a surface.

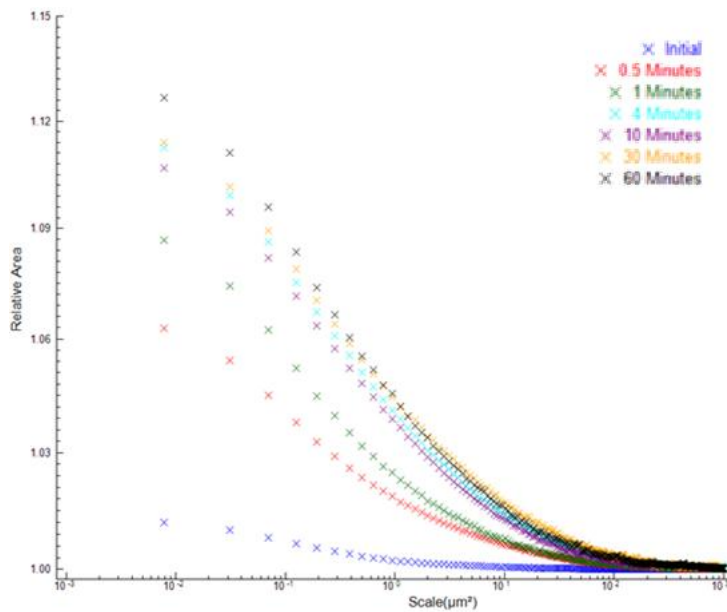


Figure 11 Relative Area vs. Scale

From Figure 11 Relative Area vs. Scale the differences of these surfaces can be seen more distinct than can be seen from the plot of Ra vs. Time. This was generated from doing a Fractal analysis on images taken at the 100x objective of the Confocal Microscope.

There was one anomaly which we found interesting. If you are to look at the Relative area of the 4 minute and 10 minute times of finishing, the 4 minute data has a higher relative area. This was found several times during our experiment. The reasoning for this is one that we can purely make conjecture as to the mechanism behind it.

When looking at the Ra. vs Time graph this is not what is seen, there is a consistent rise in the overall Ra. Therefore, this leads us to believe that the overall peak to peak roughness is less, yet when examined on a more fundamental level, these peaks are rougher after only 4 min of finishing. This could be caused by the finishing after 10 min making larger peak to peak heights, yet the additional action of the media making the peaks smoother.

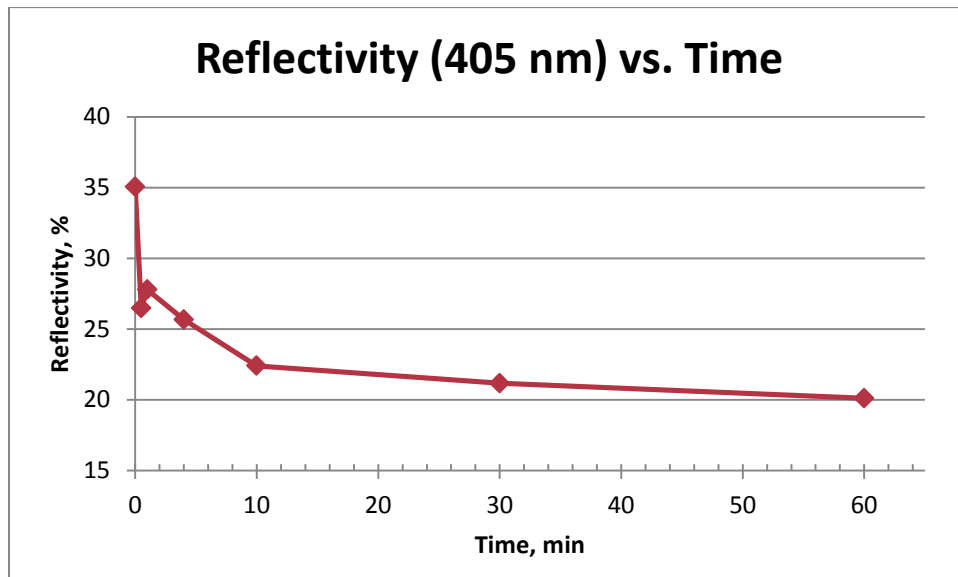


Figure 12 Reflectivity vs. Time

Correlation coefficients as high as 0.87 have been observed between the reflectivity and relative area measured during the experiments. As discussed in the methodology, there were three different scales of interaction that had to be taken into consideration when looking at this problem. We were able to plot all of these variables to determine exactly where the best correlation between the surface and the reflectance was. Analysis shows that the best correlation ($R^2=0.87$) is at a scale of $2 \mu\text{m}^2$ and a wavelength of 405 nm. A plot showing the resulting correlation for these parameters can be seen in figure 1 below.

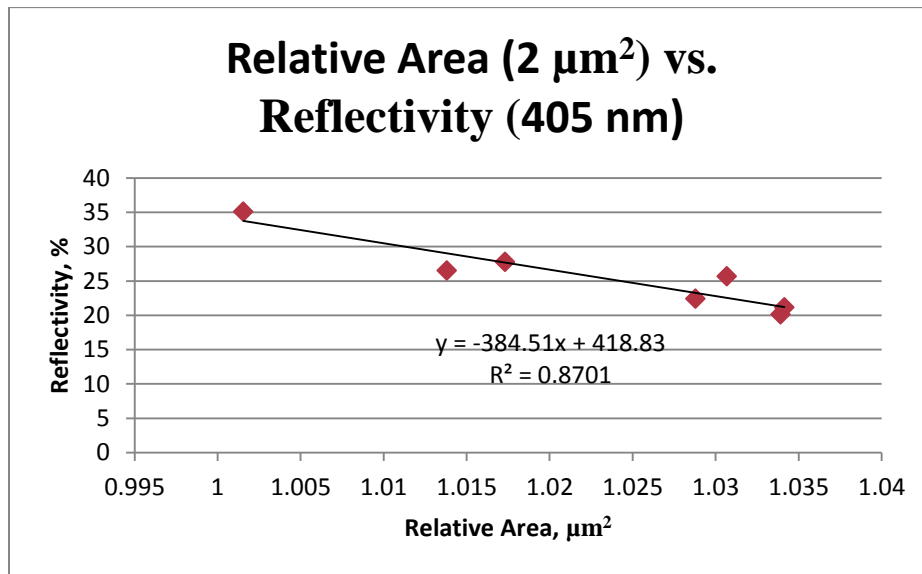


Figure 13 Relative Area vs. Reflectivity

In the process of determining the best correlation for the data, we were able to plot both the scale and wavelength against the correlation which gave a 3D space outlining all possible correlations. In general, the data fit best at wavelengths between 380-410 nm, after which the correlation drops off significantly. The team has been unable to determine just why that is what is happening. From the same data we found that the finer scales ($10^{-3} - 10^1$) fit the trend much better than the higher scales ($10^2 - 10^4$). The reason for this simply being that there is much more

noise/variance in the relative area calculations at these higher scales so the data is jumbled and not accurate.

This can be seen in Figure 14 R² vs. Scale at λ of 380 nm, as well as the 2 figures which follow it. This graph is the graph of the R² values which can be seen above in Figure 13 Relative Area vs. Reflectivity. These graph just shows how well correlations exist at certain scales at each wavelength.

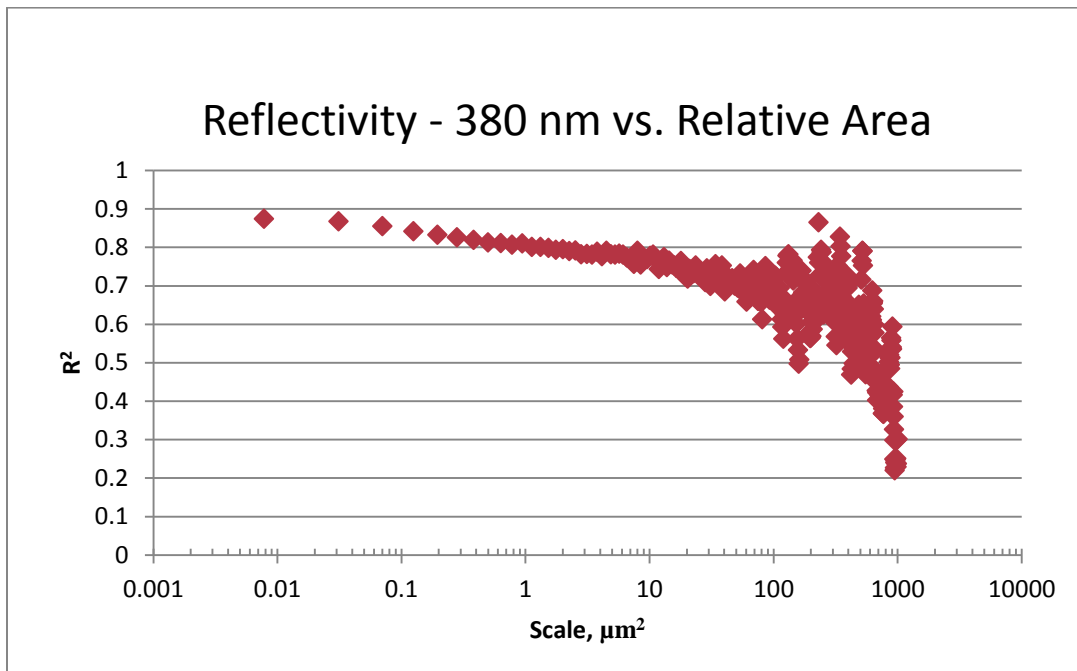


Figure 14 R² vs. Scale at λ of 380 nm

At the wavelengths around 380 nm there appears to be an upward sloping trend in the correlation of reflectivity and area scale as your scale becomes smaller.

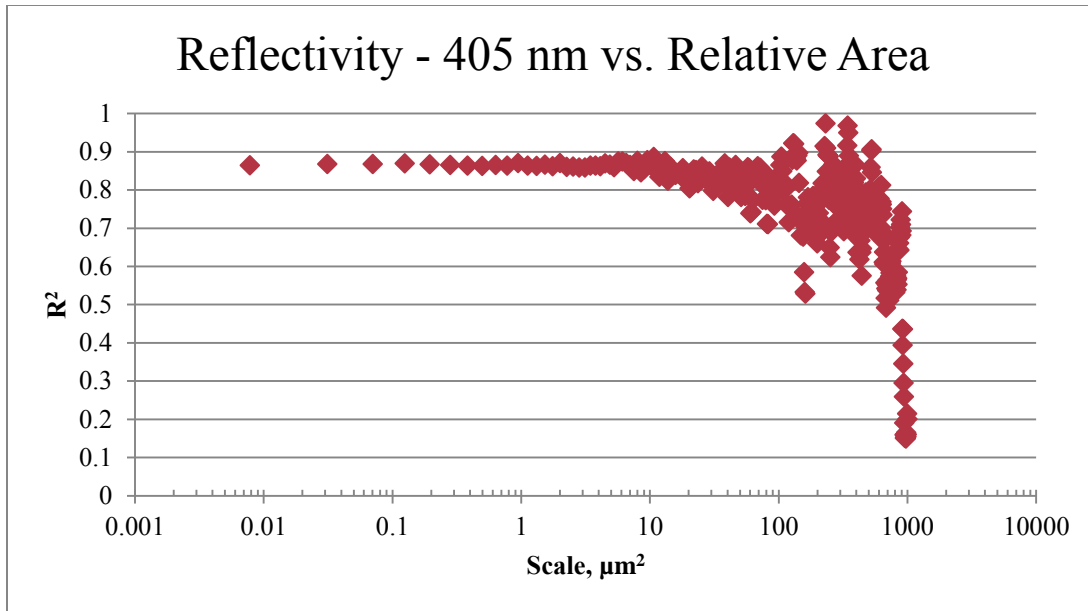


Figure 15 R² vs. Scale at λ of 405 nm

At 405 nm there exists the best correlation at around 2 μm of relating the percentage of light returned and area scale. It is interesting that this wavelength is also the same wavelength of light which the laser of the confocal microscope uses during data acquisition. We are not sure if this fact has true significance in these results; however, reproducing these findings using a different microscope, which uses a different wavelength, might be a useful experiment to determine the validity of this finding.

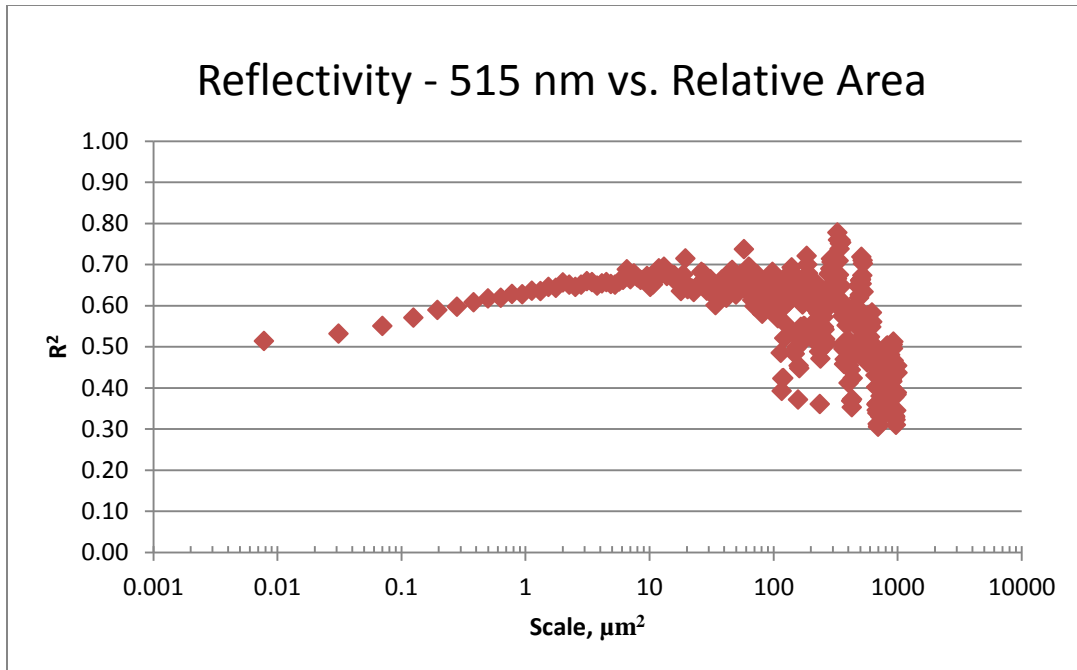


Figure 16 R² vs. Scale at λ of 515 nm

When getting out of the low 400 nm wavelengths the correlations of the data goes down drastically. This can be see when taking 515 nm as an example. The peak correlation, of any real significance, is around 0.68 which is far lower than that of 405 @ 0.87.

The preceding graphs are just the 2 axis representation of each wavelength. This then lead us to wondering what the 3 dimension space would look like when all the wavelengths are plotted together. The result of this can be seen in Figure 17 Wavelength vs. Scale vs. R2.

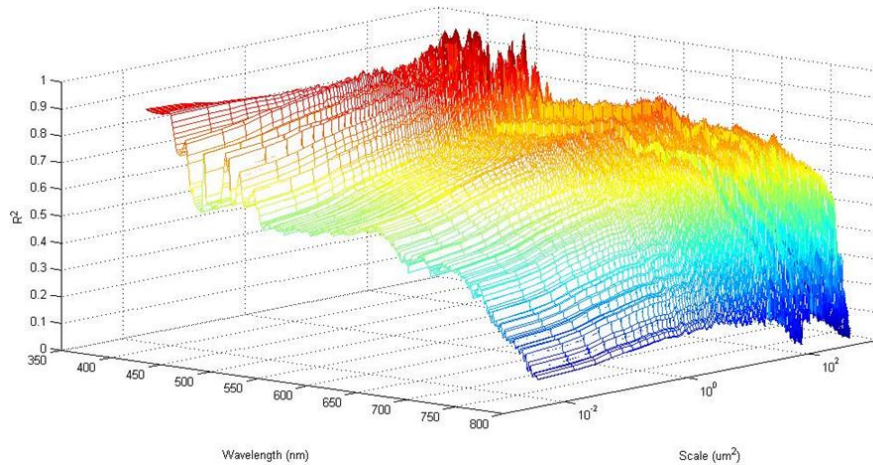


Figure 17 Wavelength vs. Scale vs. R^2

It is very apparent from this graph of the 3D space that the correlations of Area Scale and the larger wavelengths is virtually non-existent, while at the shorter wavelengths very good correlations exist.

Another aspect of this graph which is intriguing is the local maximums and minimums that exist between ~400-550 nm. This upward and downward movement of the correlation is an aspect of the behavior which we do not understand.

6. Discussion

1. After plotting all of our data together, we were able to pinpoint where exactly the best correlation was between shininess and relative area. An $R^2=0.87$ was observed at a scale of $2 \mu\text{m}^2$ and wavelength of 405 nm. From this the following equation was obtained:

$$\text{Reflectivity} = -384.51 * \text{Relative Area} + 418.83$$

Although this was the best correlation, the wavelengths and scales immediately surrounding $2 \mu\text{m}^2$ and 405 nm also show similar correlations. These can be found in Appendix A.

2. During the experiment a Ra measurement was taken after each interval of time in the mass finisher. From this data we were able to develop a correlation between time in the finisher and Ra. We found that the Ra leveled off after 10 minutes in the finisher. This data should help with processing improvements.
3. The plot of R^2 vs. Scale vs. Wavelength is shown in Figure 17 Wavelength vs. Scale vs. R^2 . Clearly the best correlations are at both lower scales and wavelengths. Although there appear to be correlations at the larger scales, this is not the case. The accuracy of relative area calculations drops off significantly at higher scales, therefore that data can be ignored. Knowing exactly what wavelengths and scales to consider when taking measurements will be a benefit for any application using these methods.
4. During the course of the experiment it was discovered that the wavelength of light used by the reflectivity machine to obtain the best correlation (405 nm) was the same wavelength used by the laser on the confocal microscope used to take the measurements. We have no explanation for this occurrence, nor is there any indication whether it has had an effect on the results of the experiment. It has simply been recognized as an interesting phenomenon and needs further attention.
5. Based on data measured from the confocal microscope we obtained an average scratch size put on the part from the mass finishing operation. We combined this data with other measurements taken of the media geometry, as well as, Vickers hardness tests. Using the

Archard equation we calculated the average normal force of a piece of media on the work piece.

6. We have recognized the need for further research to be performed on this subject. First, attention is needed to determine if the wavelength of the laser microscope has any effect on the results of the experiment. Next, the project team will conduct further research in the near future to repeat the experiment. In doing so we will be able to correct any mistakes made in the original experiment and test for repeatability. In addition, testing with different materials is of further interest.

7. Conclusions

1. Correlations between relative area and reflectivity (percentage of light returned) were discovered. The best correlation was found at a scale of $2 \mu\text{m}^2$ and wavelength of 405 nm. The best correlation obtained was with an $R^2 = 0.87$.
2. A correlation between roughness measured with the confocal microscope and time in the mass finisher was discovered. The relationship appears to follow a logarithmic curve.
3. There is a clear pattern in the correlation coefficient, R^2 , between relative area and reflectivity based on the scale and the wavelength. Relative area and reflectivity are best correlated with both decreasing wavelength and scale.
4. The wavelength used by the confocal microscope's laser (405 nm) is the same wavelength at which we found the best correlation between reflectivity and relative area.
5. Based on scratch depth measurements, media geometry and hardness tests a value for the average normal force of media on a part was calculated. The average normal force is 19.09 mN.

8. References

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Appendix A

Results at Roughest Finish

Correlation Results - Reflectivity(380 nm) vs.Relative Area

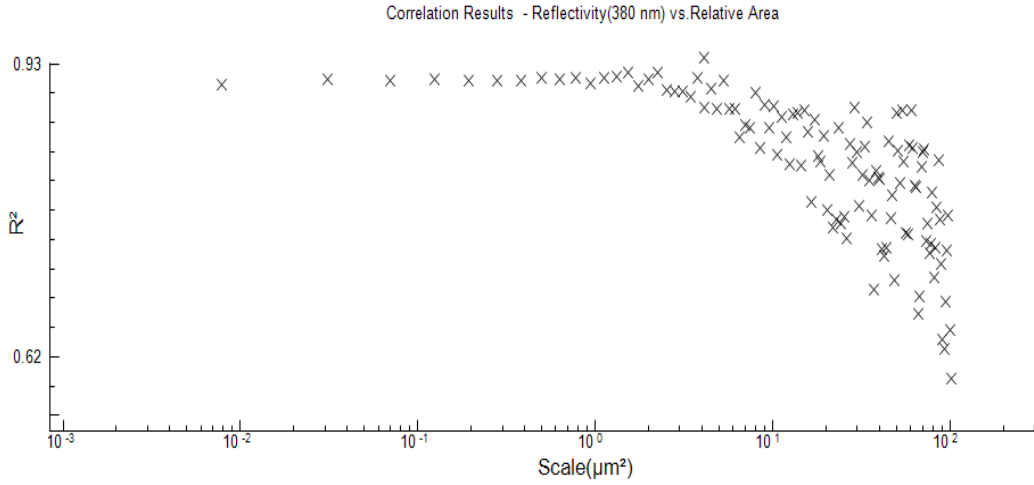


Figure 18: 380 nm for roughest surface

Correlation Results - Reflectivity - 390 nm vs.Relative Area

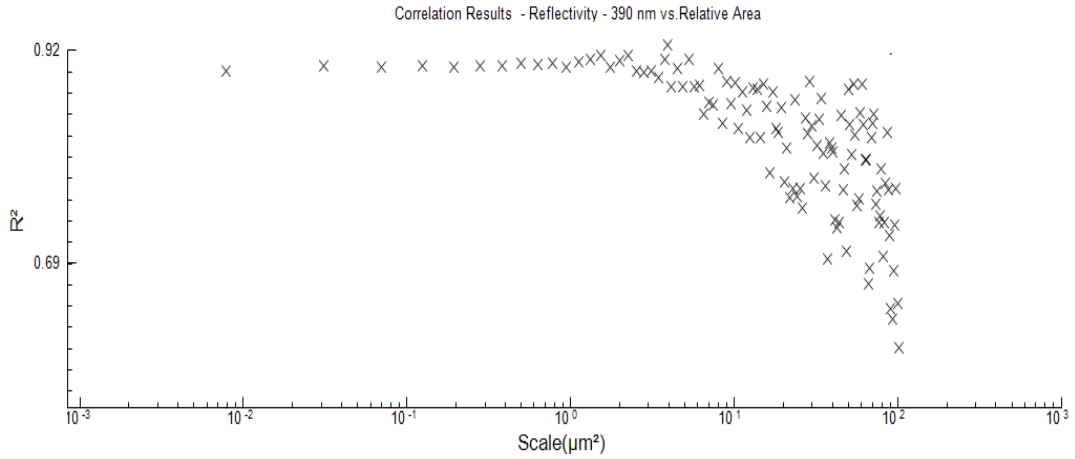


Figure 19 390 nm for roughest surface

Correlation Results - Reflectivity - 630 nm vs. Relative Area

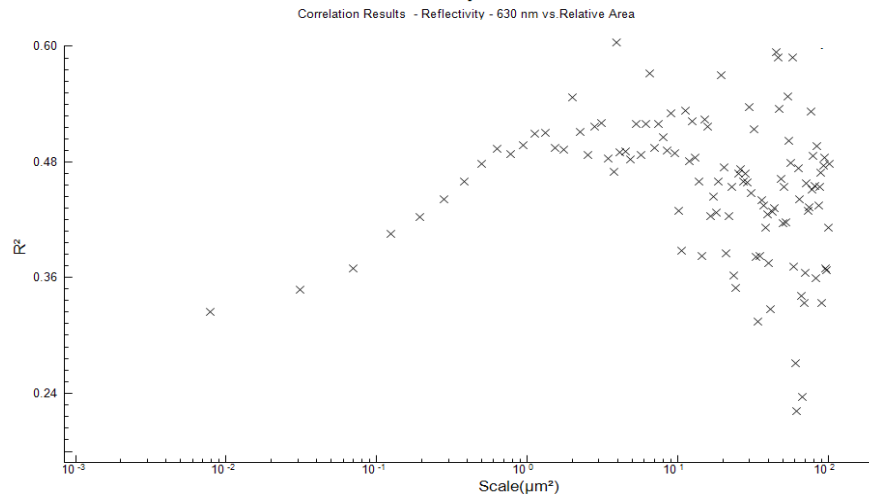


Figure 20 630 nm for roughest surface

Complexity Results

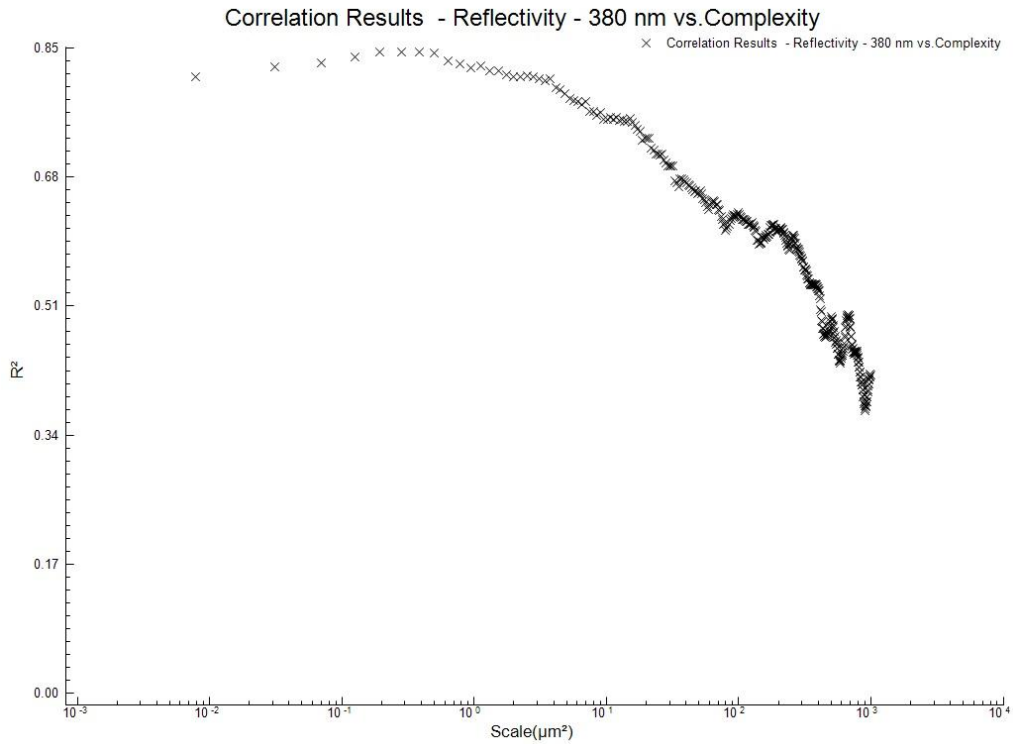


Figure 21 Complexity Correlation vs. Scale @ 380 nm

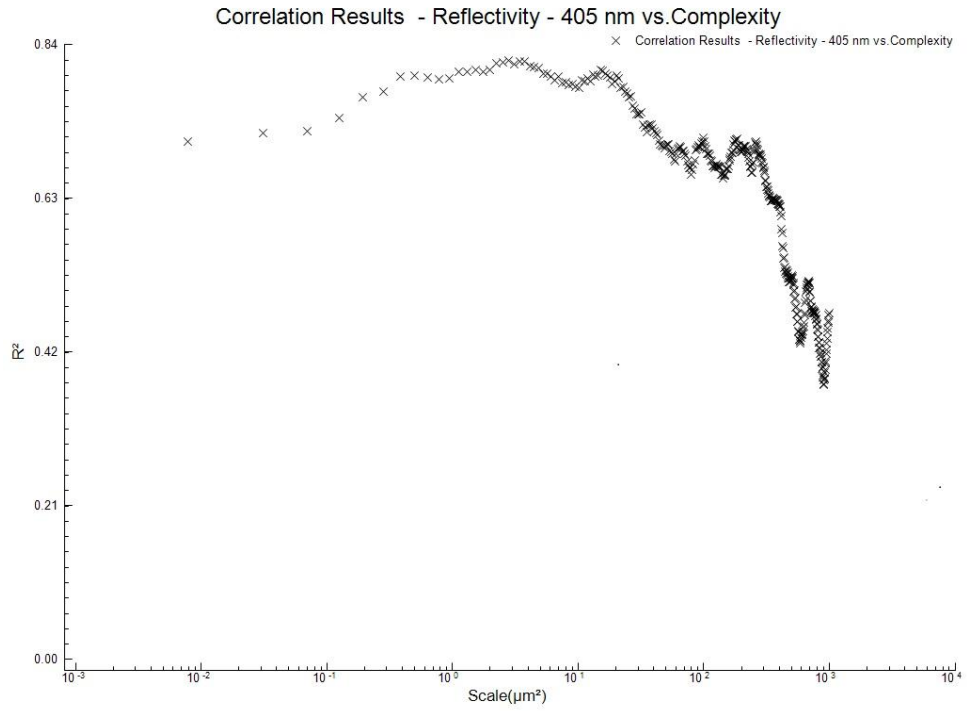


Figure 22 Complexity Correlation vs. Scale @ 405 nm

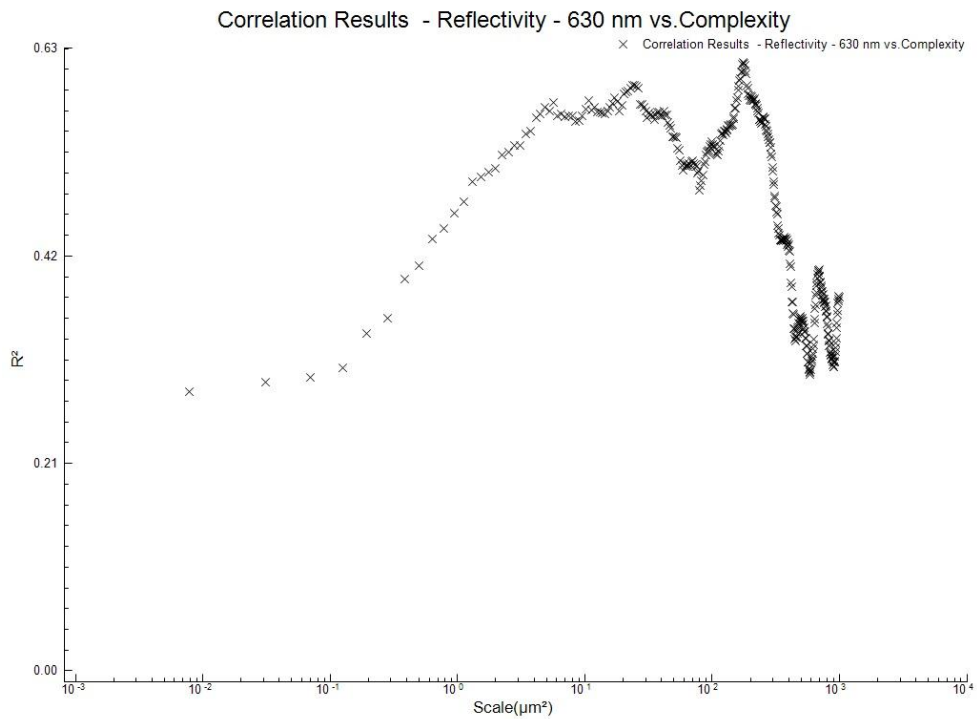


Figure 23 Complexity Correlation vs. Scale @ 630 nm

Appendix B

Mass Finisher Design Component

The purpose of this aspect of the project is to satisfy the Mechanical Systems Design aspect of the Worcester Polytechnic Institute Bachelors of Science in Mechanical Engineering program.

For this aspect of the project, an add on to the current mass finisher was designed. This was done through an Axiomatic Design process modeled after the work of Nam P Suh. The purpose of this is to simplify the design and justify all aspects of the design.

The purpose of the design is to extract parts from the mass finisher in such a way that all parts would be removed at the same time in such a way that the removal of all the media in the mass finisher is not necessary.

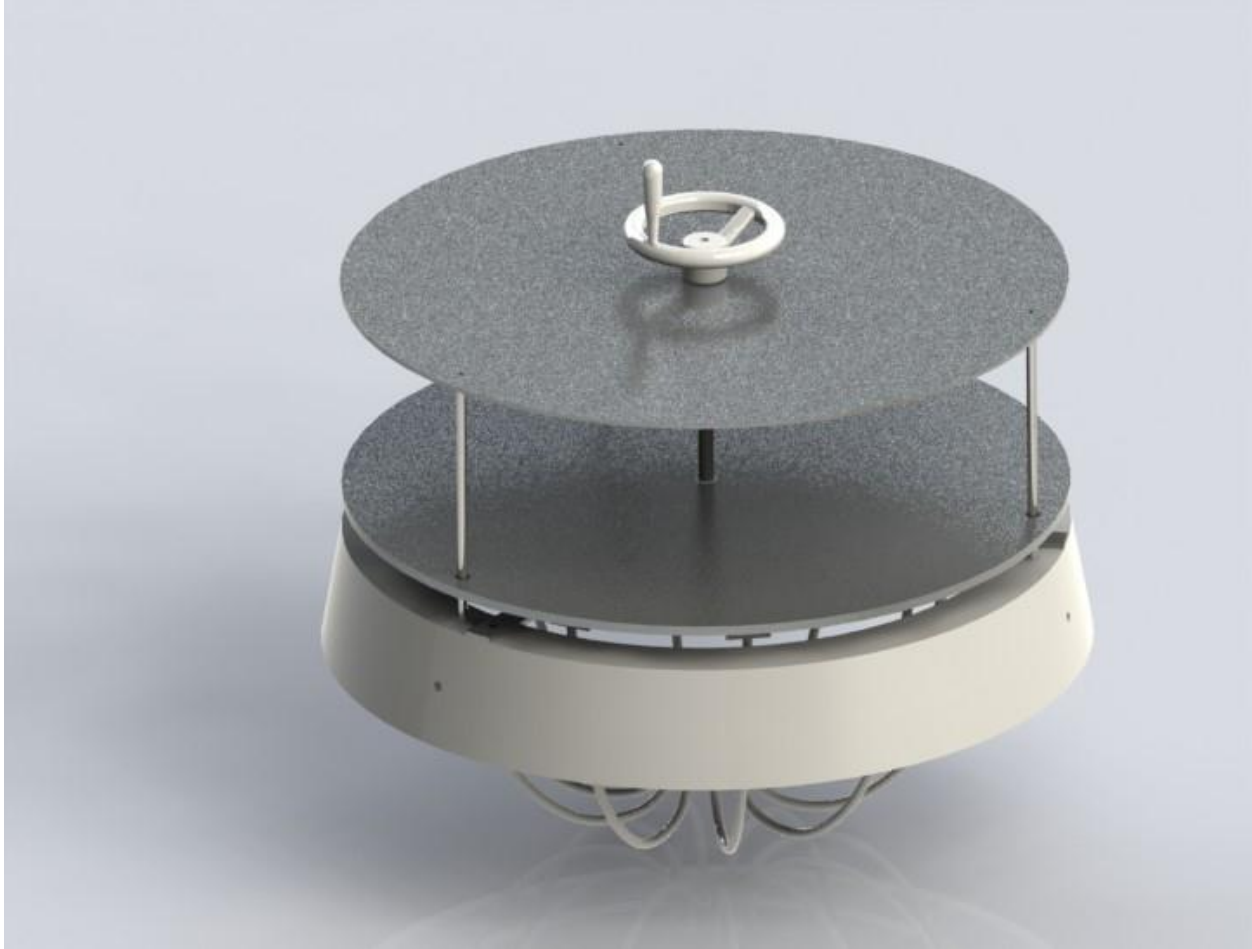


Figure 24 Final Design of Part Extraction Device (PhotoView 360 Render)

The design in Figure 24 Final Design of Part Extraction Device (PhotoView 360 Render) was the result of an Axiomatic Design Functional Requirement Design Parameter decomposition. These Functional Requirements (FR's) and Design Parameters (DP's) are listed here:

FR

1. Provide for portability
2. Provide for part removal

3. Provide for media to remain in finisher
4. Provide for extraction of parts in ranges of media where parts will exist in Mass Finisher
5. Provide for securing to finisher during extraction
6. Provide for all parts to be removed at the same time
7. Provide for no unwanted axis's of movement of moving parts

DP

1. Have a ring which can be picked up
2. Finger like devices move through media
3. Fingers vibrate to ensure media does not come out
4. Fingers will move along an arc path to remove parts
5. Device must clamp to rim of mass finisher
6. Device will use lead screw to drive in all finger mechanisms
7. Device will move downward in a fashion that only allows downward by use of guide rails, and the finger mechanisms will only be allowed to move along their arched path by channels

In this, each numbered FR corresponds to the DP with the same number.

The rationale behind each of these is that:

1. It must be easy to carry
2. The purpose of this design is to remove parts from the mass finisher
3. Dumping the Media out of the Mass Finisher is time consuming and messy
4. The parts only end up along certain parts of the media stream, and therefore anything more than this is wasted

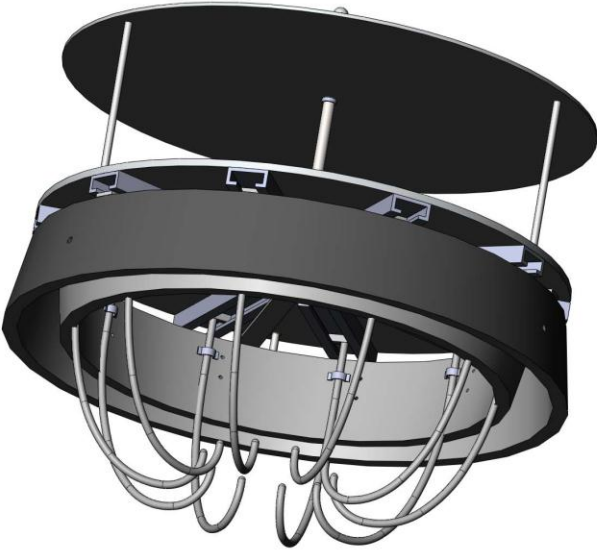
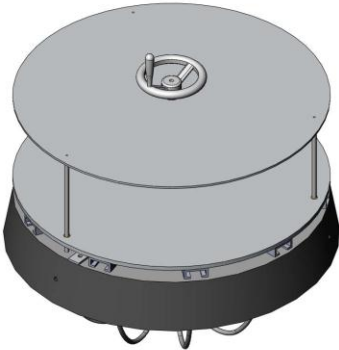
5. Securing the Part to the Finisher provides a stable platform for removal
6. If all the parts are removed at the same time you can ensure that no parts will be over finished because they get missed by the device.
7. Any unwanted axis's of movement will not allow for proper removal

	DP0:	DP1:	DP2:	DP3:	DP4:	DP5:	DP6:	DP7:
FR0:	O							
FR1:		X						
FR2:		O	X					
FR3:		O	X	X				
FR4:		O	O	O	X			
FR5:		O	O	O	O	X		
FR6:		O	O	O	O	O	X	
FR7:		O	O	O	O	O	O	X

Figure 25 Acclaro Screen Shot

Above is an image taken from Acclaro, which is my FR DP decomposition in matrix form. This shows a Triangular matrix, which means that the design is “partially coupled” due to an issue I foresaw in FR’s 2&3. Therefore I adjusted my design accordingly to avoid any interference in the overall design. However, not the most ideal case, a partially coupled design is far better than a completely coupled design, but less ideal than an uncoupled design.

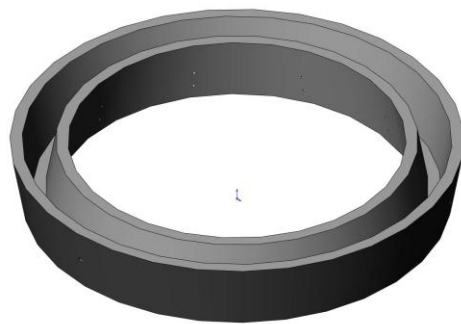
Assembly Top Level



PARTS

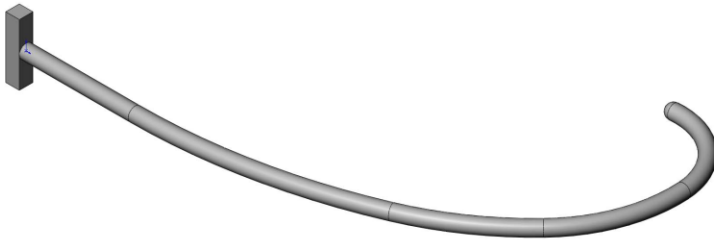
Note: Each of the Numbered parts corresponds to the FR and DP set forward in the previous section.

DP 1



This is a guide ring and is the base part of the entire assembly. This channel seen above goes around the ring of the mass finisher.

DP 2



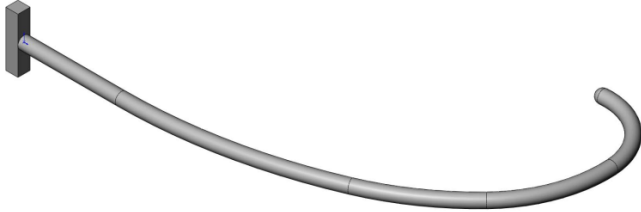
This bent piece of rod will serve as the portion which enters the media.

DP 3



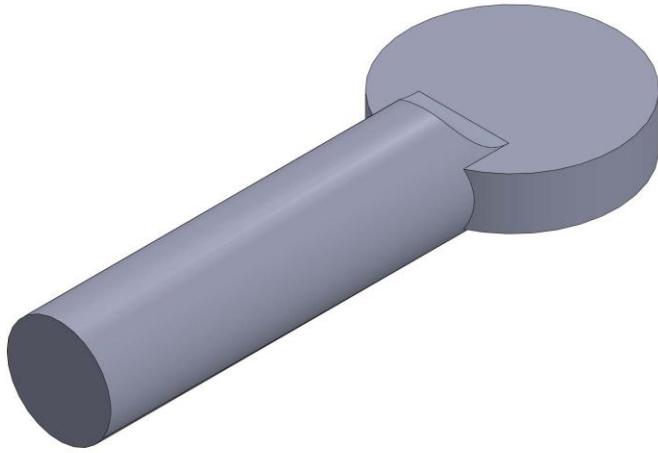
This vibratory motor will be incased in a box which will also contain a battery unit for power under the travel plate (See DP 6).

DP 4



This finger like mechanism is the part which goes into the media to remove the parts and the curvature of the part ensures its motion.

DP 5

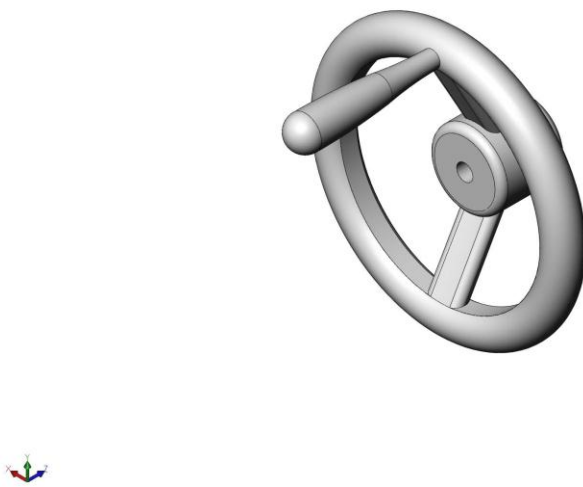


This is a Wing screw which is used to secure the ring to the mass Finisher and ensures that the ring can be secured to the mass finisher.

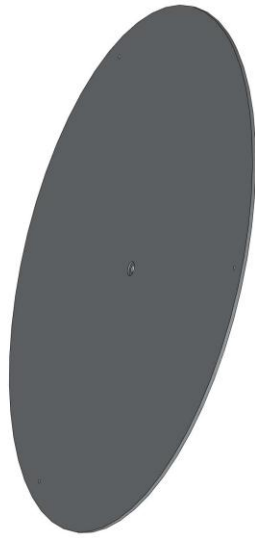
DP 6



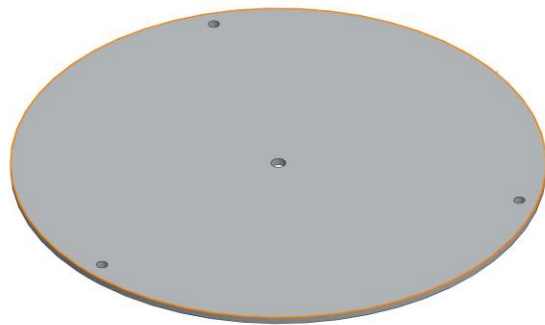
This is an image of the lead screw. The pitch is $\frac{1}{2}$ -2 which means that with just 12 turns of the screw the device will be fully engaged.



This is a handle which drives the lead screw.



This is the top plate which captures the lead screw and bearings



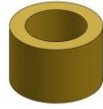
This is a plate which travels up and down via the lead screw and a nut. The Plate has guided rails which pass through it and the lead screw passes through the center.



This Plate Captures the lead screw on the bottom and holds the bottom bearing, the large cut outs are to provide clearance for the finger mechanisms.

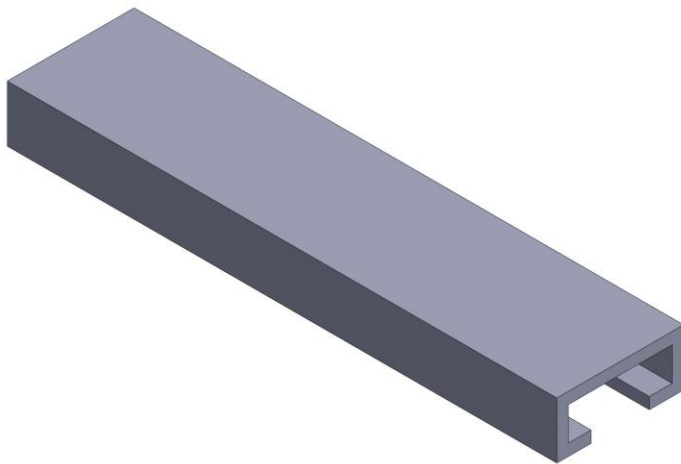


This is the guide rail which the traveler plate moves along

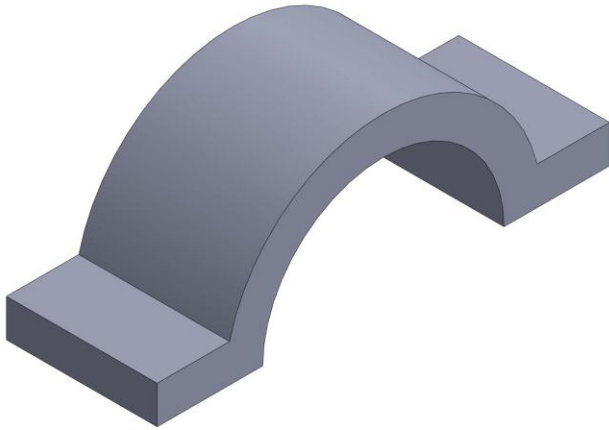


This is a bronze bushing which is compression fit into the traveler plate to ensure that the motion is smooth and minimizes the chances of binding.

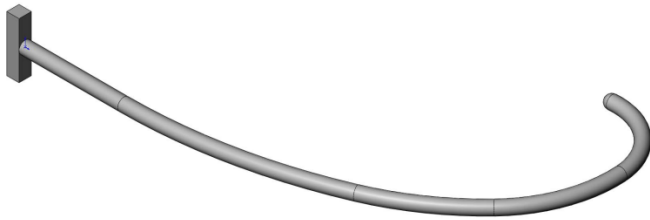
DP 7



This is a guide channel. The purpose of this device is to ensure that the finger mechanisms cannot twist during their insertion into the medial.

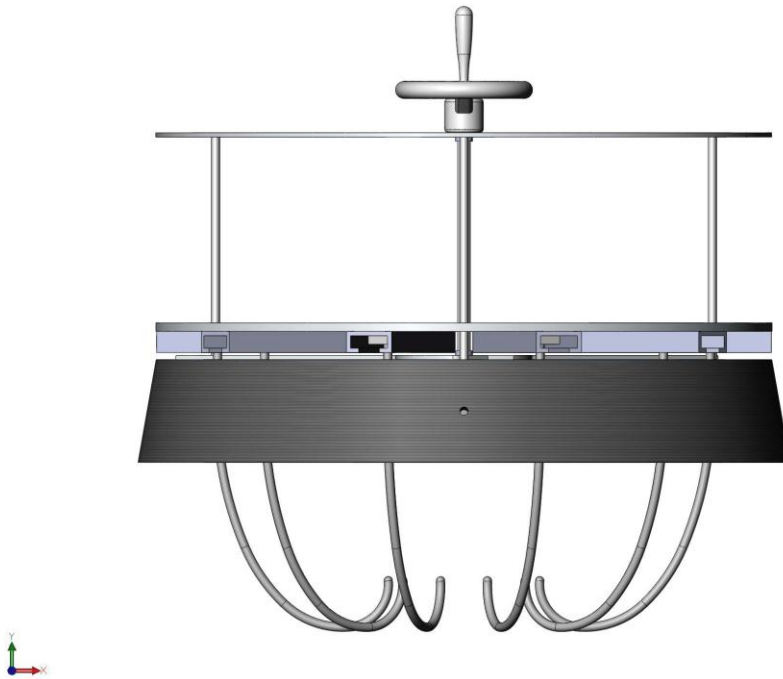


This Mechanism guides the shaft of the finger mechanisms through its travel keeping it in one place.



The top square portion of the finger mechanism travels through the guide channel and ensures no twisting during the function of the device.

Assembly



This is a side view of the assembly, which shows the traveler plate, the guide channels, the fully engaged fingers, and the general setup of the lead screw which is capture top and bottom and drives the travel plate.